



ENR501474 | Nonlinear Static Simulation of an Oil and Gas Multicontact Seal Application

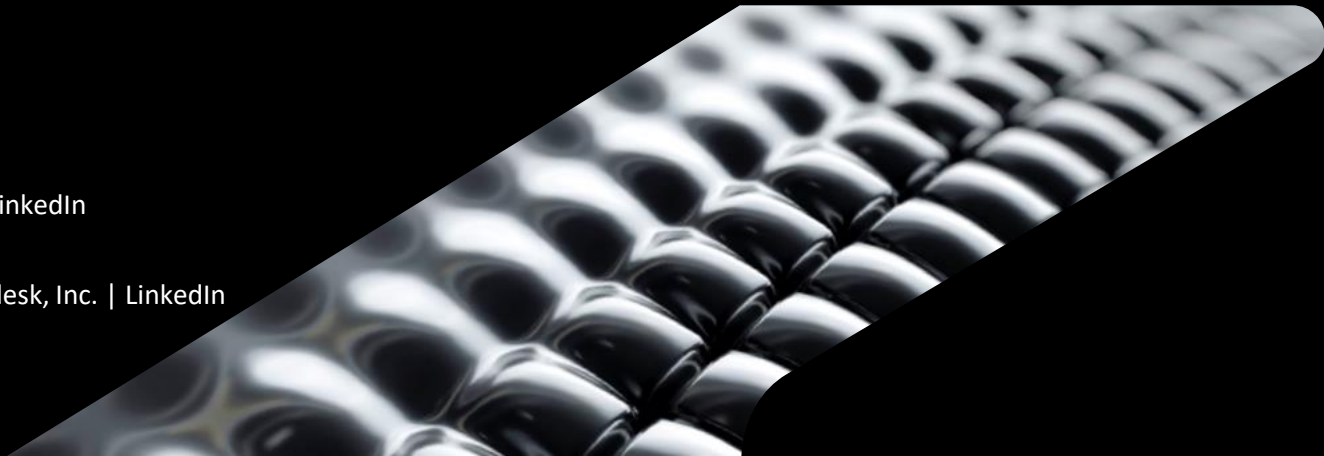
Wednesday September 28th 11:30 am

Arne Kjaer

CEO – Owner | PTFE Engineering A/S | LinkedIn

David Weinberg

Distinguished Research Scientist | Autodesk, Inc. | LinkedIn





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Arne Kjaer

CEO / owner @ PTFE Engineering

- Polymer Specialist and Mechanical Engineer from the Technical University of Denmark
- 39 years of experience in development of material compositions and processing within the PTFE industry
- First FEA material model work in 1992 with the University of Stuttgart
- Polymeric Materials Modeling for 6 years with, Autodesk Nastran, LS Dyna, COMSOL and ANSYS.
- Meet David first time at AU 2015 in Las Vegas





David Weinberg

- Distinguished Research Scientist with Autodesk
- Autodesk Product Development and Manufacturing Solutions (PDMS), Nastran Simulation and Generative Design group
- Primary developer for Autodesk Nastran and Inventor Nastran
- Currently lead the team of developers for Autodesk Nastran
- Over 35 years' experience in FEA simulation working both as a user for several large Aerospace companies and as a developer
- Retired USAF aircraft commander/pilot

AUTODESK UNIVERSITY



AU presentations by

- David and Arne

AU 2018 – Las Vegas

- *Challenges of Simulating Advanced Materials in Nonlinear Applications*

AU 2019 – Las Vegas

- *Simulating with Nonlinear Materials like Hyperelastic and Isotropic Polymer Material*

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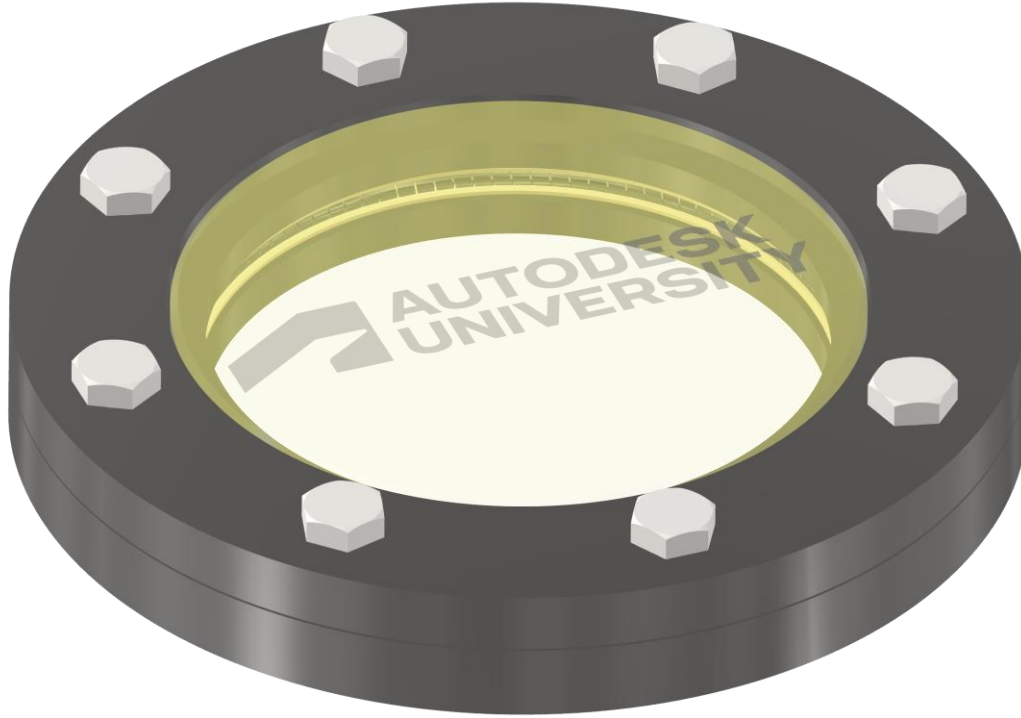
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Learning Objectives.

- Prepare the Inventor Assembly to the Nastran Simulation.
- Setup of a Nonlinear Static Nastran Analysis from an Inventor Assembly.
- Using Material Model Data from Customer Material Measurements.
- Using multiple Subcases using same constraints and loads.
- Setup of Enforced Motion, Surface Pressure.
- Optimize the Mesh and Mesh Control to get reliable results in less time.
- Special Parameters setting to help the Analysis Running.
- Looking at the Results

Case Story

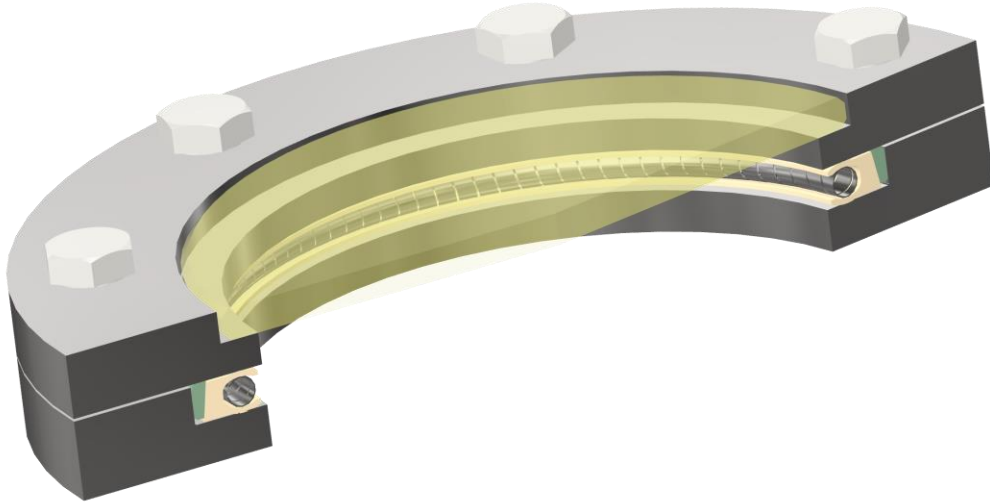


An Inspection Hatch in a Machinery with high Pressure and elevated Temperature need to be sealed of so the inside substance can not escape to the outside.

This Hatch is constructed to be used for this demonstration of Inventor Nastran 2023.

This case is constructed only for the AU 2022 in New Orleans, USA.

Case Story



Cross section of the Hatch showing the Sealing System making a tight assembly between the lid and the groove.

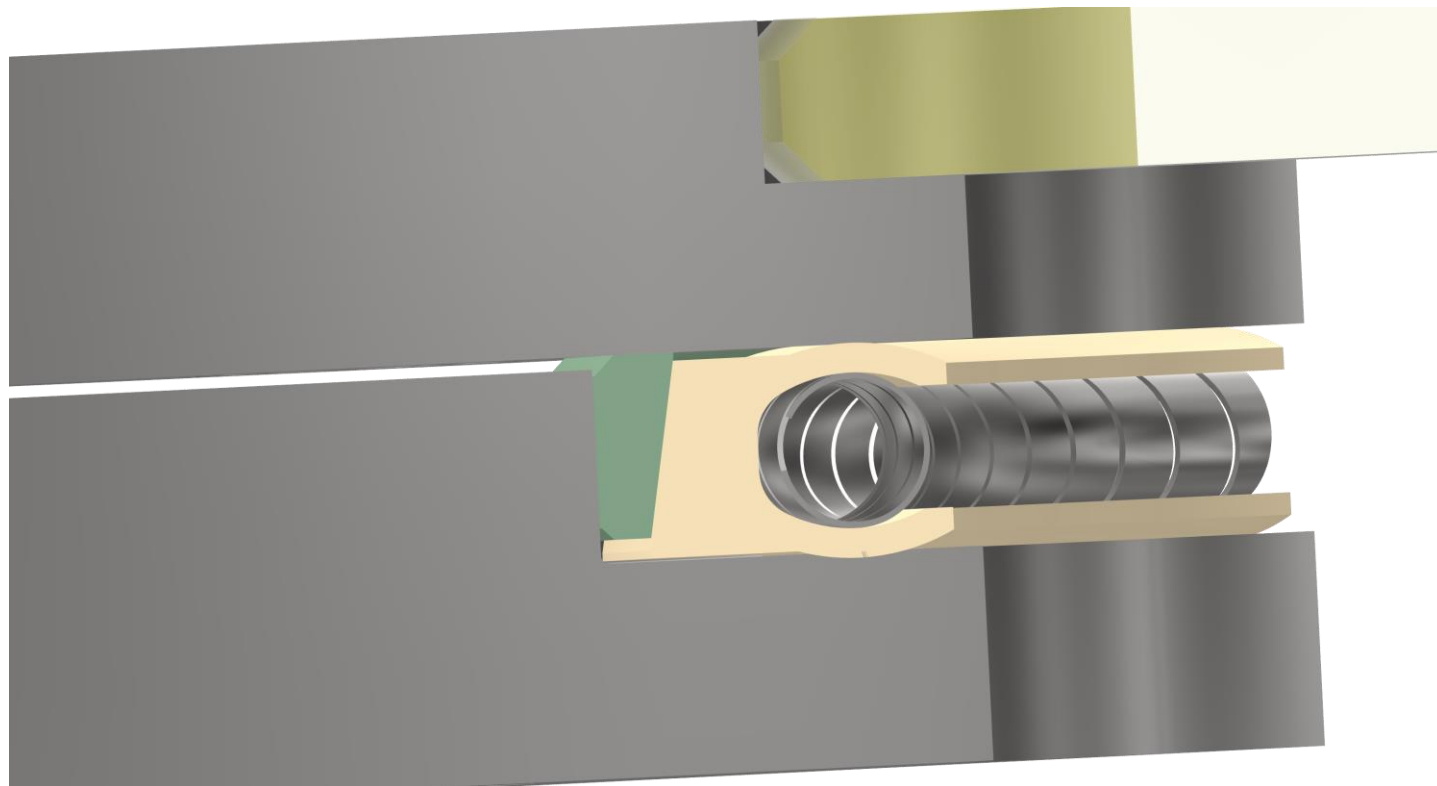
The Seal is a high-pressure Metal Spring Activated Seal supported by a PEEK Back UP Ring to prevent the Seal the escape in the clearance between the groove and the Lid.

Pressure and temperature in such a case will typically be room temperature and compressed air-pressure.

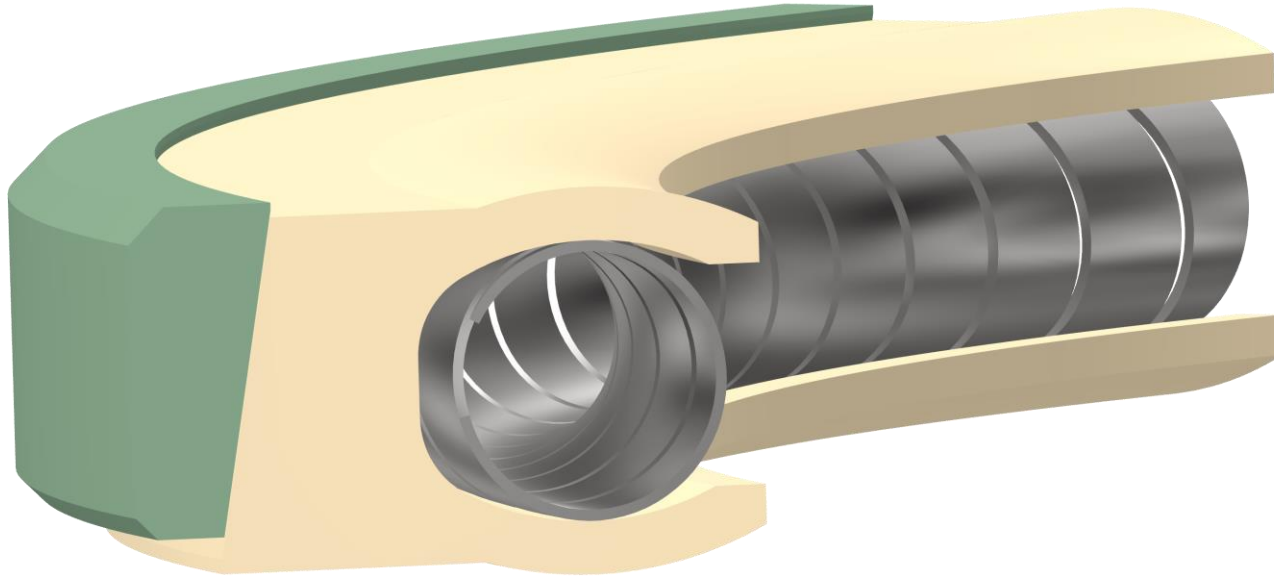
In this case here we calculate with much higher pressure 1450 psi.

Temperature will be calculated at 73°F

Case Story



Case Story

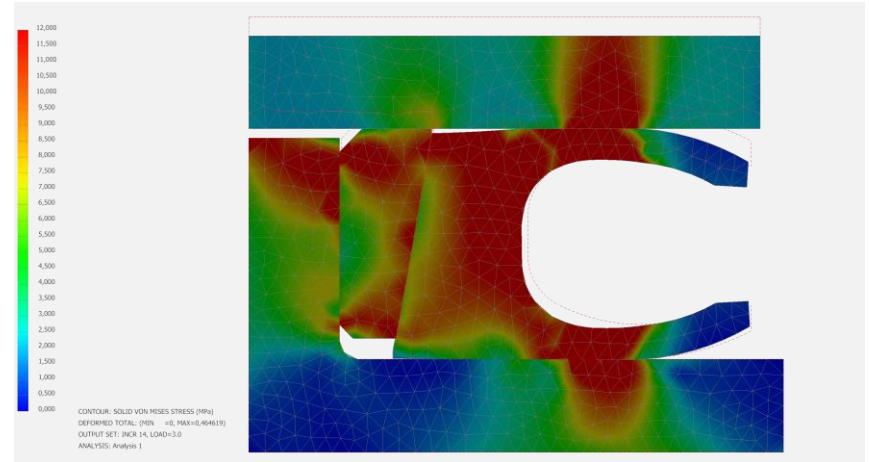
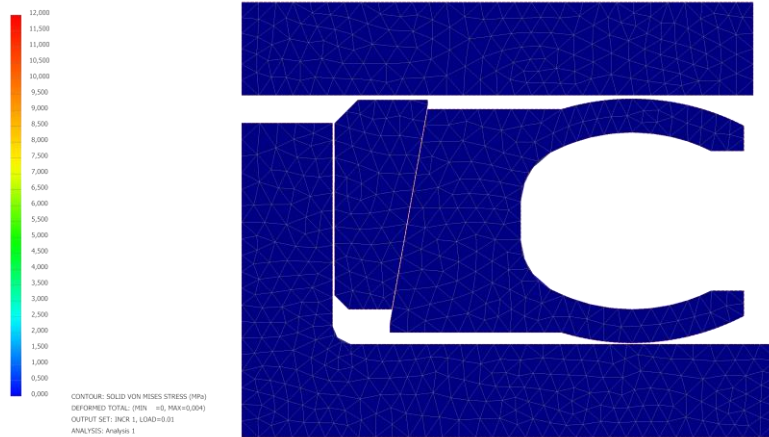


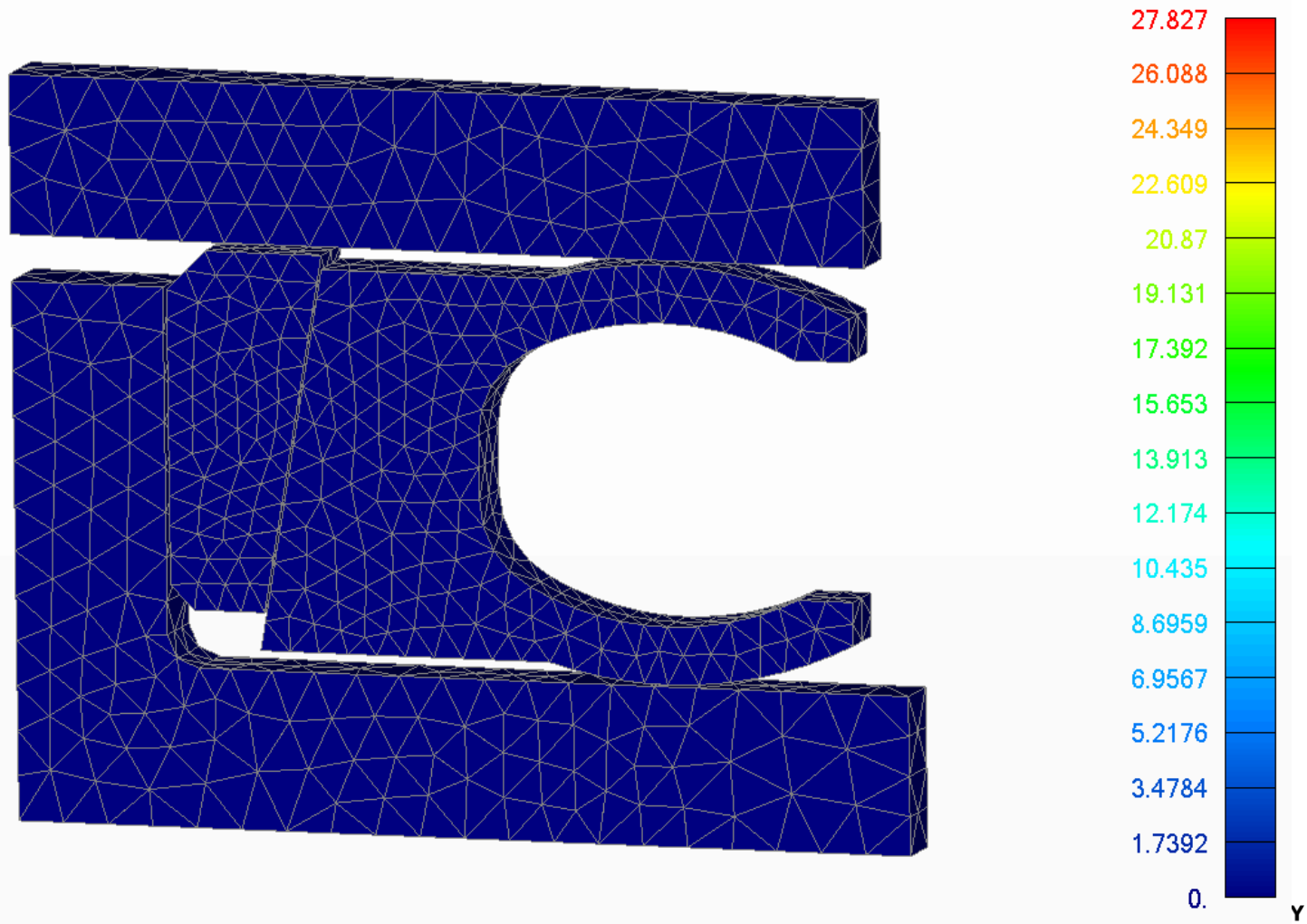
We need to make this Assembly simpler to be able to simulate it.

The Metal Spring has to be exchanged by a spring force or a surface pressure.

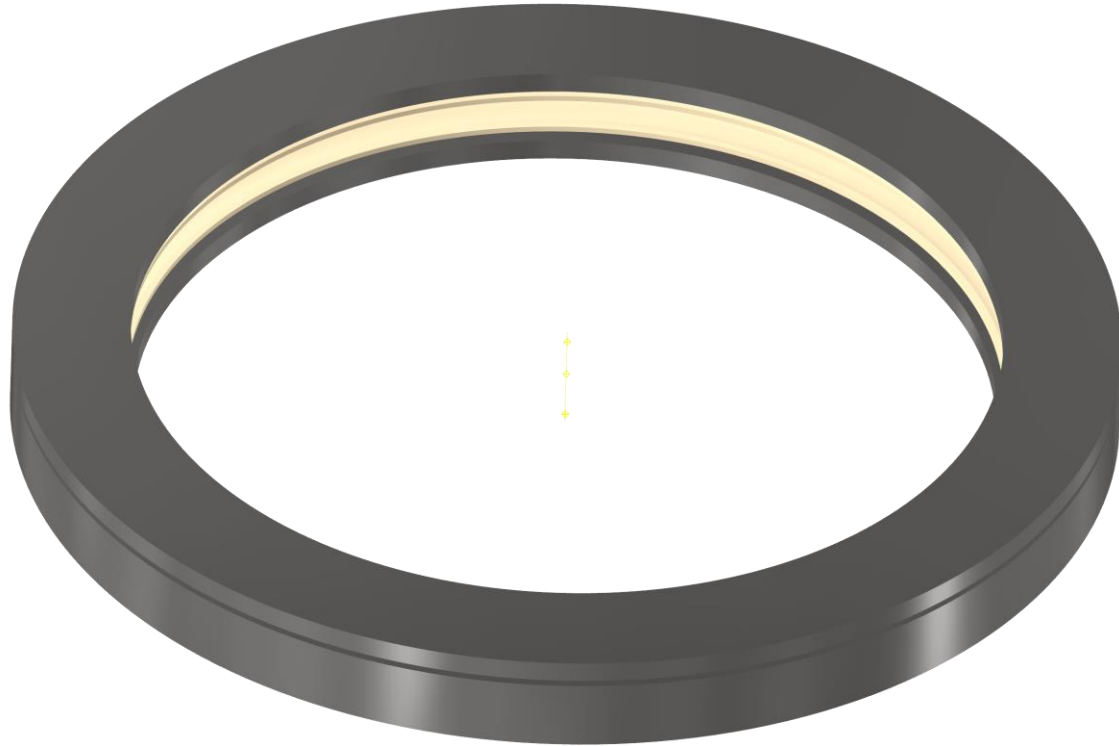
What do we simulate in this class ?

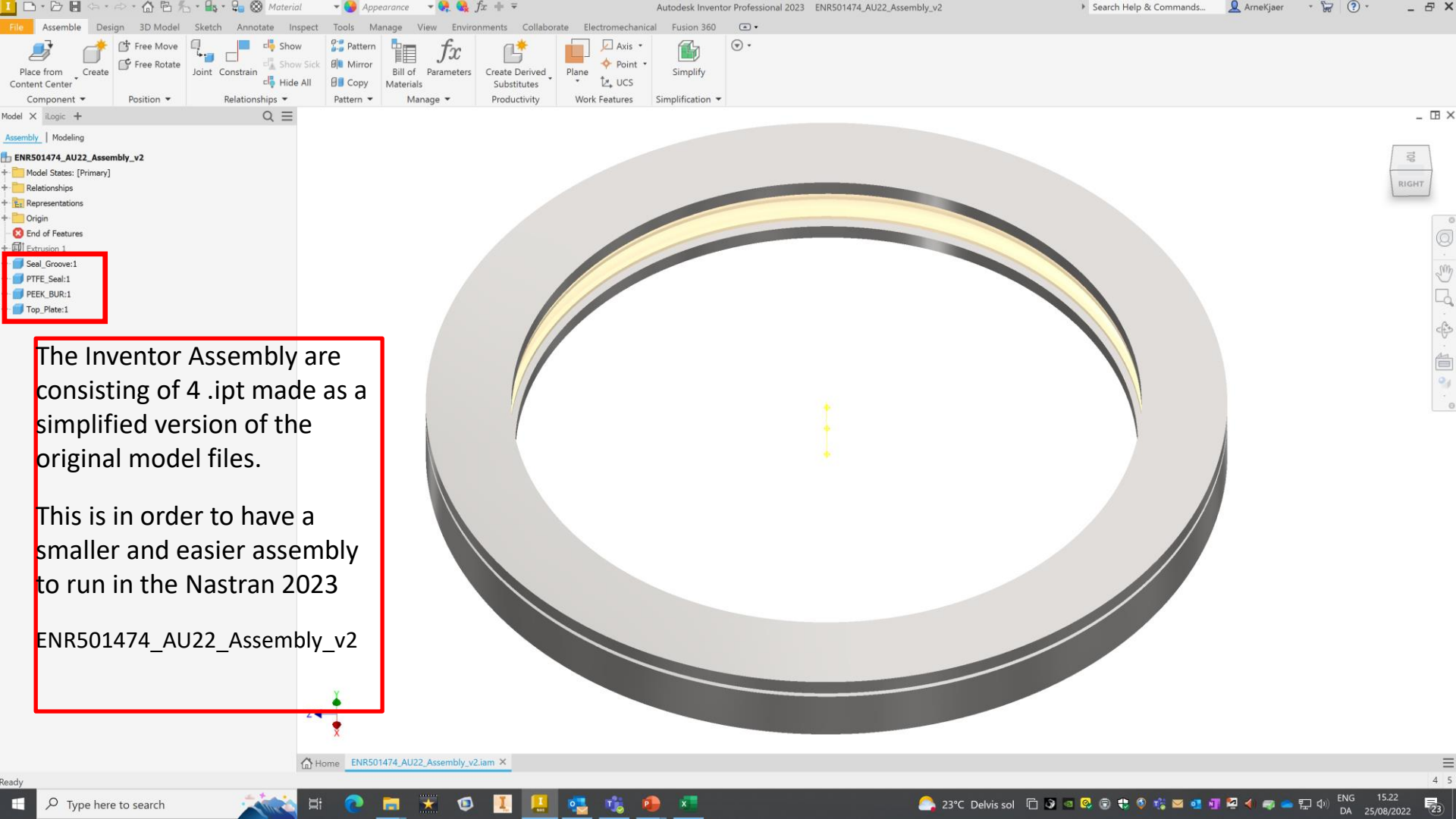
Initial compression of the installed seals, metal spring simulation and high-pressure simulation





Autodesk Inventor Nastran 2023 Assembly



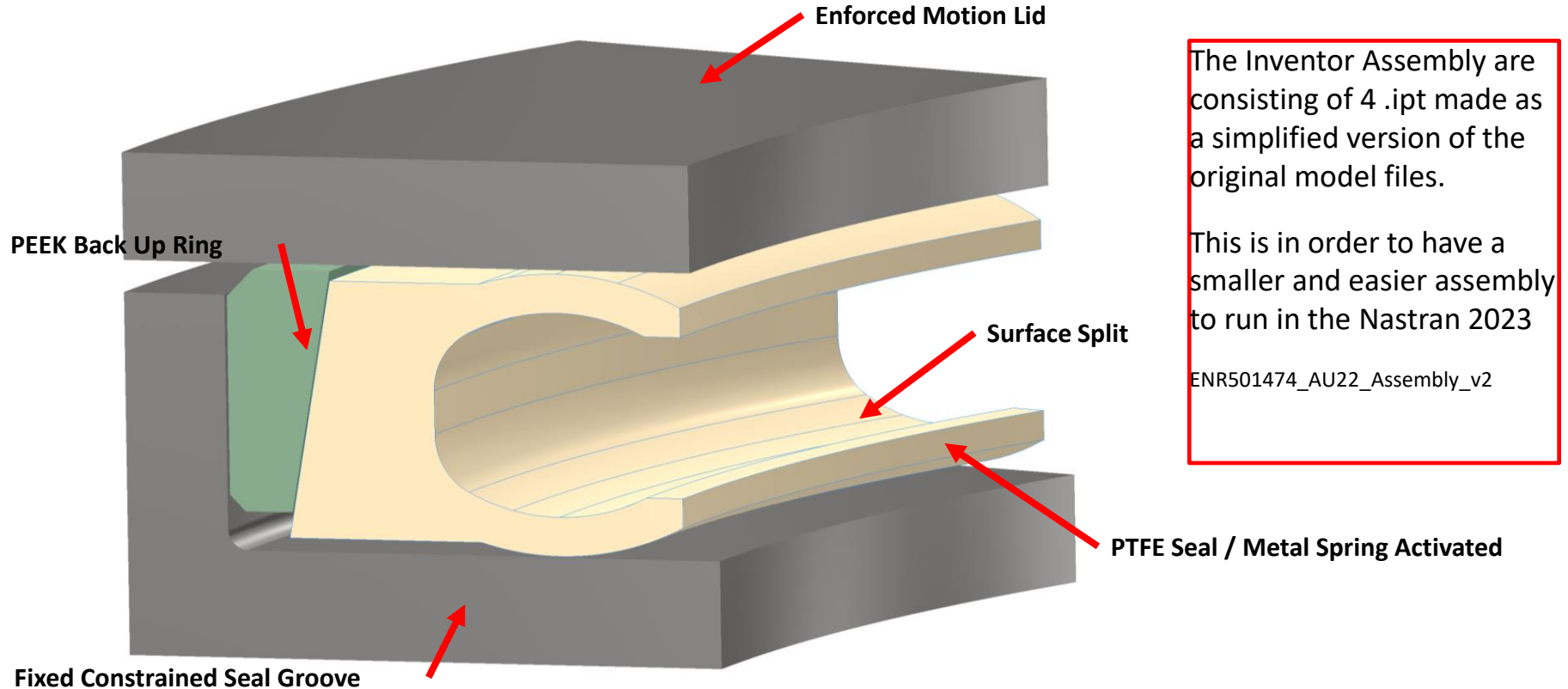


The Inventor Assembly are consisting of 4 .ipt made as a simplified version of the original model files.

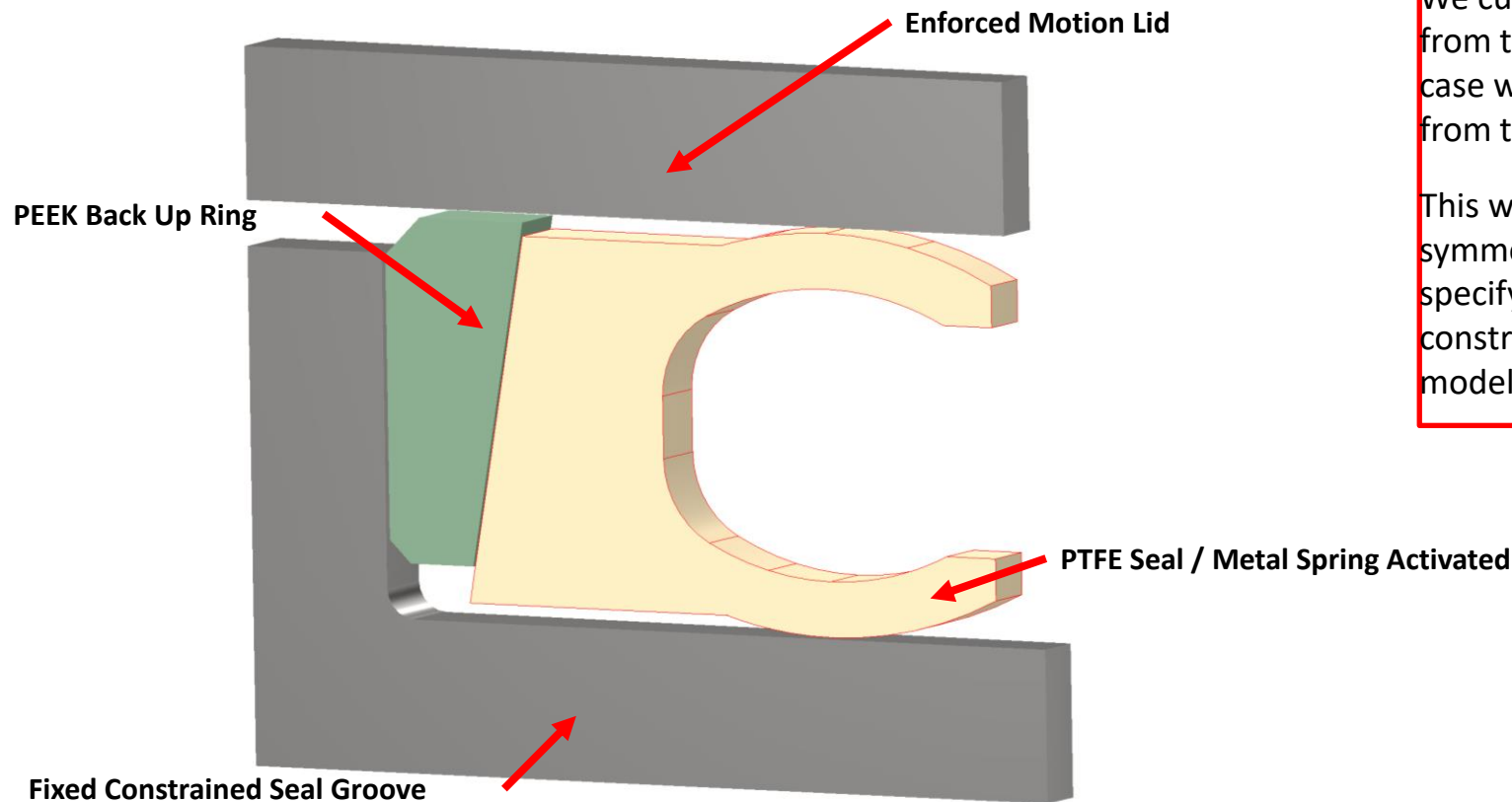
This is in order to have a smaller and easier assembly to run in the Nastran 2023

ENR501474_AU22_Assembly_v2

Autodesk Inventor Nastran 2023 Assembly



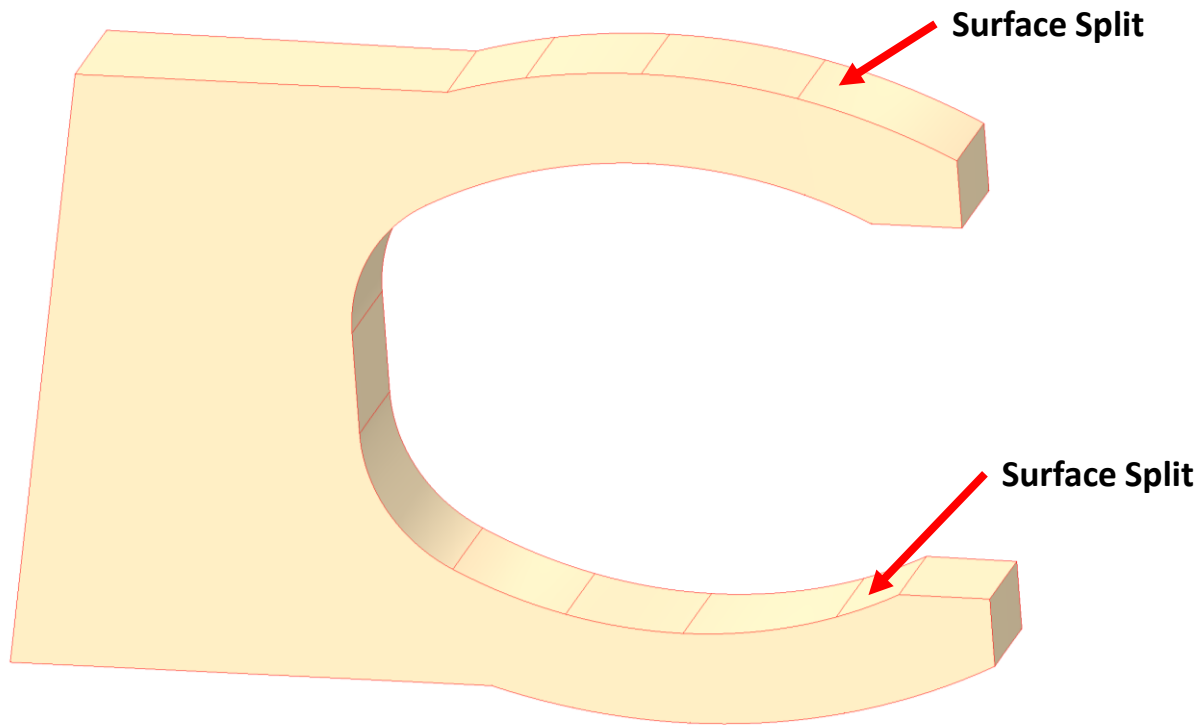
Autodesk Inventor Nastran 2023 Assembly



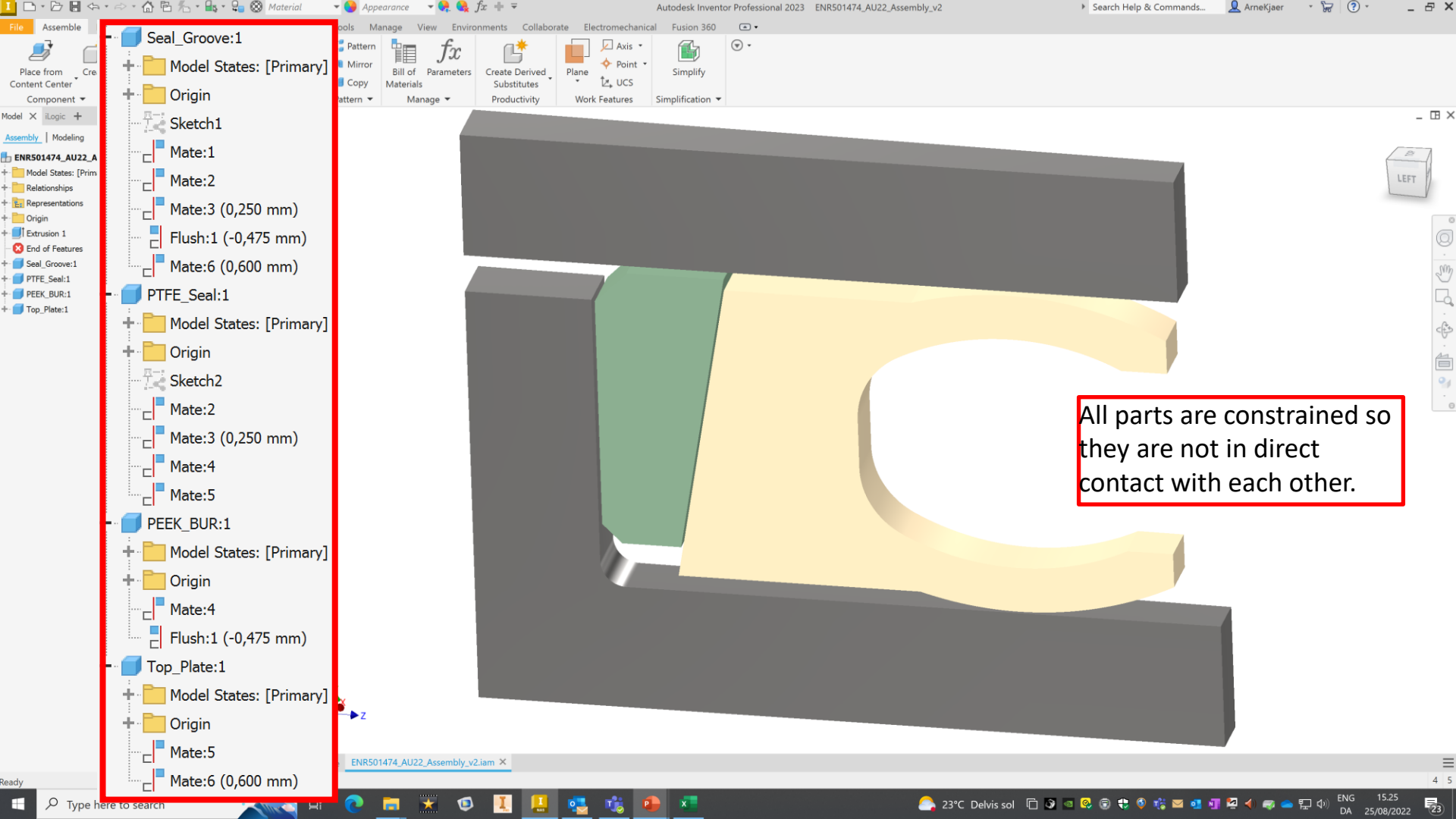
We cut out a smaller slice from the Assembly, in this case we are using $\pm 0,50^\circ$ from the radial centerline.

This will make the symmetry easier when specifying the symmetry constrain in the simulation model in Nastran 2023

Autodesk Inventor Nastran 2023 Assembly



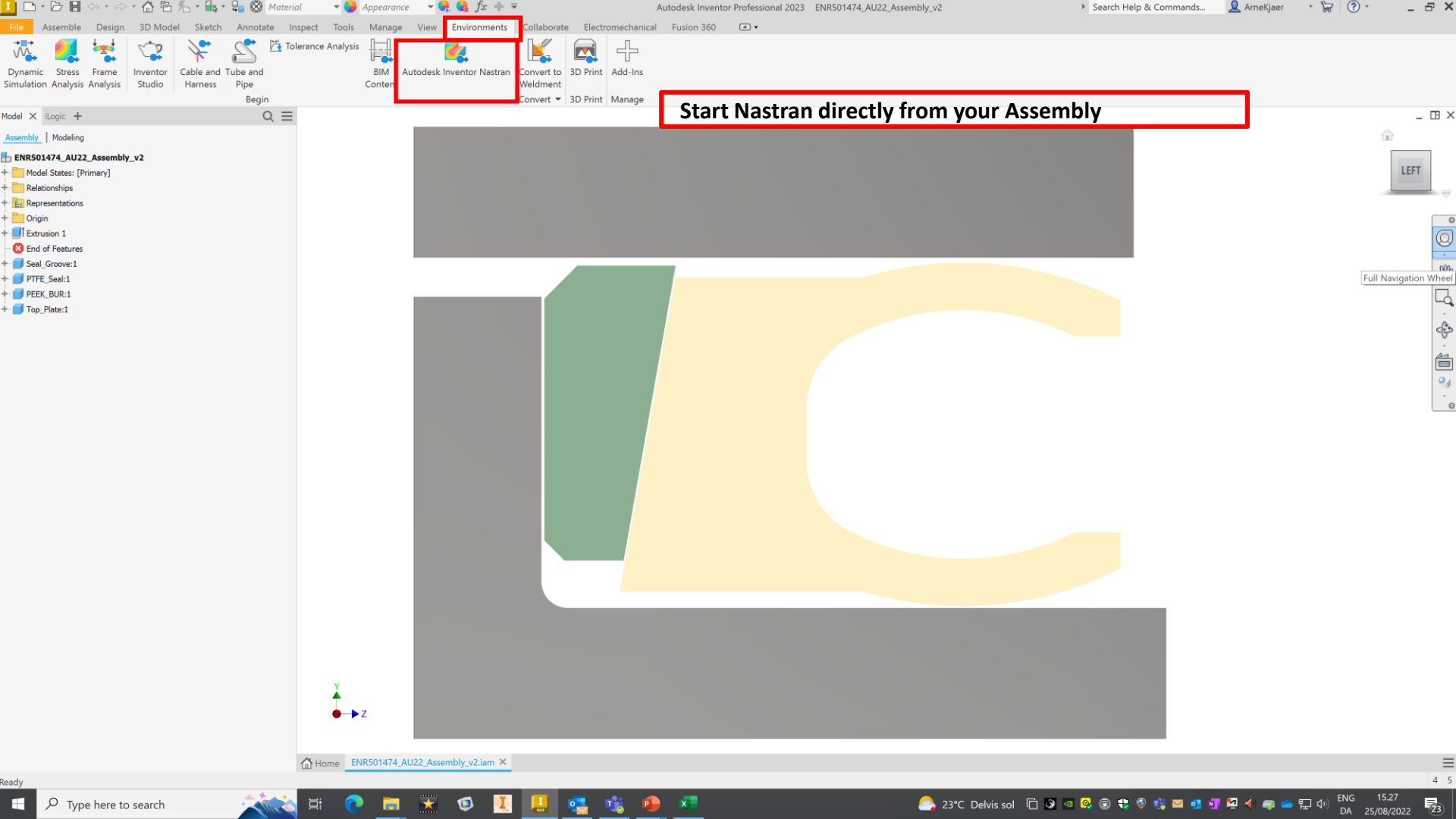
The Seal has been split into several surfaces in order to apply forces and constraints into smaller parts of surfaces. We will later apply a load on those areas.

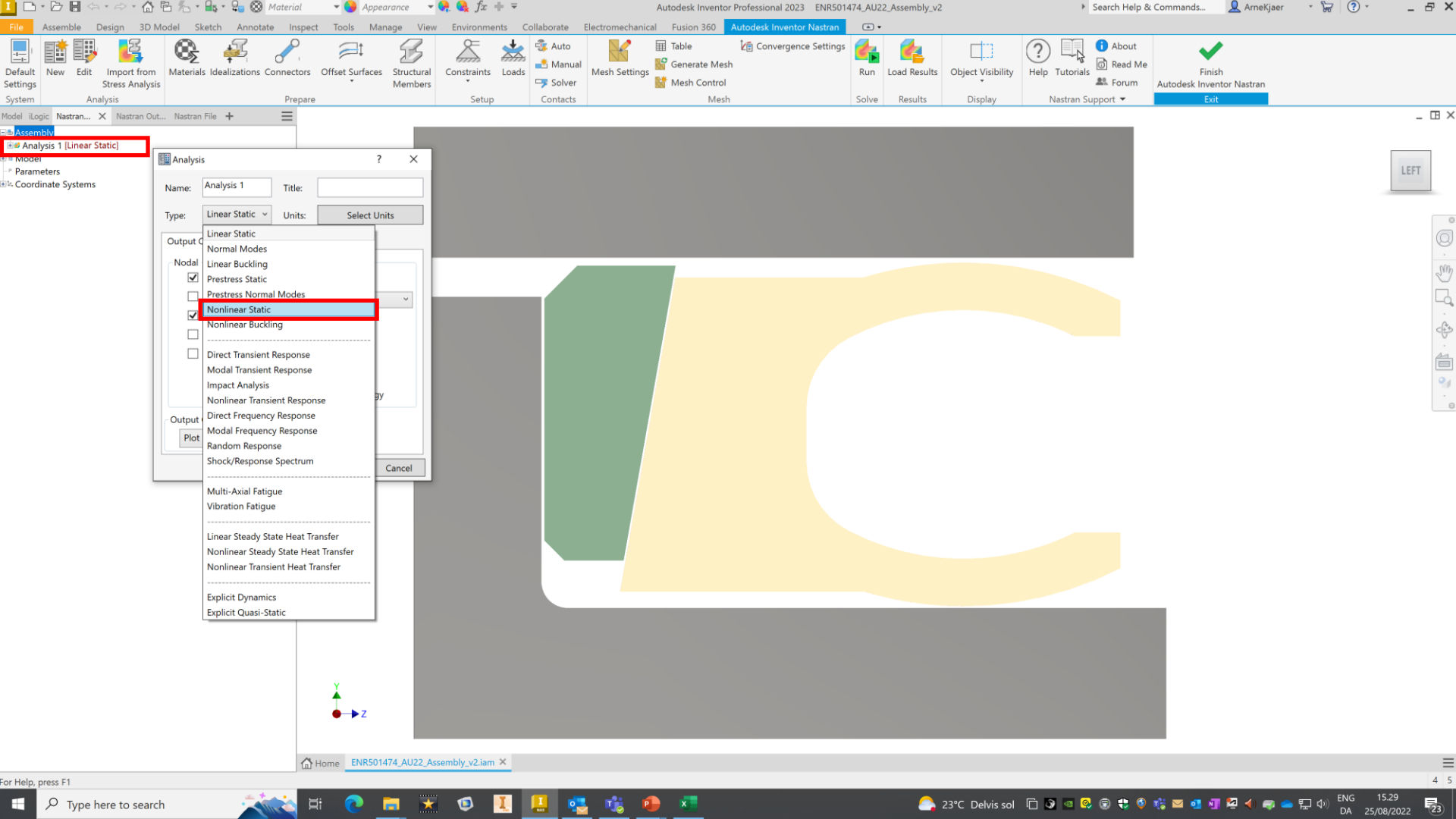


Analysis Method

Coordinate System

Material Set Up





Analysis 1 [Linear Static]

Analysis

Name: Analysis 1 Title:

Type: Linear Static Units: Select Units

Output

Nodal

- ☒ Linear Static
- ☐ Normal Modes
- ☐ Linear Buckling
- ☒ Prestress Static
- ☐ Prestress Normal Modes
- ☒ Nonlinear Static
- ☐ Nonlinear Buckling
- ☐ Direct Transient Response
- ☐ Modal Transient Response
- ☐ Impact Analysis
- ☐ Nonlinear Transient Response
- ☐ Direct Frequency Response
- ☐ Modal Frequency Response
- ☐ Random Response
- ☐ Shock/Response Spectrum

Output

Plot

Cancel

Multi-Axial Fatigue

Vibration Fatigue

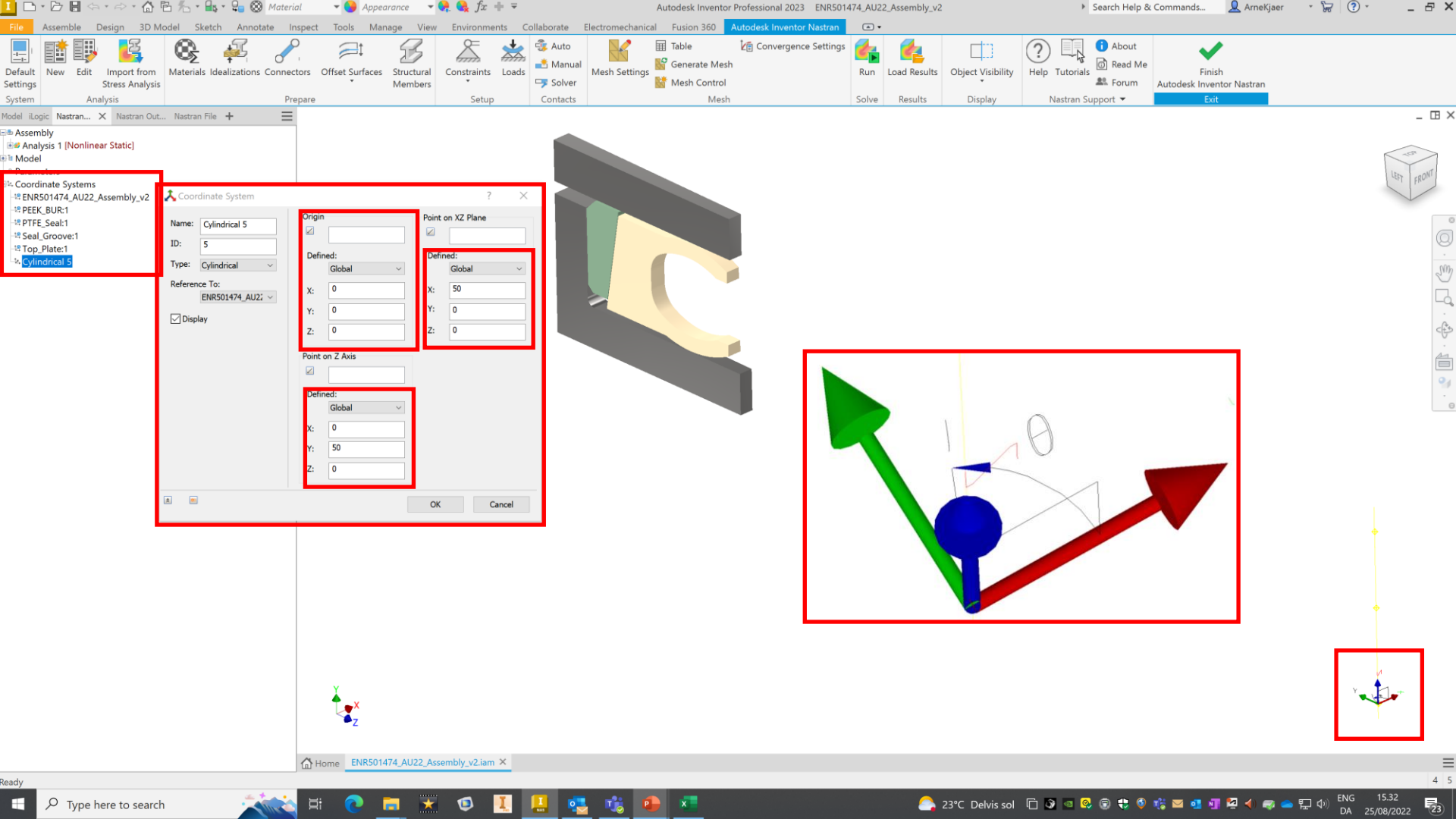
Linear Steady State Heat Transfer

Nonlinear Steady State Heat Transfer

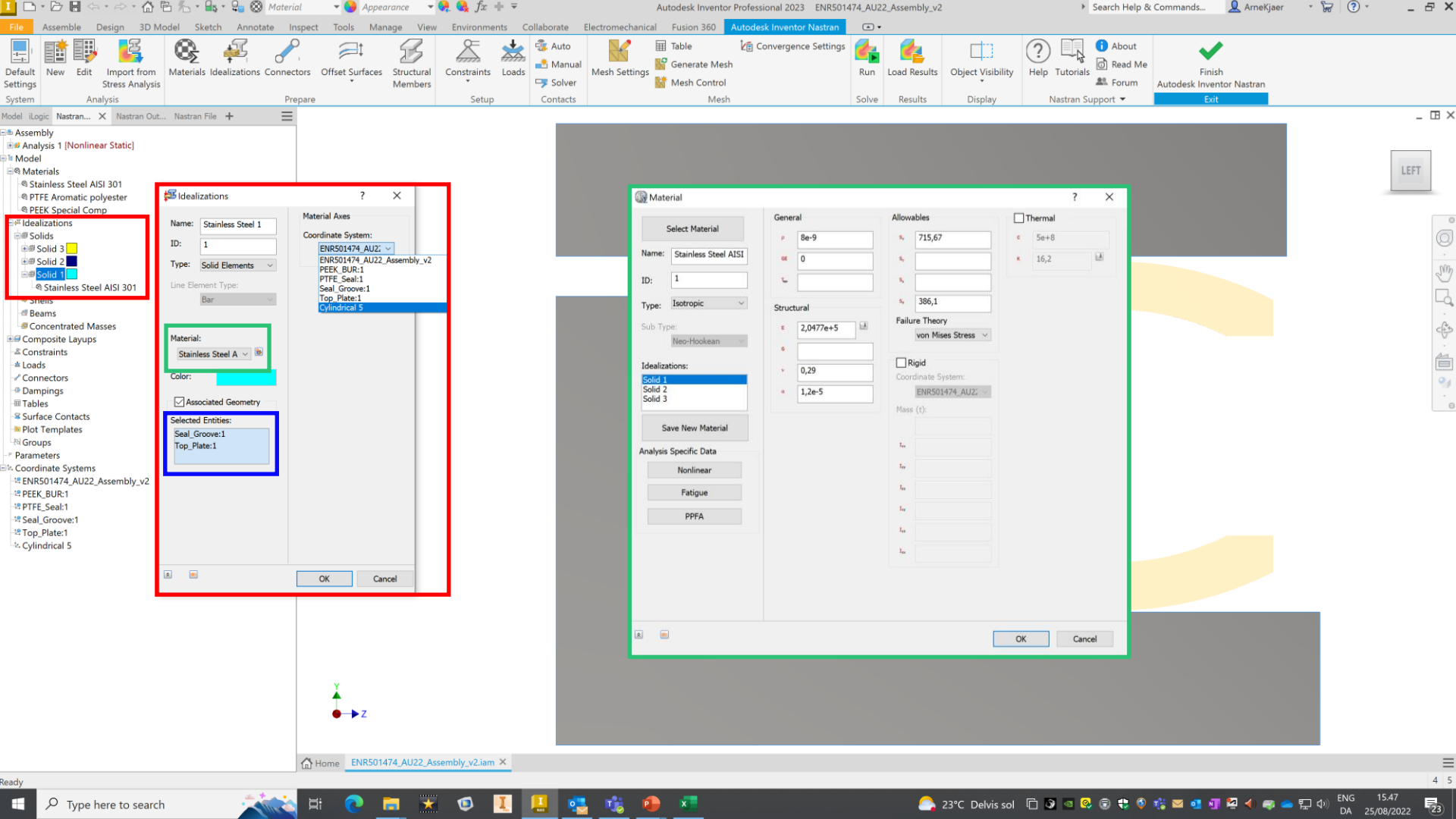
Nonlinear Transient Heat Transfer

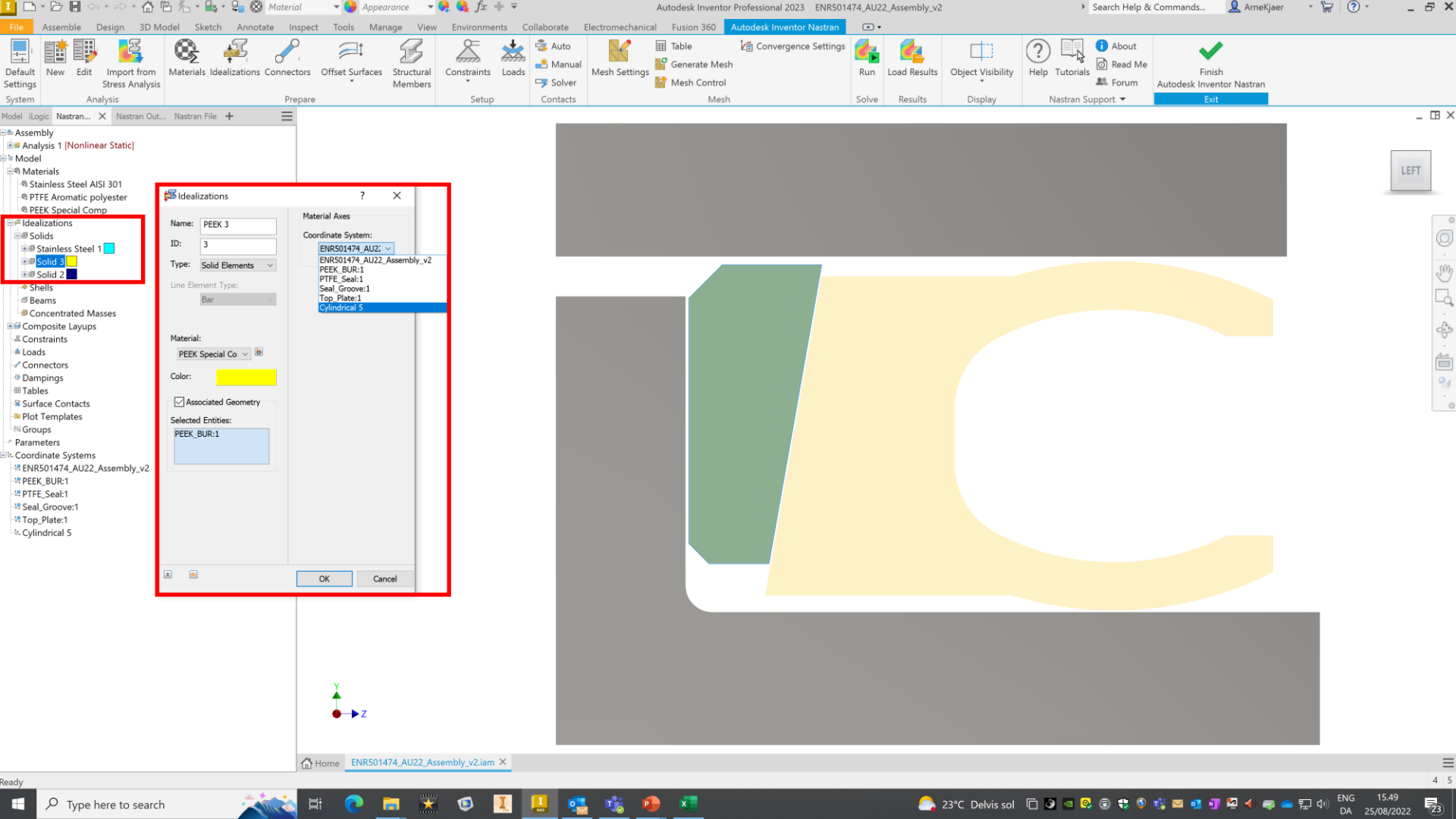
Explicit Dynamics

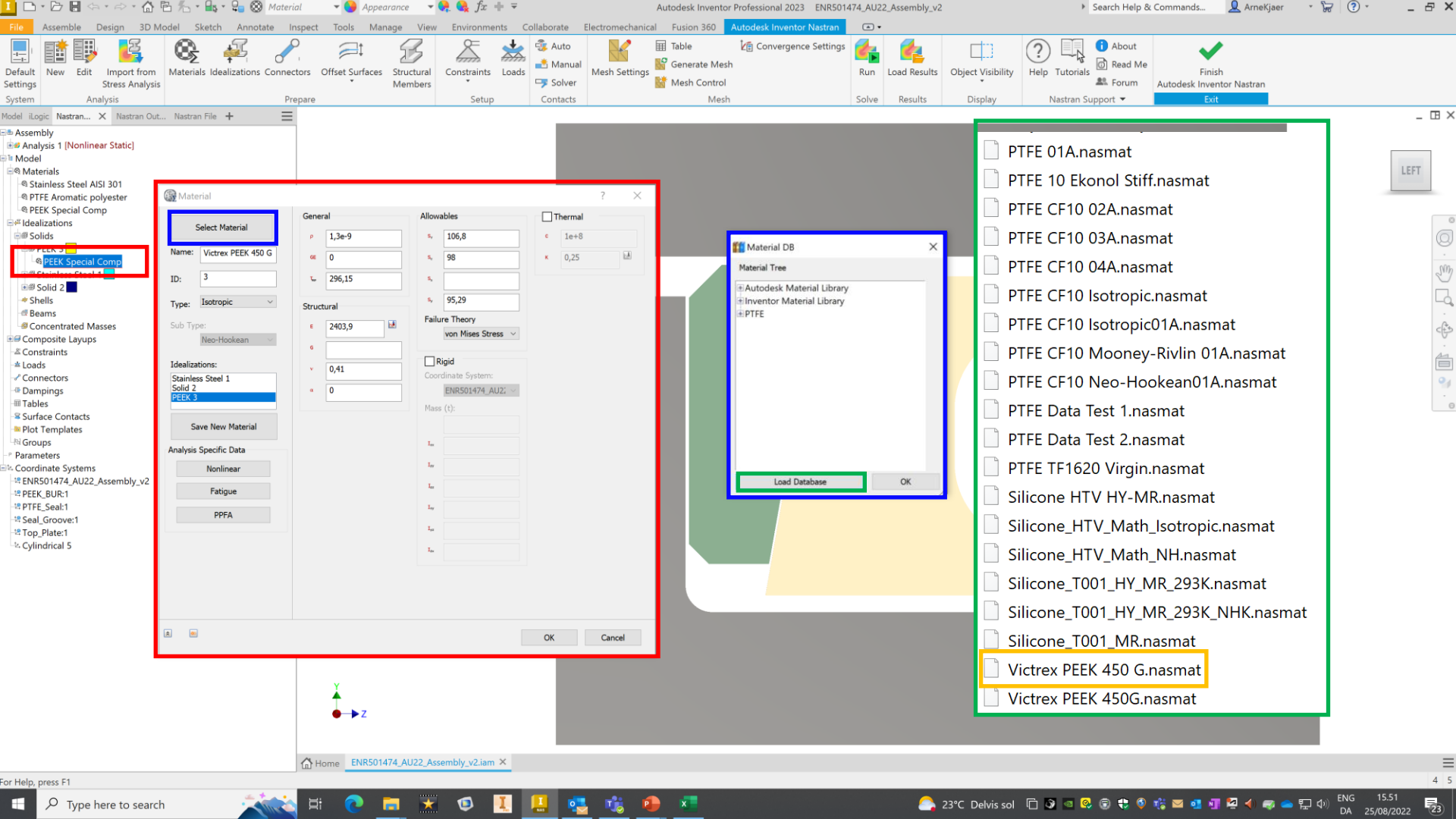
Explicit Quasi-Static

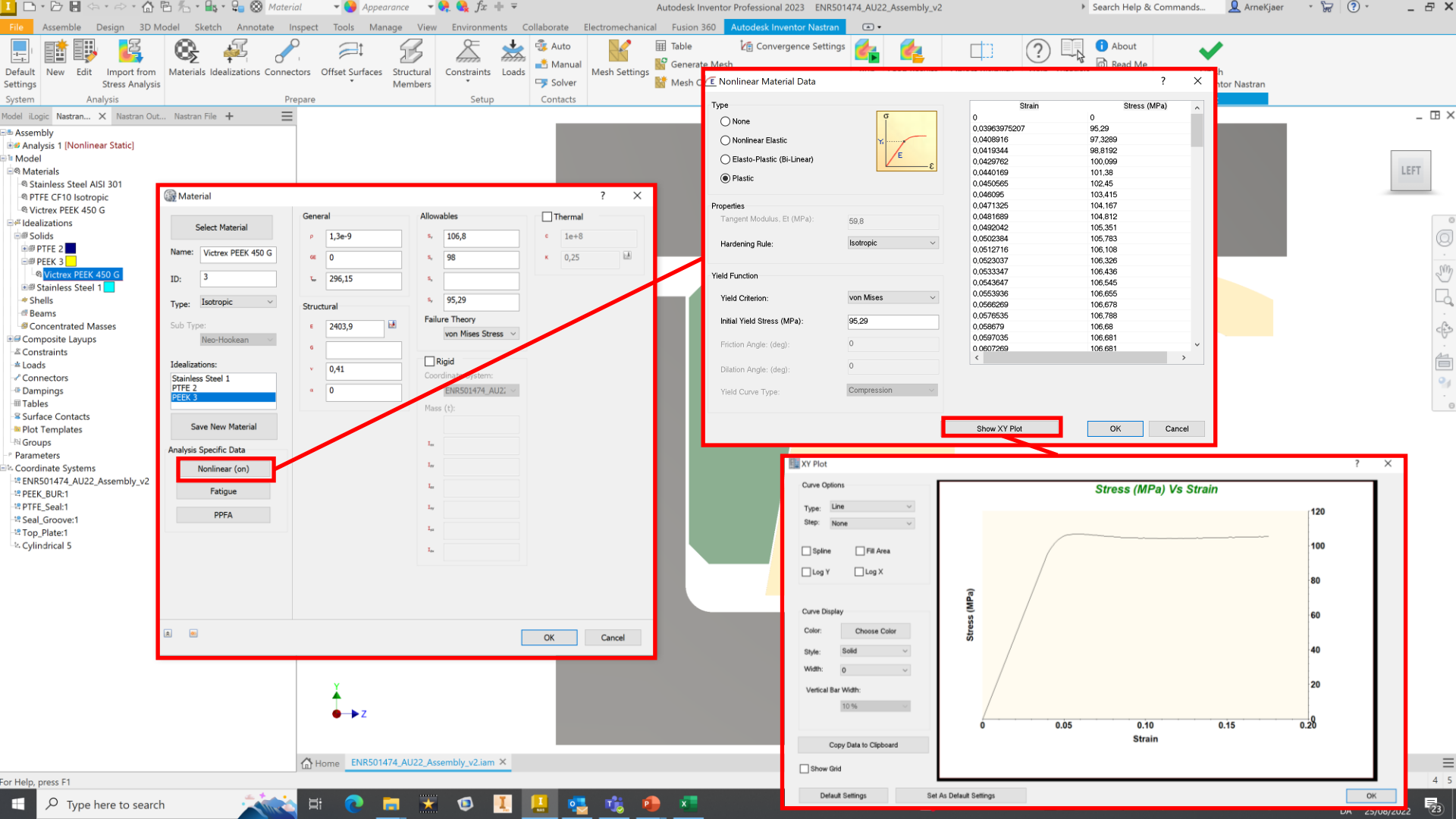


Material data





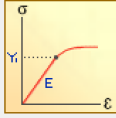




Nonlinear Material Data

Type

- ☐ None
☐ Nonlinear Elastic
☐ Elasto-Plastic (Bi-Linear)
☒ Plastic



Properties

Tangent Modulus, E_t (MPa):

59,8

Hardening Rule:

Isotropic

Yield Function

Yield Criterion:

von Mises

Initial Yield Stress (MPa):

95,29

Friction Angle: (deg):

0

Dilation Angle: (deg):

0

Yield Curve Type:

Compression

Strain Stress (MPa)

0	0
0,03963975207	95,29
0,0408916	97,3289
0,0419344	98,8192
0,0429762	100,099
0,0440169	101,38
0,0450565	102,45
0,046095	103,415
0,0471325	104,167
0,0481689	104,812
0,0492042	105,351
0,0502384	105,783
0,0512716	106,108
0,0523037	106,326
0,0533347	106,436
0,0543647	106,545
0,0553936	106,655
0,0566269	106,678
0,0576535	106,788
0,058679	106,68
0,0597035	106,681
0,0607269	106,681

Show XY Plot

XY Plot

Curve Options

Type: Line

Step: None

☐ Spline ☐ Fill Area

☐ Log Y ☐ Log X

Curve Display

Color: Choose Color

Style: Solid

Width: 4

Vertical Bar Width: 10 %

Copy Data to Clipboard

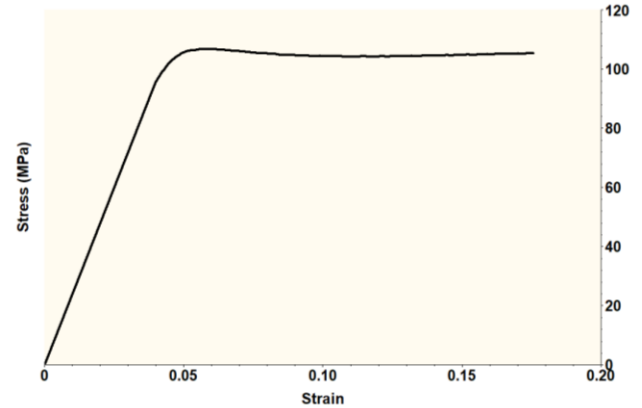
☐ Show Grid

Default Settings

Set As Default Settings

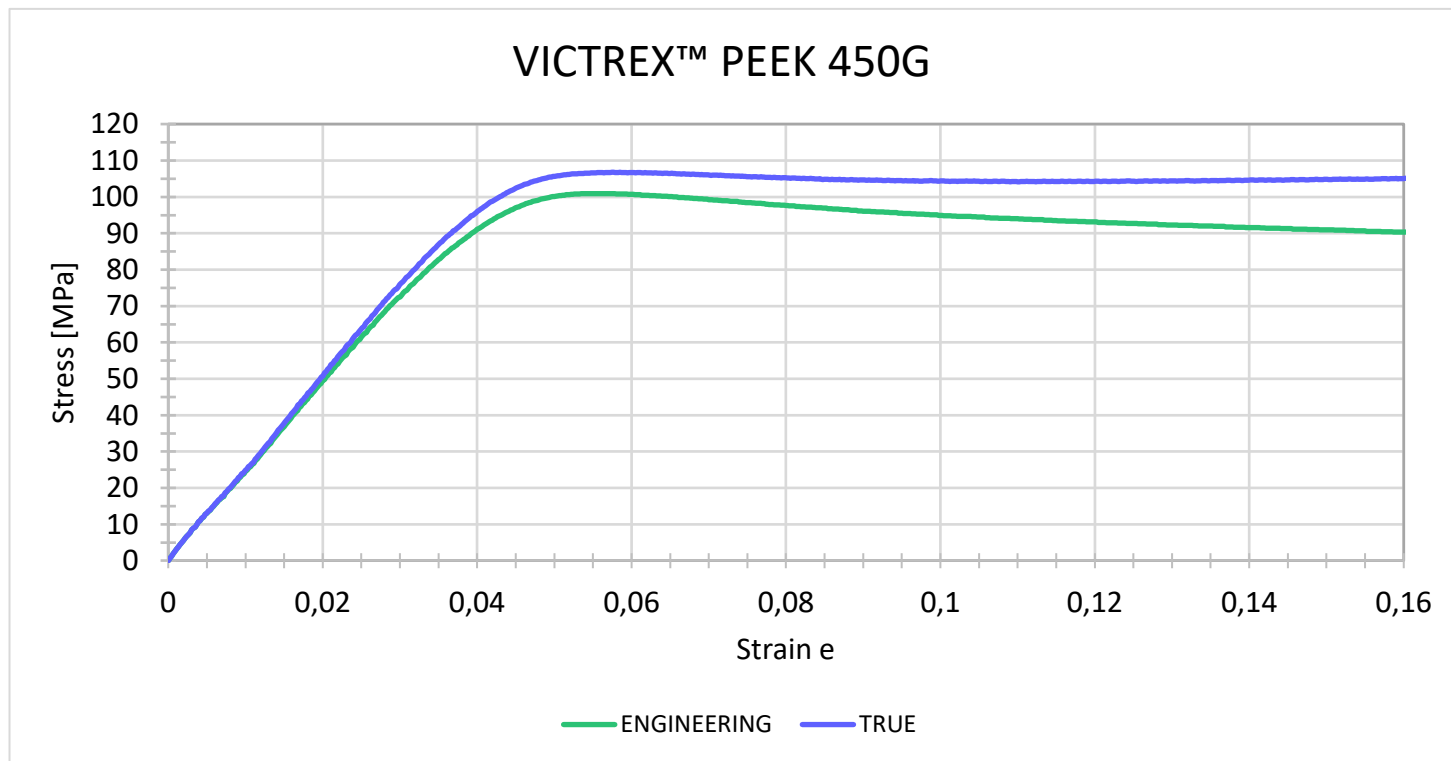
OK

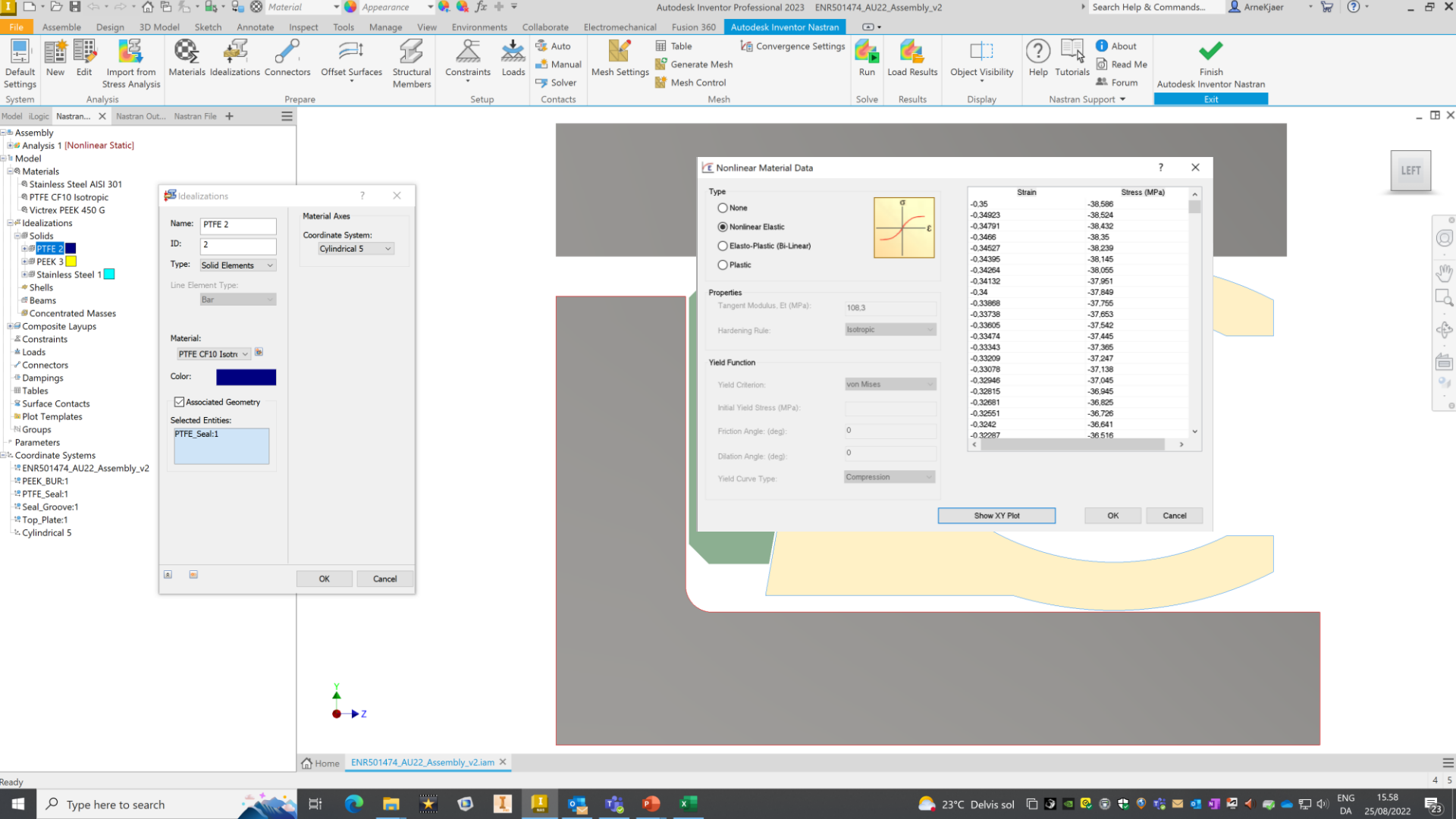
Stress (MPa) Vs Strain



Material data kindly provided by

Dr John Grasmeder, Chief Scientist, Victrex plc, Victrex Technology Centre

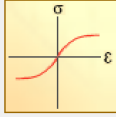




Nonlinear Material Data

Type

- ☐ None
☒ Nonlinear Elastic
☐ Elasto-Plastic (Bi-Linear)
☐ Plastic



Properties

Tangent Modulus, E_t (MPa):

108,3

Hardening Rule:

Isotropic

Yield Function

Yield Criterion:

von Mises

Initial Yield Stress (MPa):

Friction Angle: (deg):

0

Dilation Angle: (deg):

0

Yield Curve Type:

Compression

Strain	Stress (MPa)
-0,35	-38,586
-0,34923	-38,524
-0,34791	-38,432
-0,3466	-38,35
-0,34527	-38,239
-0,34395	-38,145
-0,34264	-38,055
-0,34132	-37,951
-0,34	-37,849
-0,33868	-37,755
-0,33738	-37,653
-0,33605	-37,542
-0,33474	-37,445
-0,33343	-37,365
-0,33209	-37,247
-0,33078	-37,138
-0,32946	-37,045
-0,32815	-36,945
-0,32681	-36,825
-0,32551	-36,726
-0,3242	-36,641
-0,32287	-36,516

Show XY Plot

OK

XY Plot

Curve Options

Type: Line

Step: None

☐ Spline ☐ Fill Area

☐ Log Y ☐ Log X

Curve Display

Color: Choose Color

Style: Solid

Width: 0

Vertical Bar Width: 10 %

Copy Data to Clipboard

☐ Show Grid

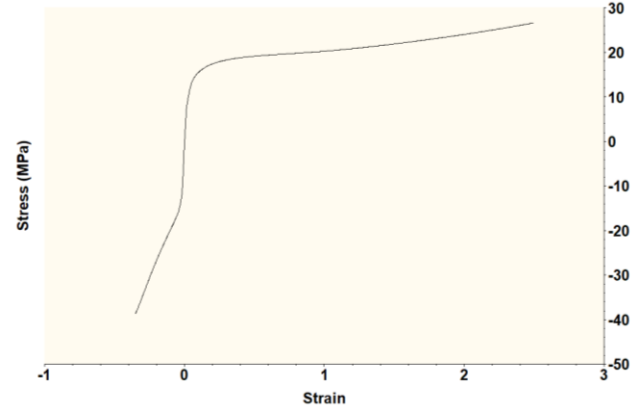
Default Settings

Set As Default Settings

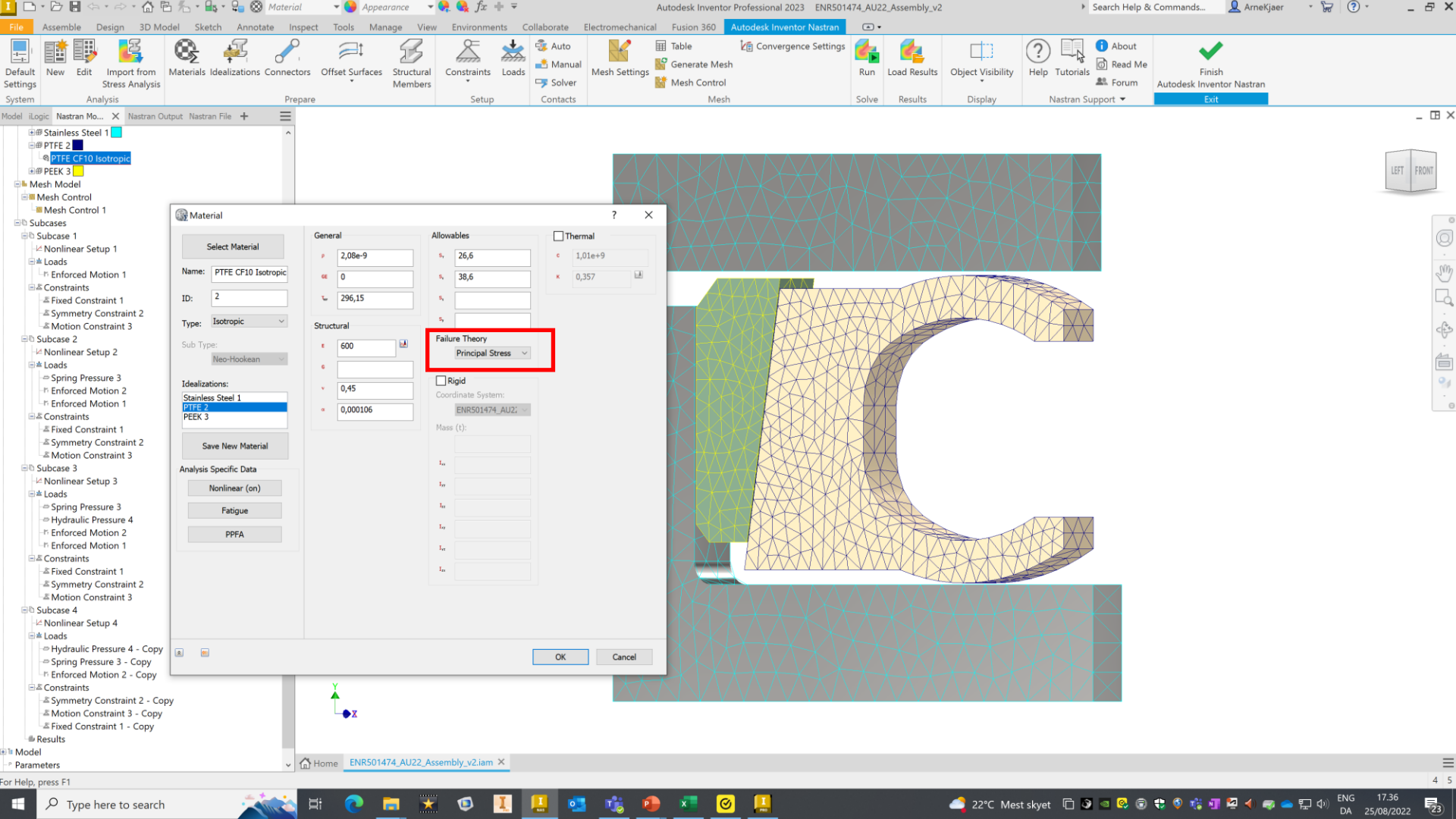
?

×

Stress (MPa) Vs Strain



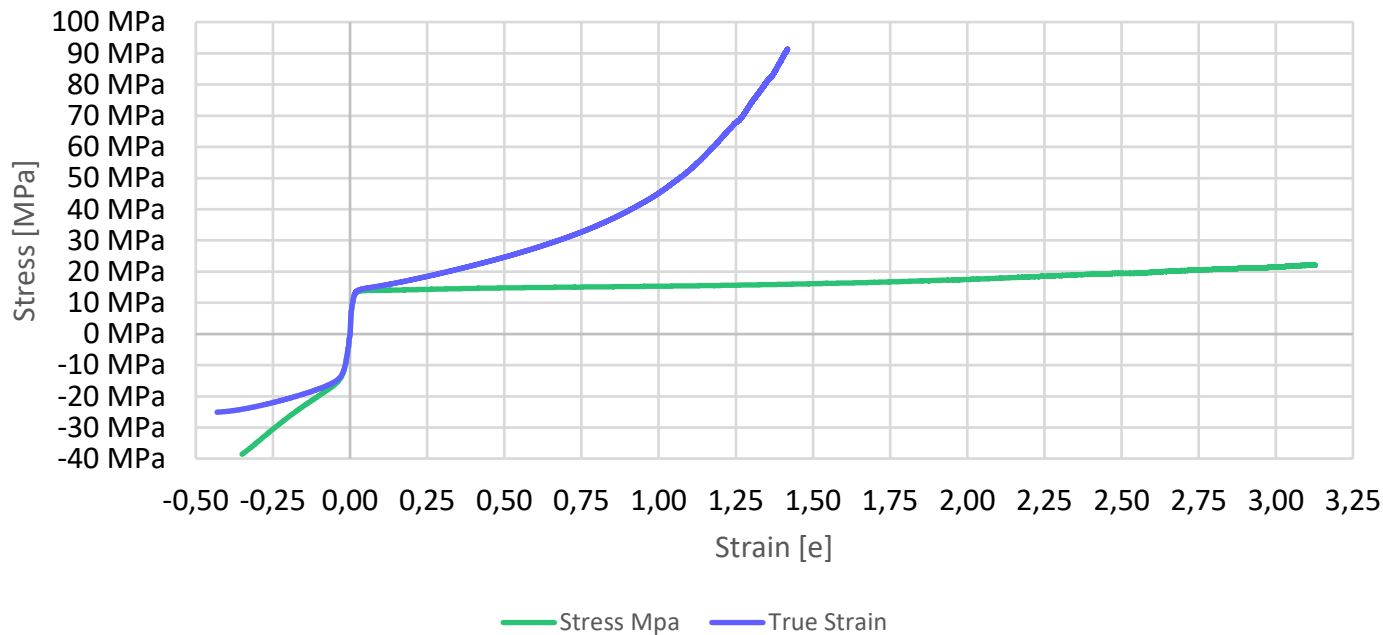
OK



Material data measured and engineered by

PTFE Engineering A/S

PTFE with CF Filler Stress - Strain Curve Eng



Setup of the Nastran 2023

The screenshot displays the Autodesk Inventor Professional 2023 interface for setting up a Nastran analysis. The left sidebar shows the 'Idealizations' tree, which is expanded to show the 'Solids' section. The 'Solids' section lists three solid types: 'Steel Solid 1' (Stainless Steel), 'PTFE Solid 2' (PTFE CF10 Isotropic), and 'PEEK Solid 3' (Victrex PEEK 450 G). The main area shows a 3D model of a mechanical part with a red box highlighting the 'Idealizations' tree. A red box on the right side of the image highlights the 'Idealizations' tree structure, showing the hierarchy: Idealizations > Solids > Steel Solid 1 > Stainless Steel, PTFE Solid 2 > PTFE CF10 Isotropic, and PEEK Solid 3 > Victrex PEEK 450 G.

Idealizations

- Solids**
 - Steel Solid 1
 - Stainless Steel
 - PTFE Solid 2
 - PTFE CF10 Isotropic
 - PEEK Solid 3
 - Victrex PEEK 450 G

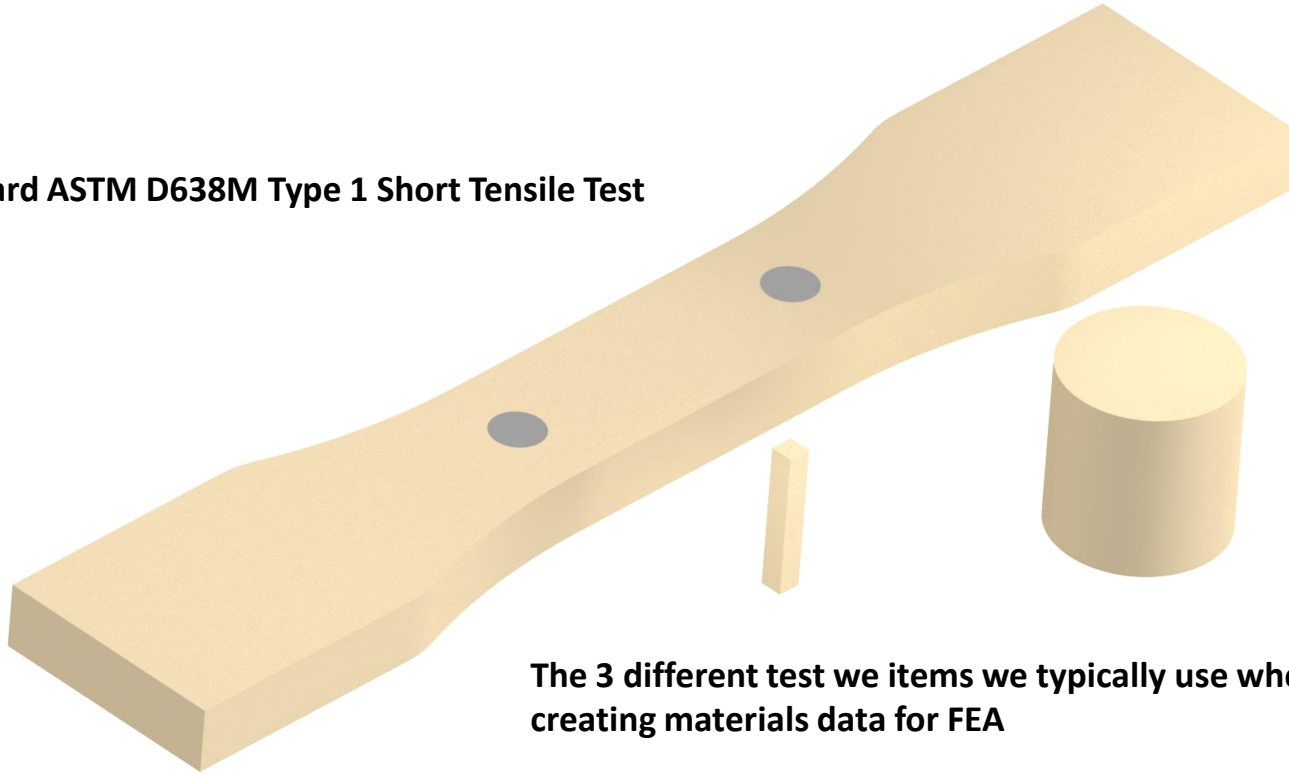
Your Own Material data

PTFE Material Data

- Basically, we now have data to run a simple FEA.
- With a few additional information's we are actually ready to go with a not too bad first simulation.
- You will also need the following information's.
 - Mass density (Specific Gravity)
 - Reference Temperature
 - Elastic modulus (Tensions / Compression)
 - Poisson's Ratio
 - Tensile Limit
 - Compressive Limit
 - Yield Limit (Initial Yield Stress)
 - Tangent Modulus
 - Thermal Expansion Coefficient

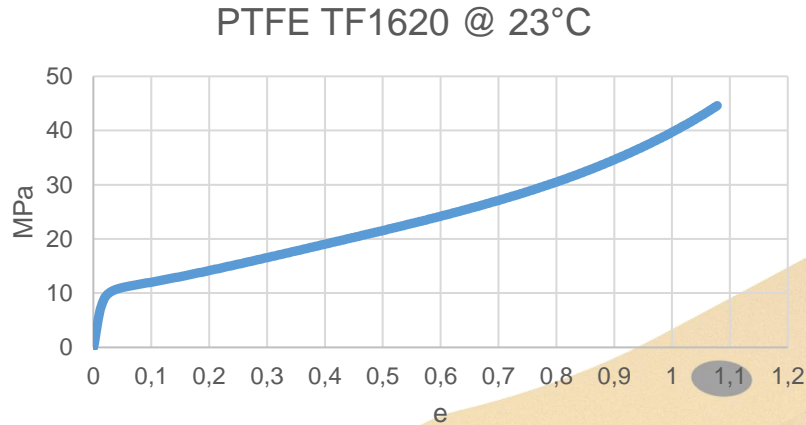
PTFE Material Data

Standard ASTM D638M Type 1 Short Tensile Test



The 3 different test we items we typically use when we start creating materials data for FEA

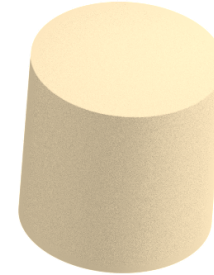
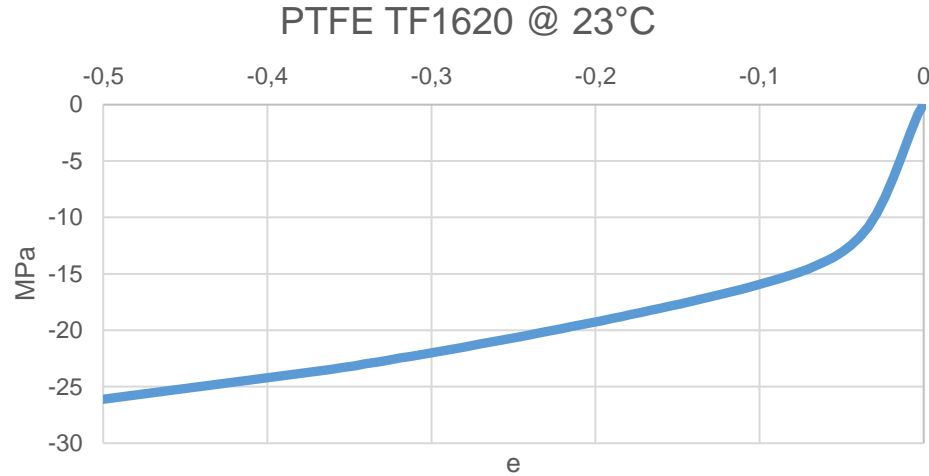
PTFE Material Data



Tensile Test Bar according to ASTM D638M Type 1 - Short

The normal length of ATSM D638M is 175 mm and we use only 100 mm. We have a gauge length of 25 mm and we typically test at a strain rate of $0,01 s^{-1}$

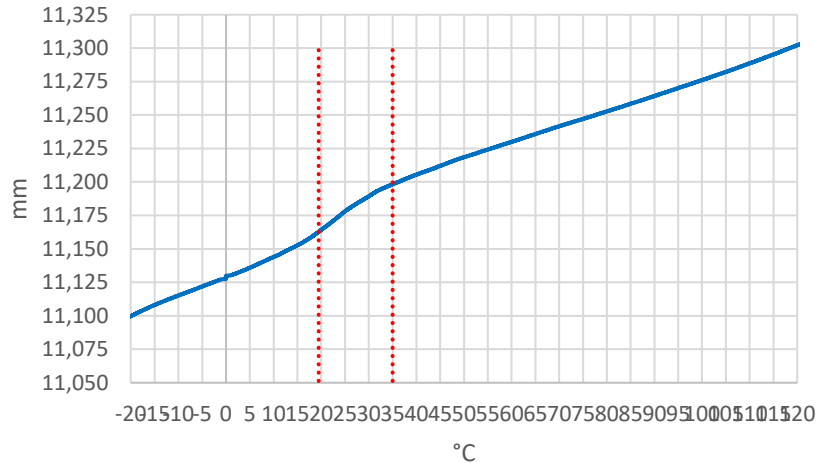
PTFE Material Data



Compression Test Billet
Ø12,7 mm x 12,7 mm

PTFE Material Data

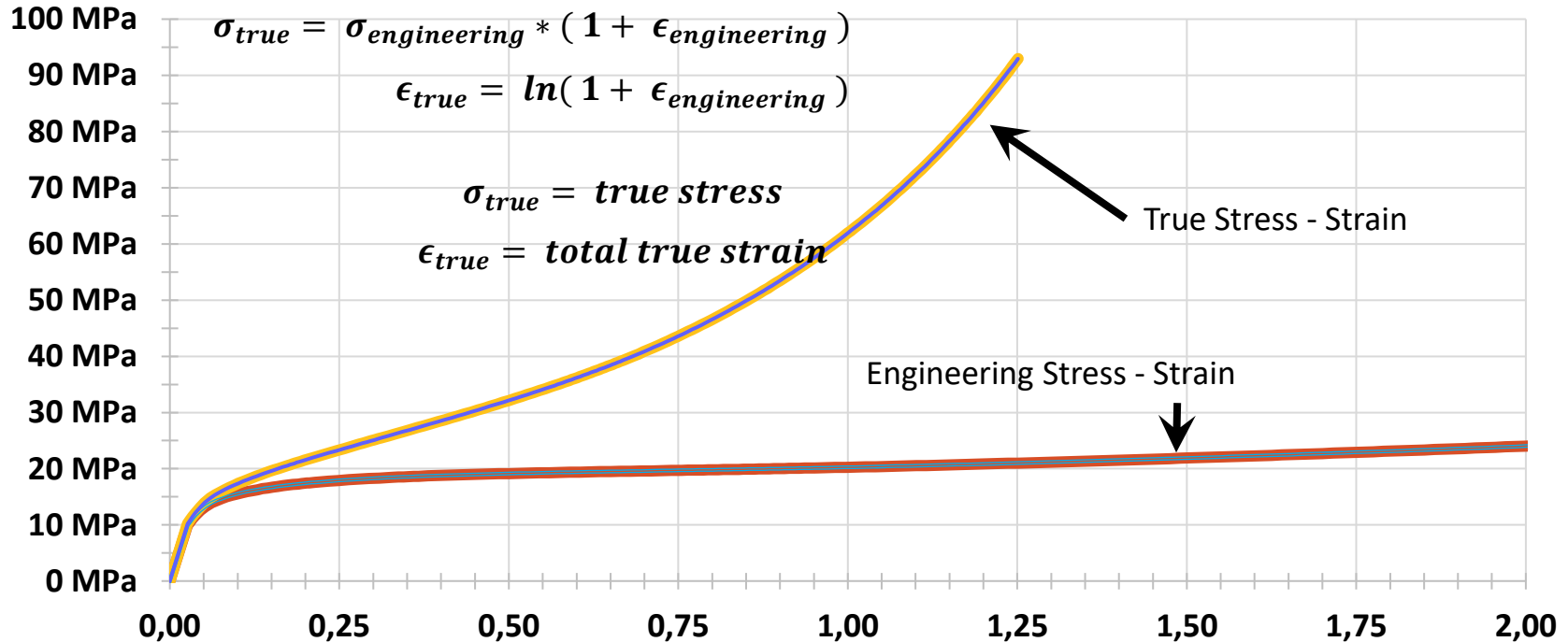
Thermal Expansion PTFE Engineering A/S



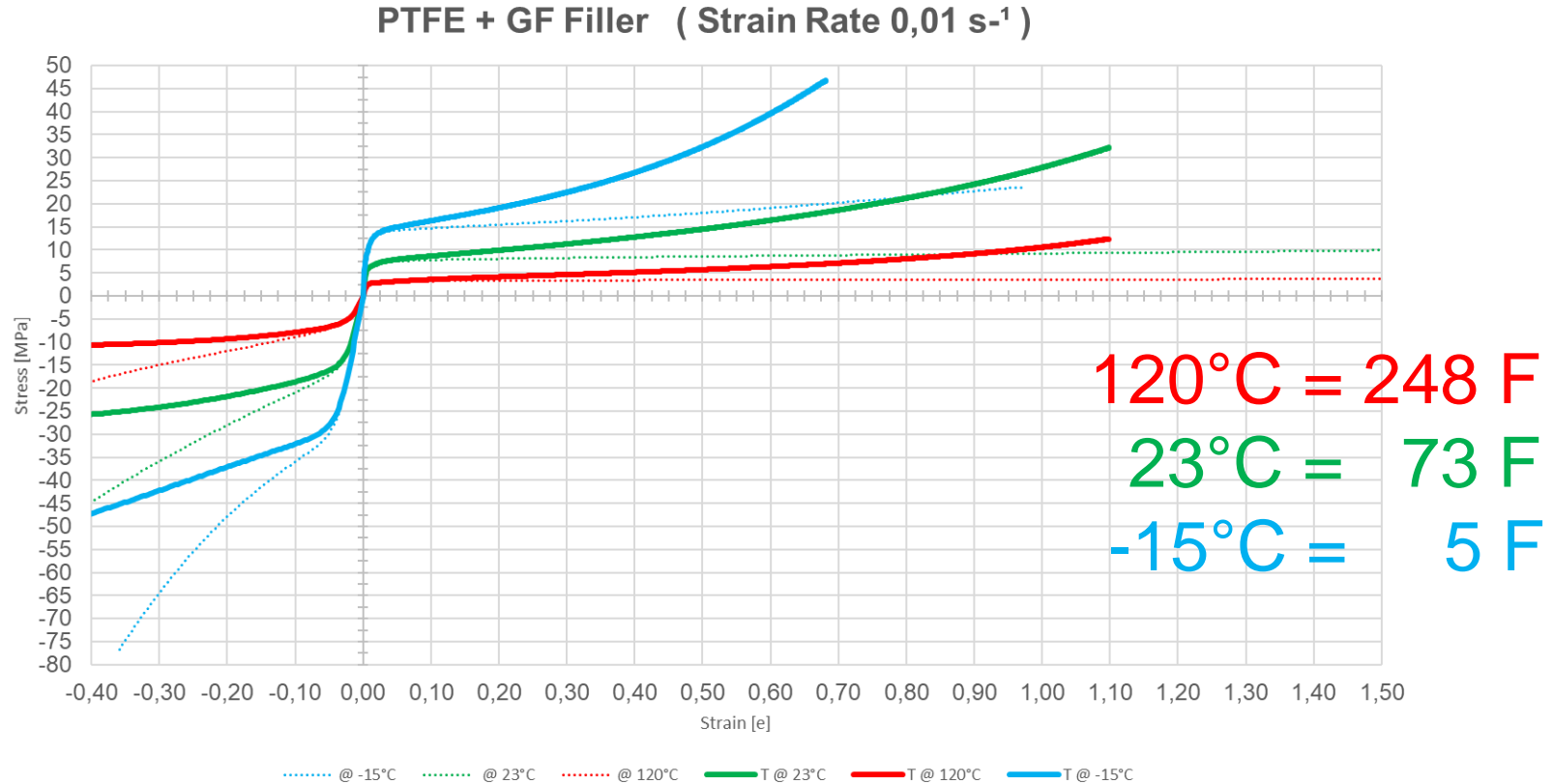
Thermal Expansion Test Bar
1,75 mm x 1,75 mm x 11,0 mm

Engineering stress to True stress

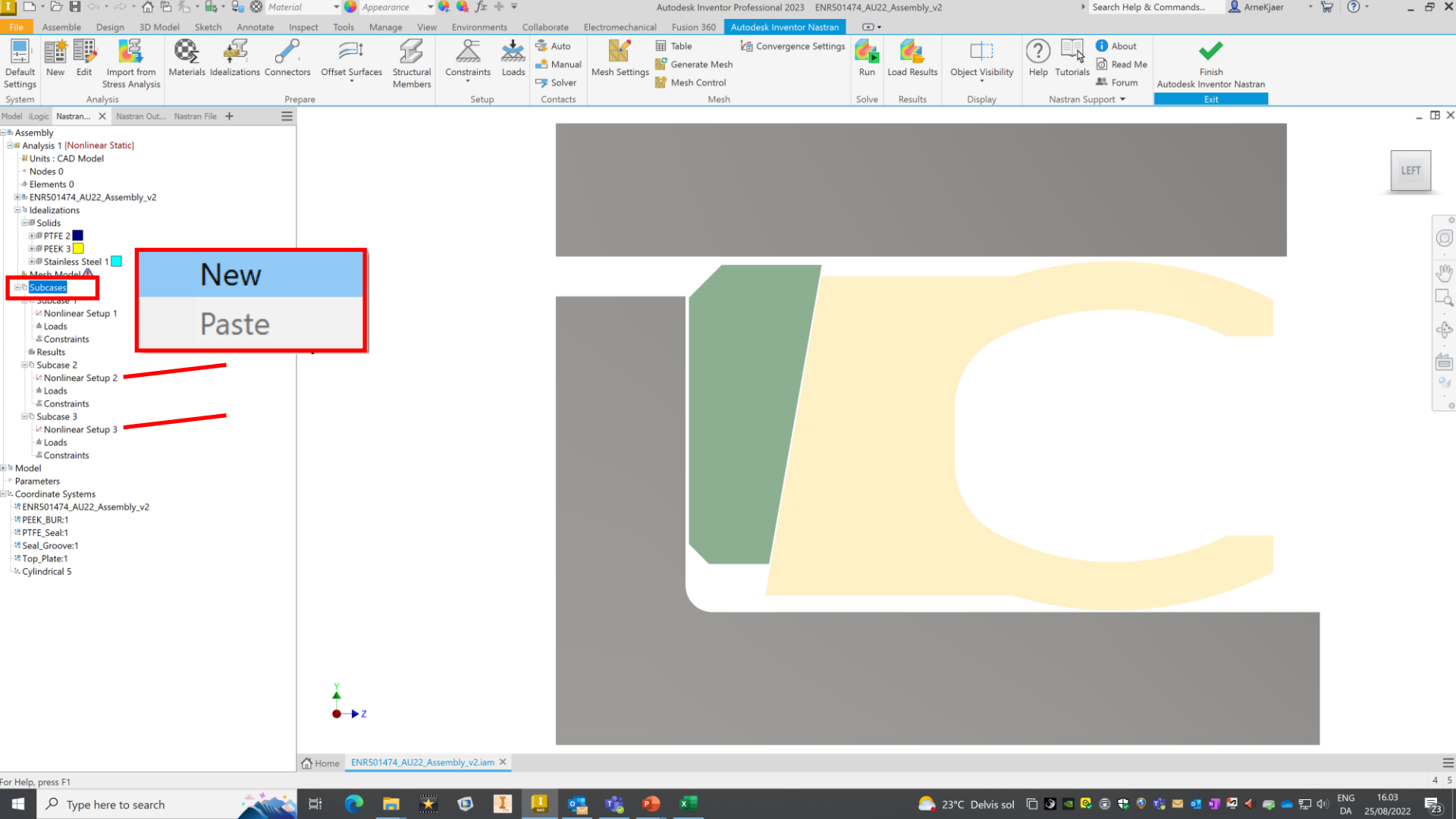
Tensile Test PTFE CF10 03A Eng / True Stress – Strain [MPa]

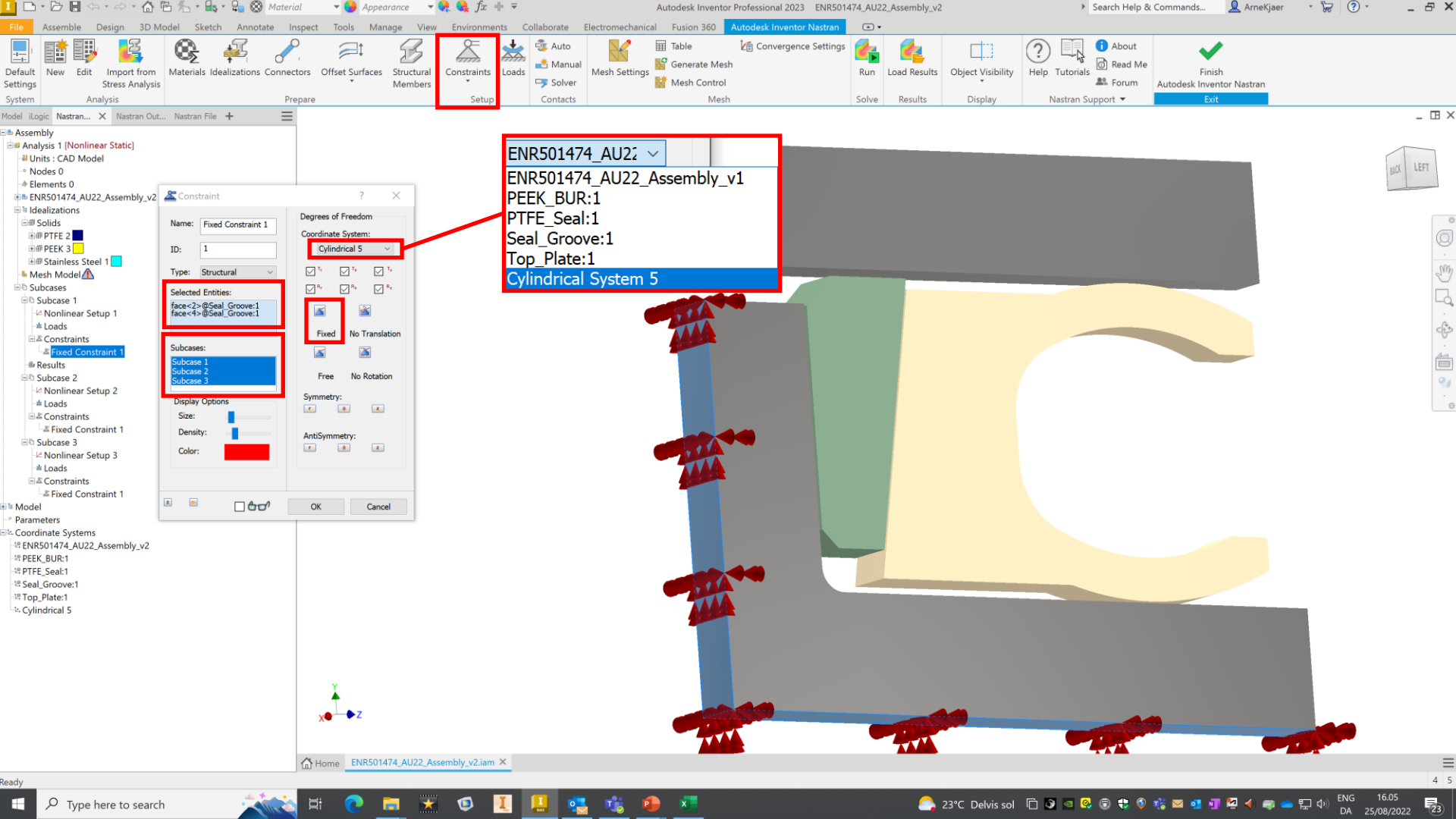


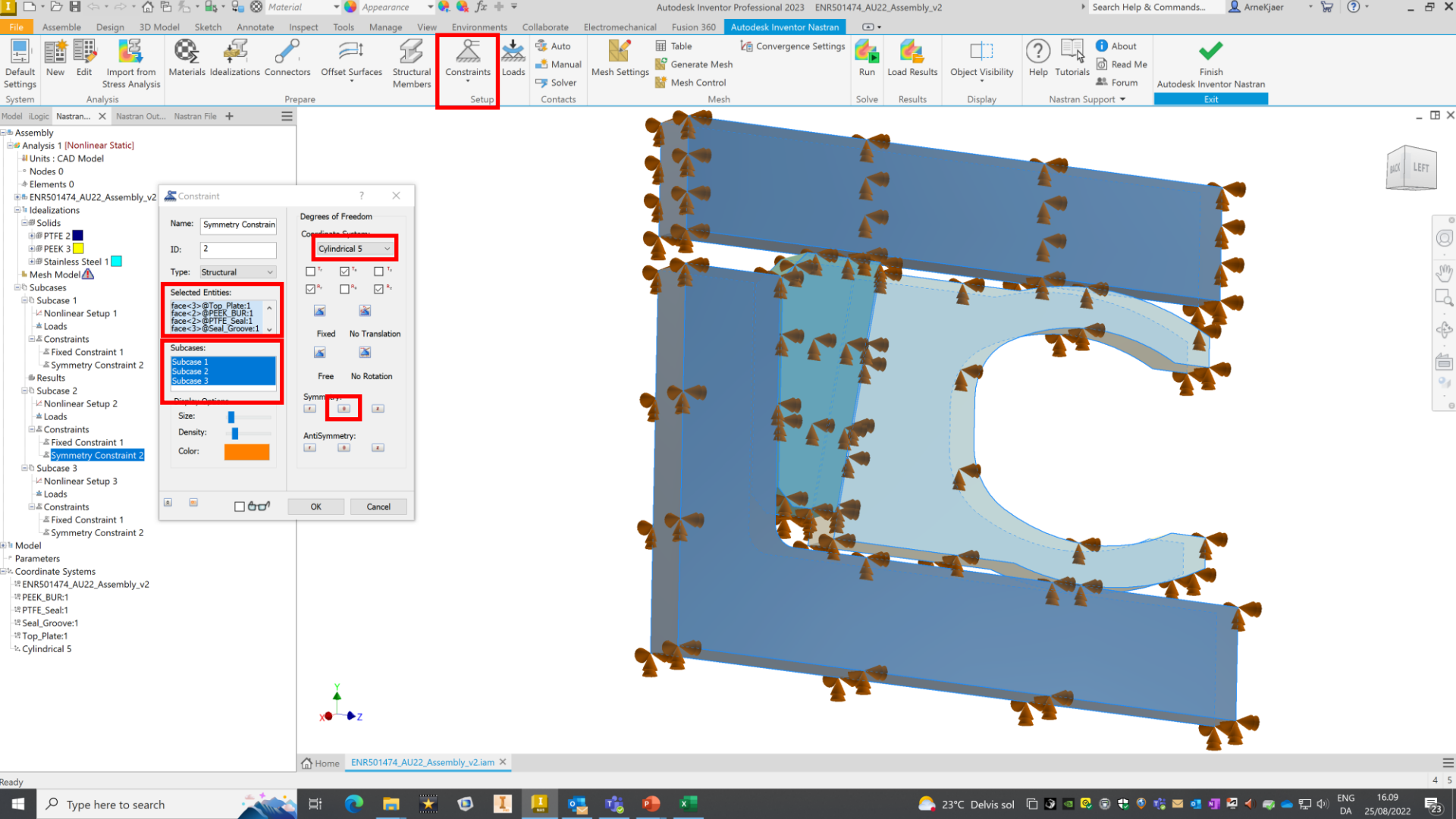
PTFE Material Data

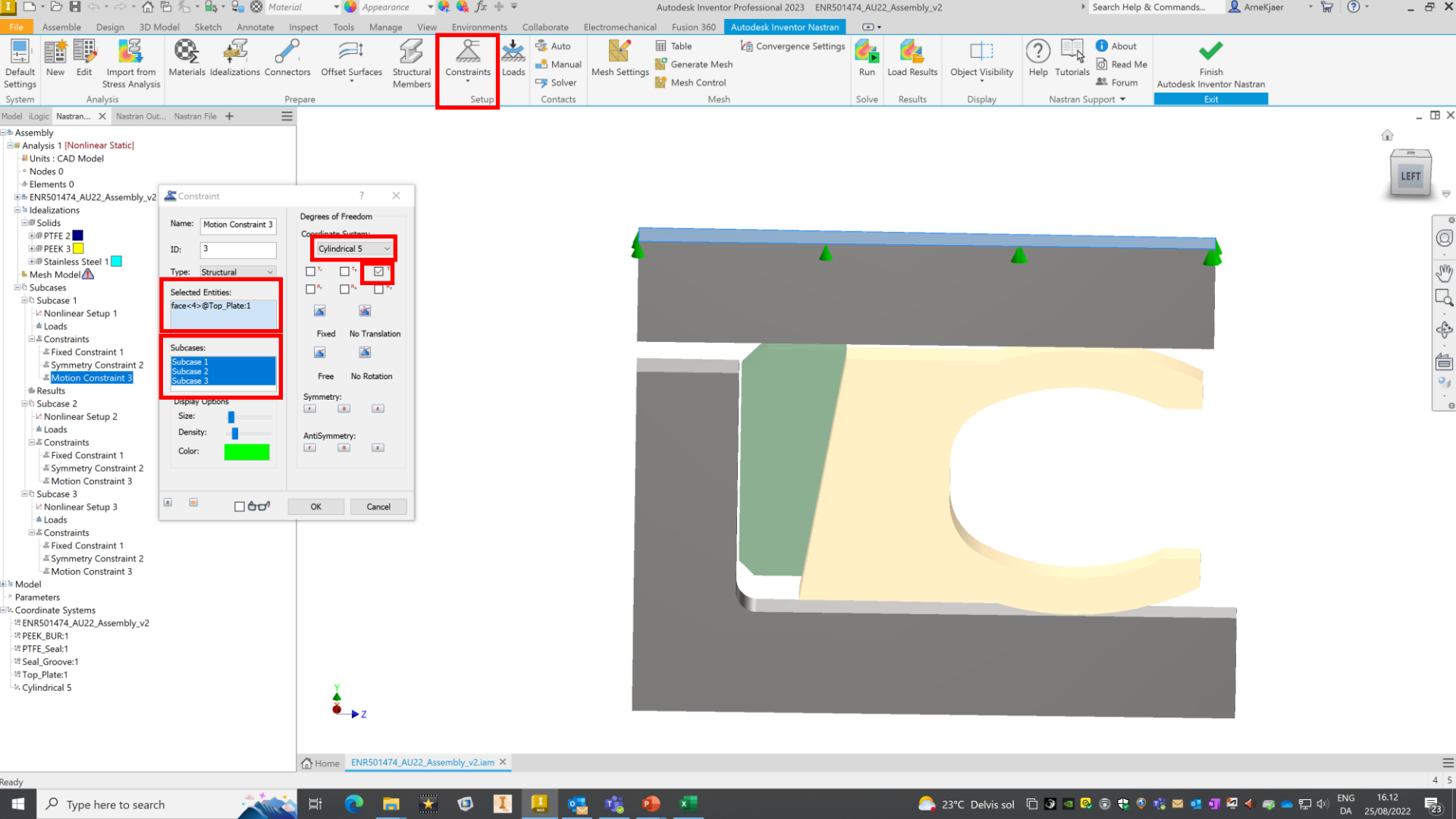


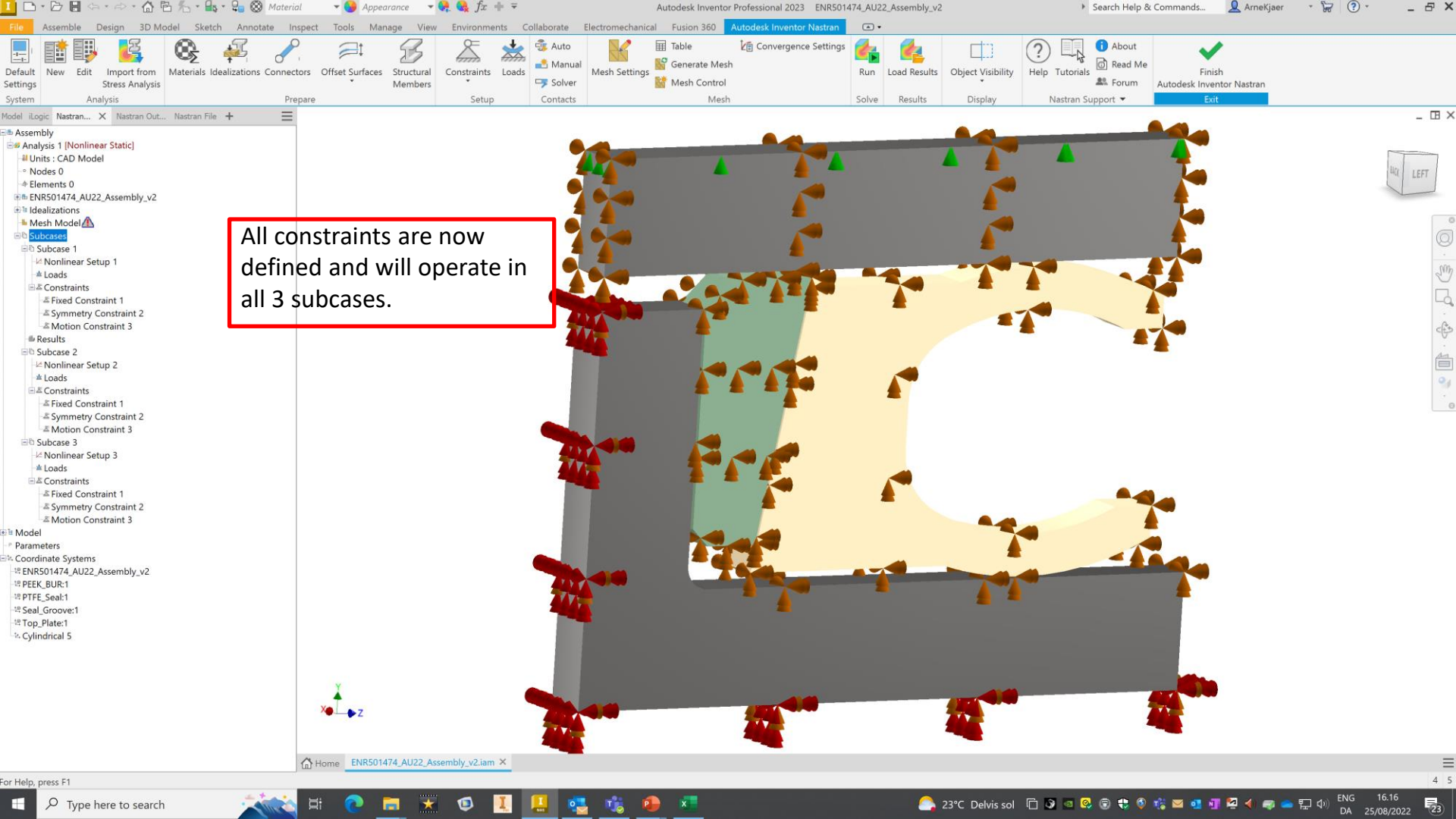
Subcase Constraints



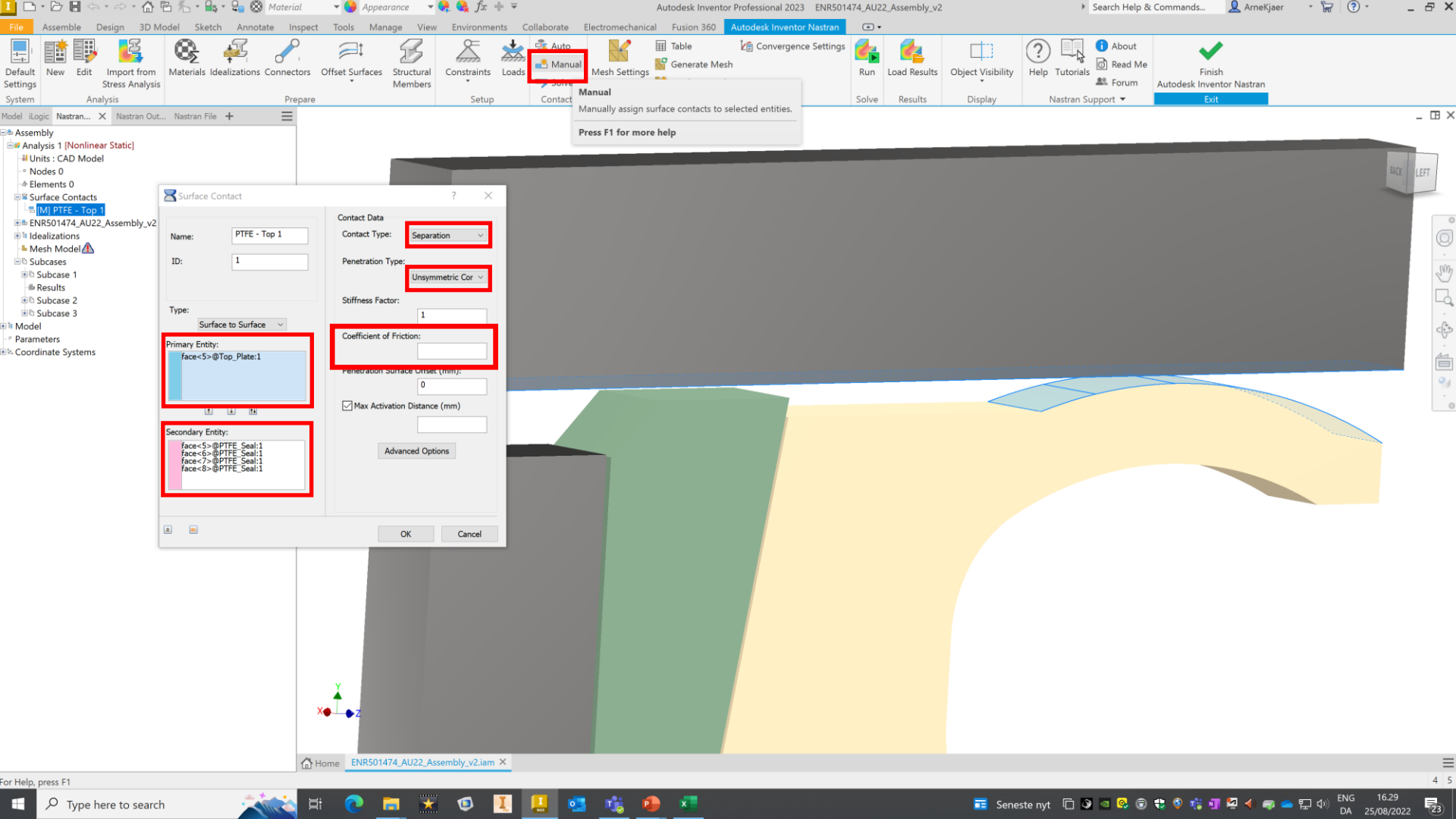


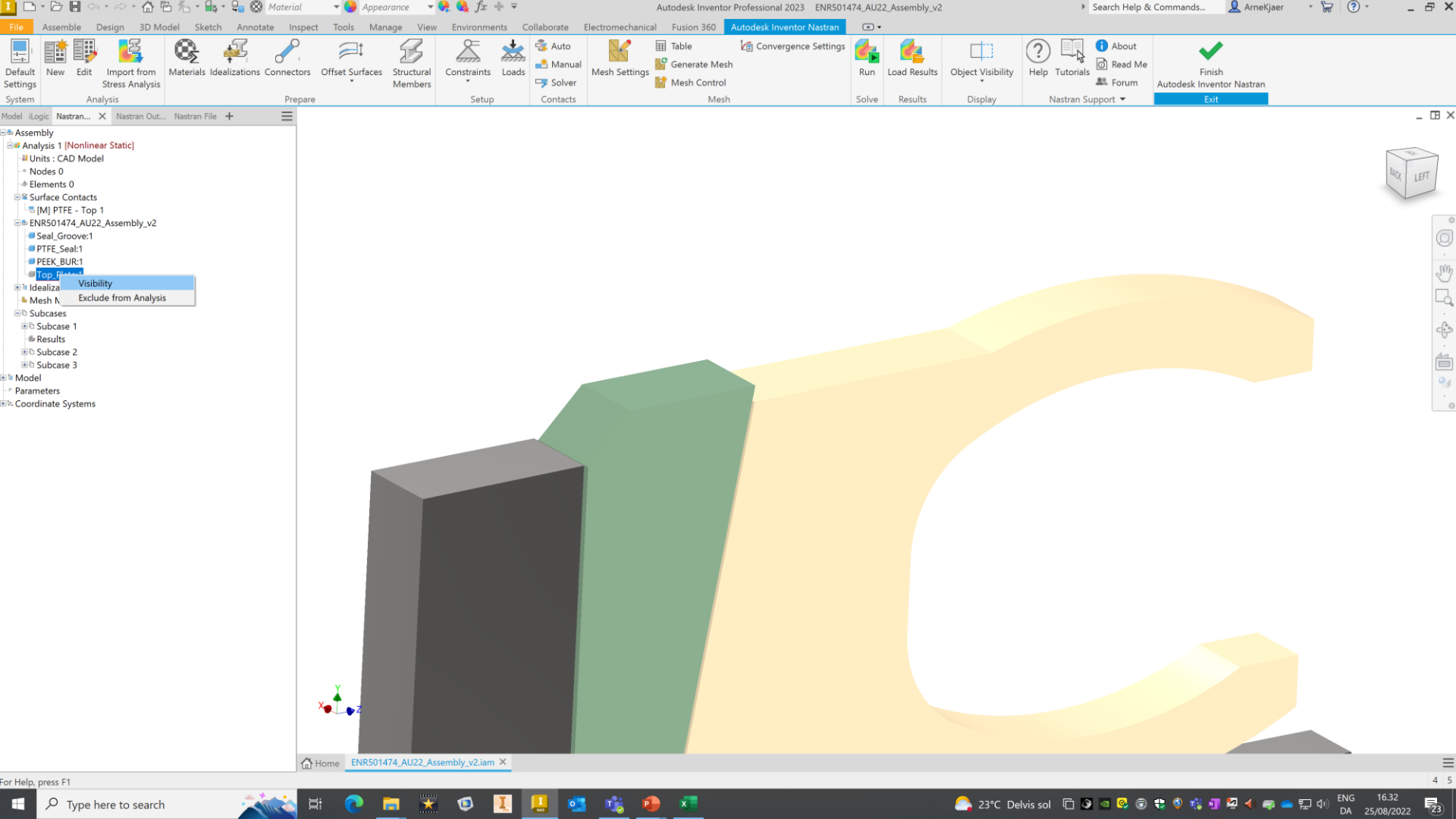


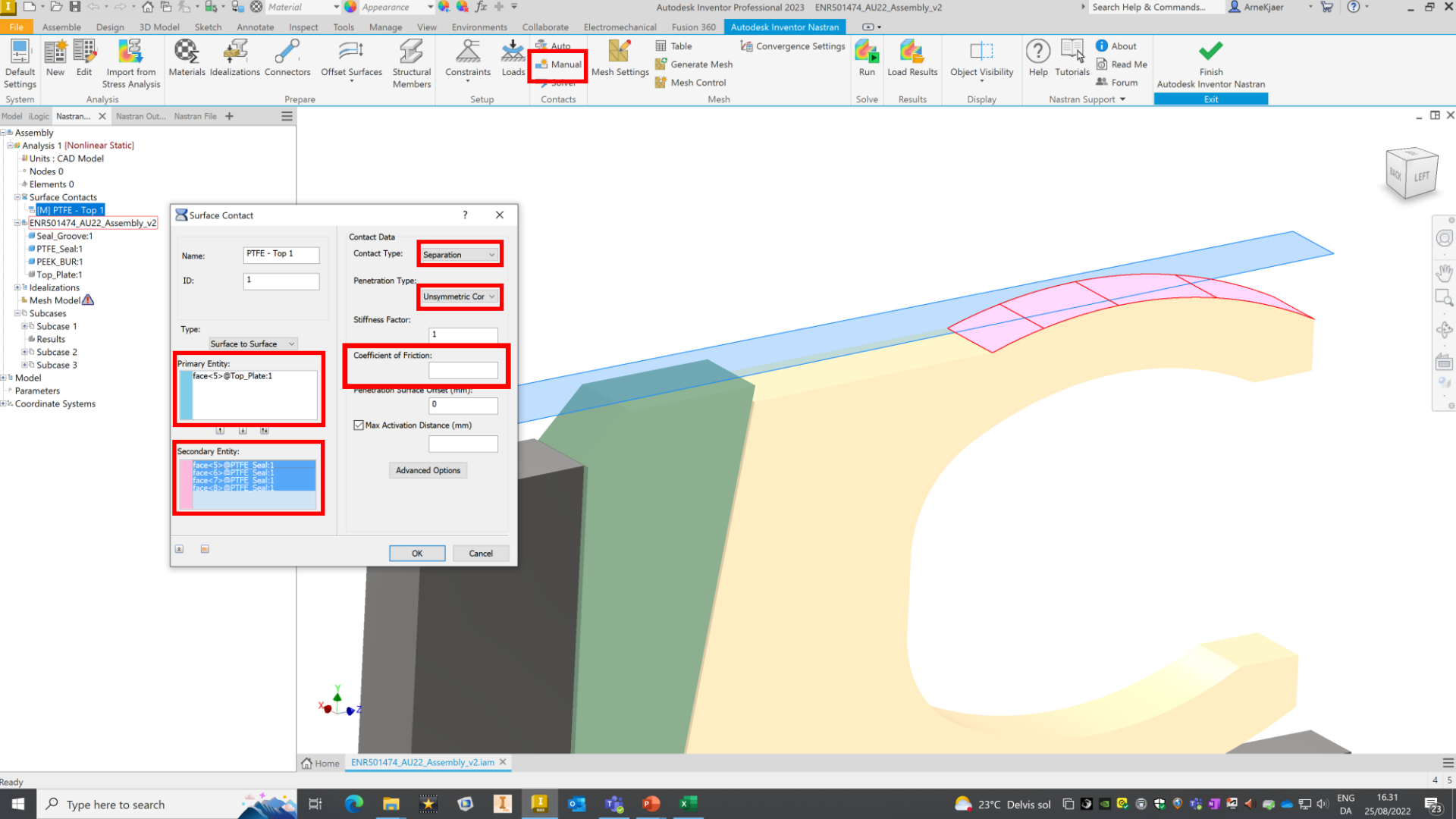


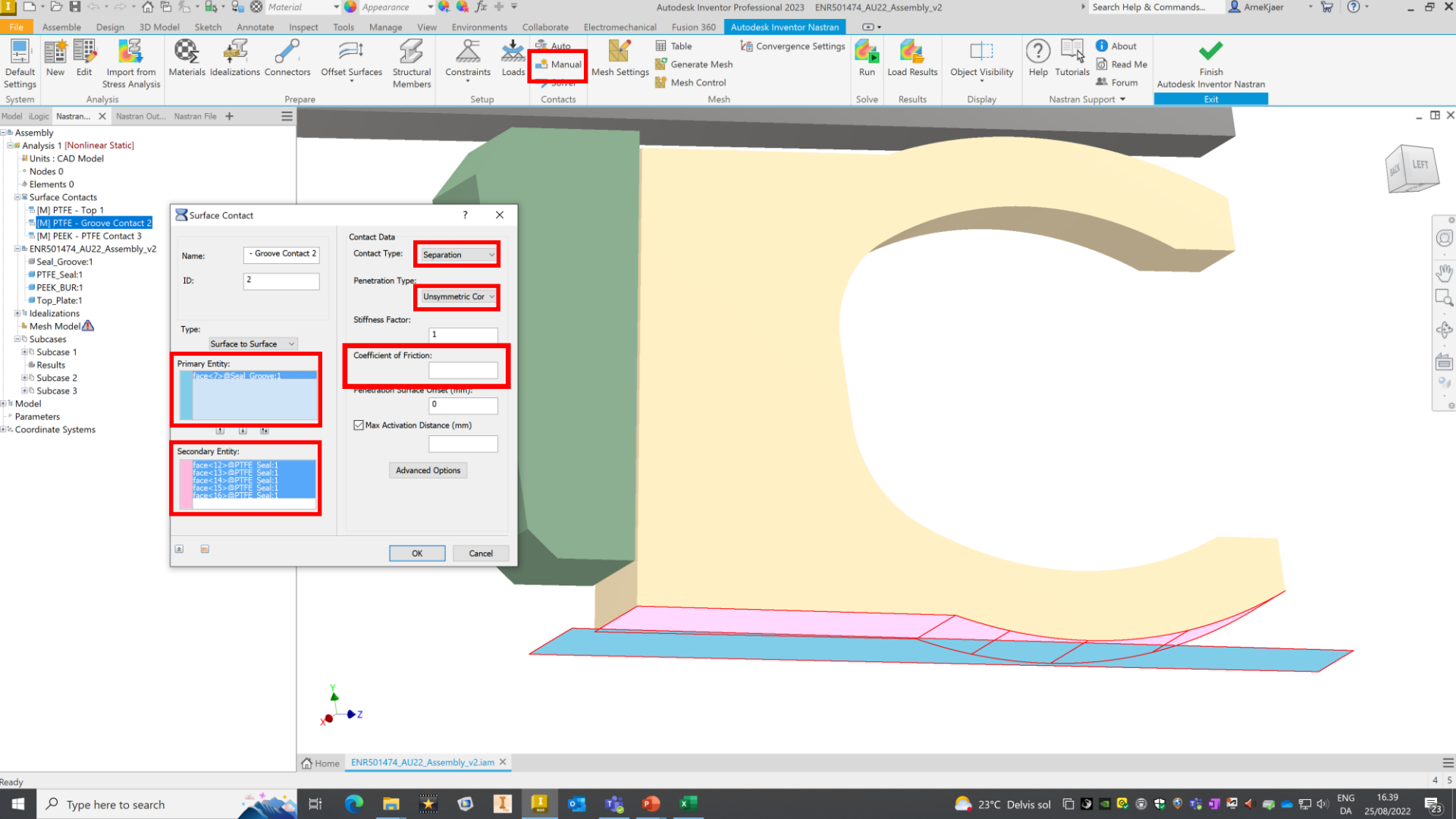


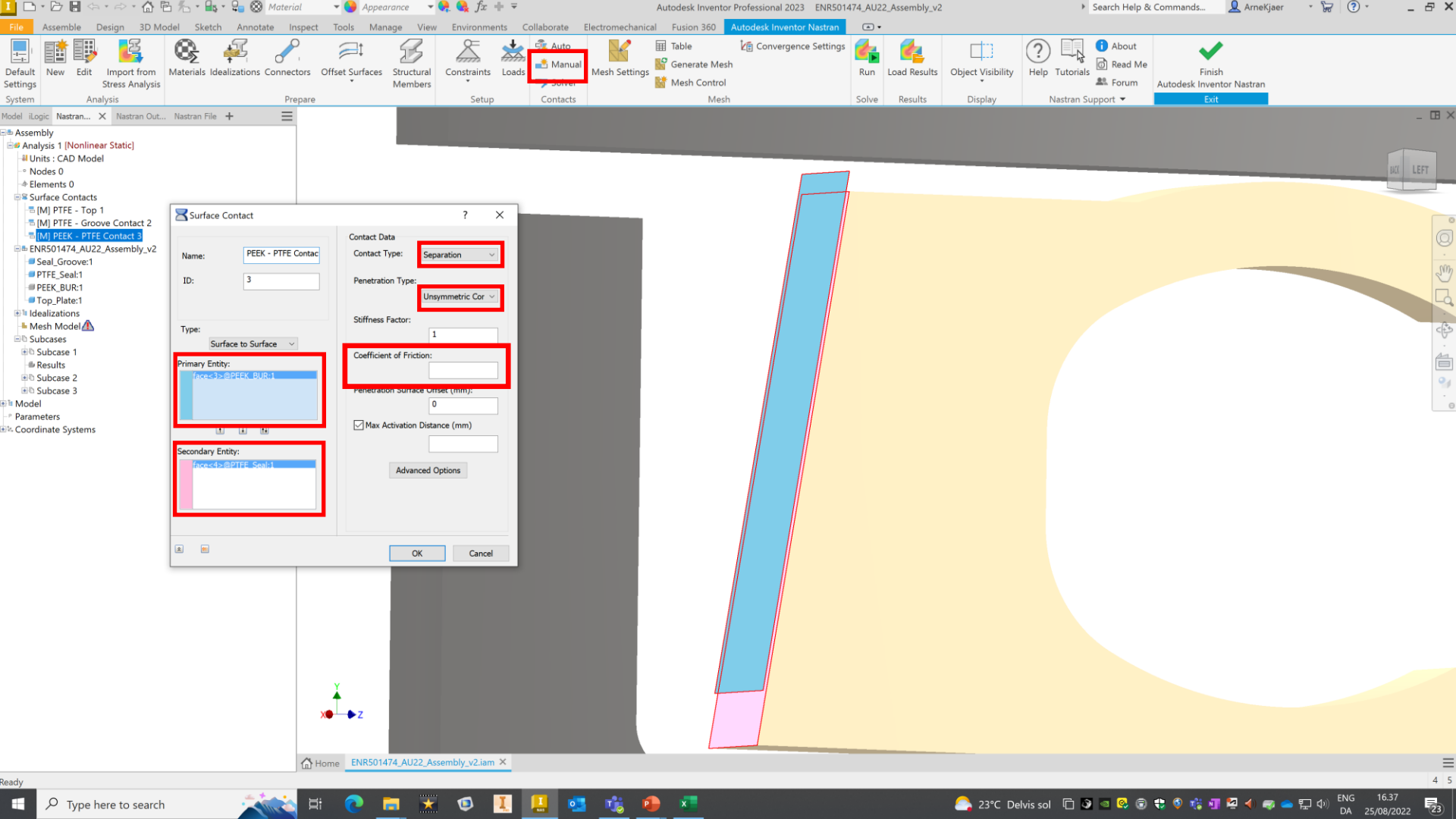
Contacts

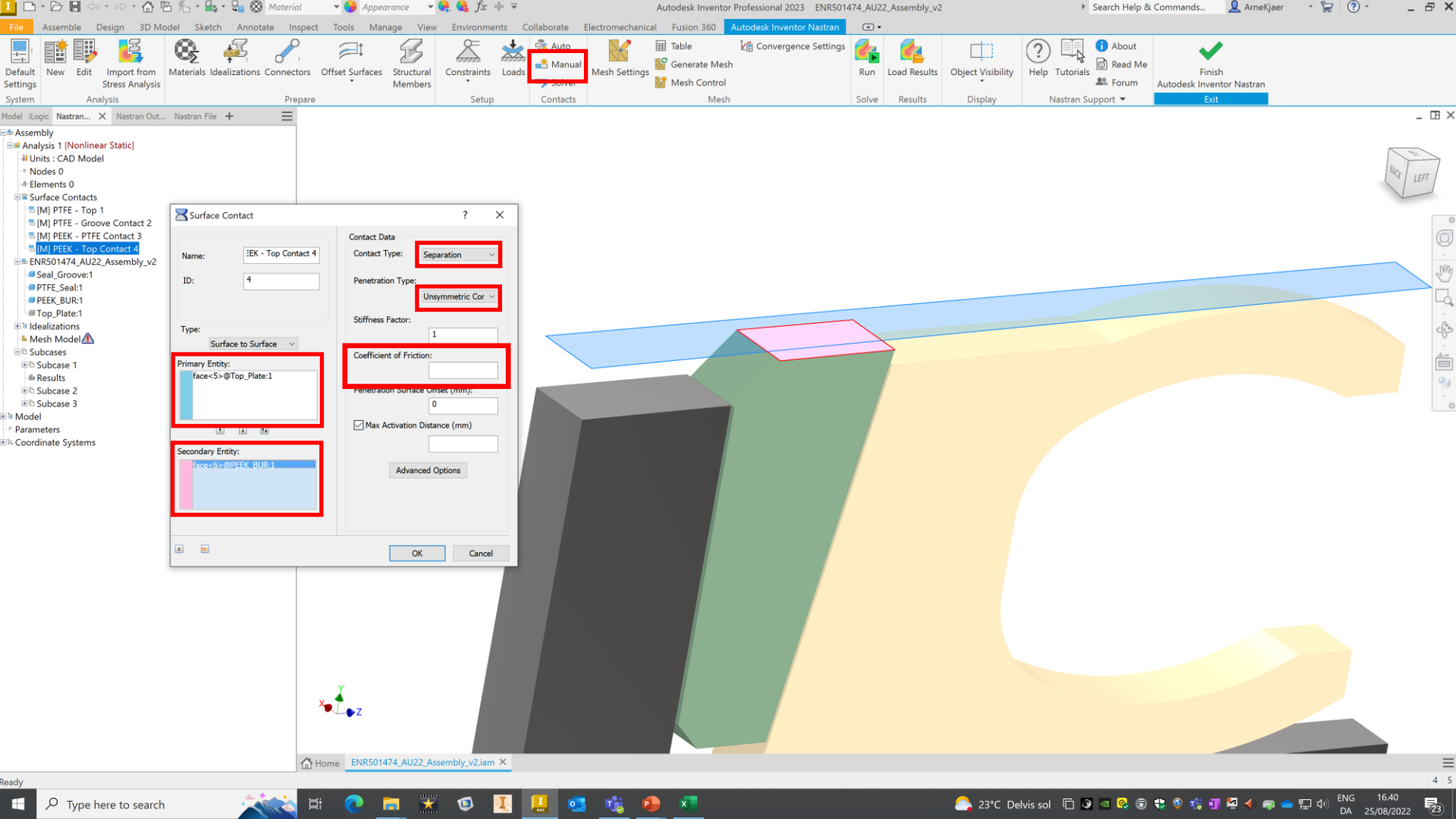












Surface Contact

Name:

ID:

Type:

Primary Entity:

Secondary Entity:

Contact Data

Contact Type:

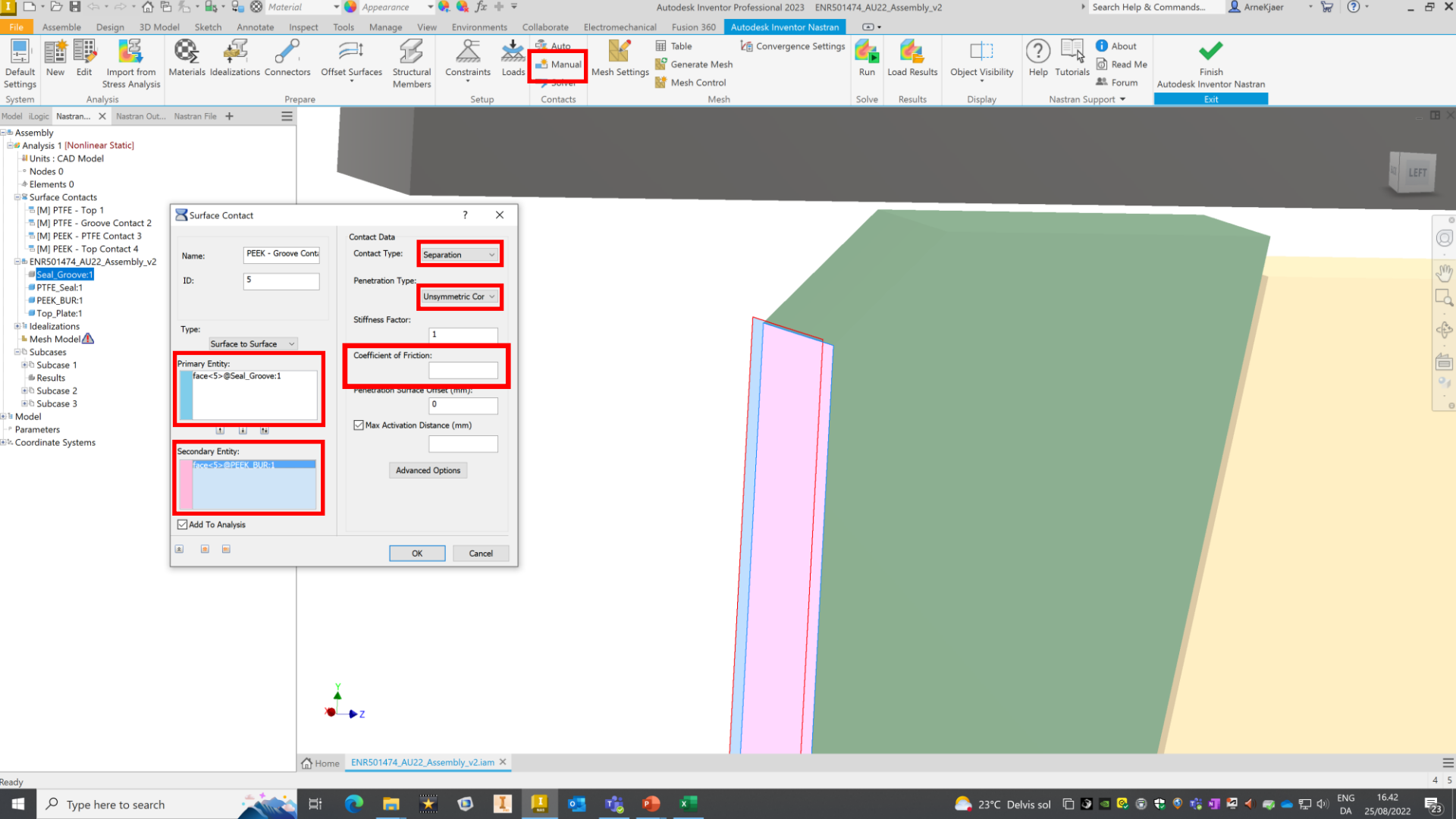
Penetration Type:

Stiffness Factor:

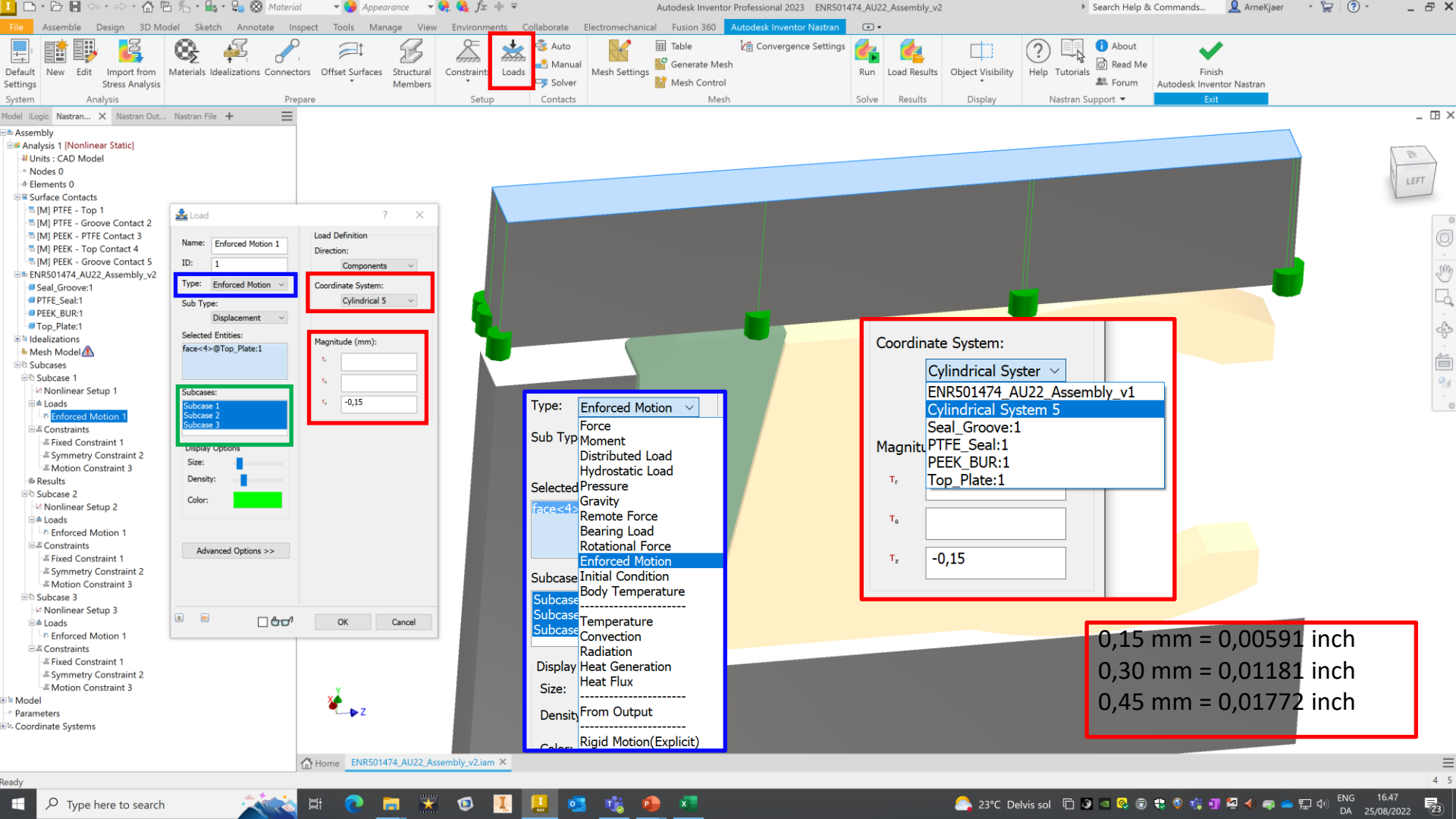
Coefficient of Friction:

Penetration surface offset (mm):

☒ Max Activation Distance (mm)



Loads



Load

Name: Enforced Motion 1
ID: 1

Type: Enforced Motion
Sub Type: Displacement

Selected Entities:
Face<4>@Top_Plate:1

Subcases:
Subcase 1
Subcase 2
Subcase 3

Display Options
Size:
Density:
Color:

Advanced Options >>

OK Cancel

Load Definition

Direction: Components

Coordinate System: Cylindrical 5

Magnitude (mm):
T_x
T_y
T_z -0,15

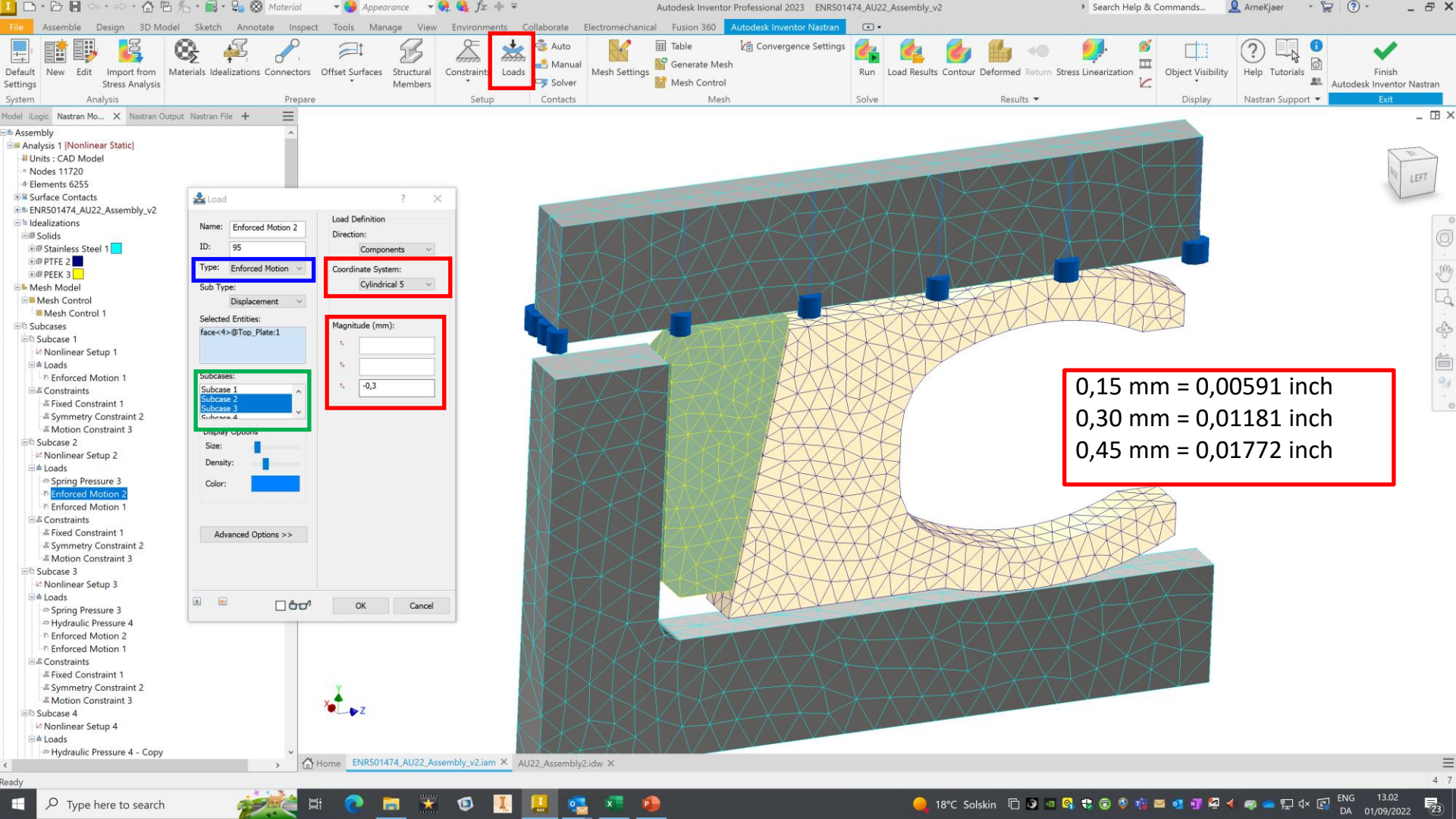
Type: Enforced Motion
Sub Type: Moment
Selected: face<4>
Subcase: Subcase 1
Subcase: Subcase 2
Subcase: Subcase 3
Display: Heat Generation
Size: Heat Flux
Density: From Output
Color: Rigid Motion(Explicit)

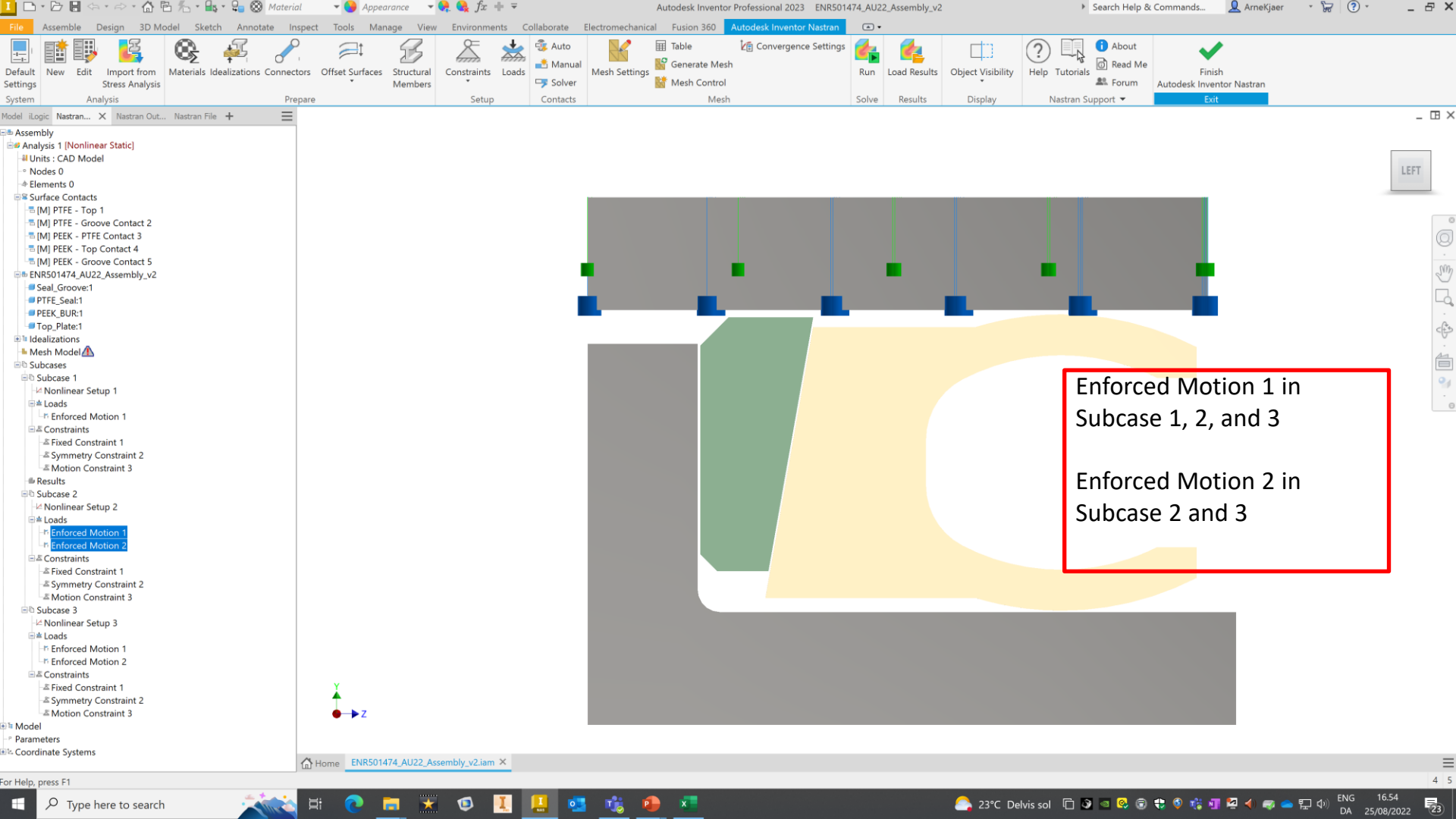
Coordinate System:

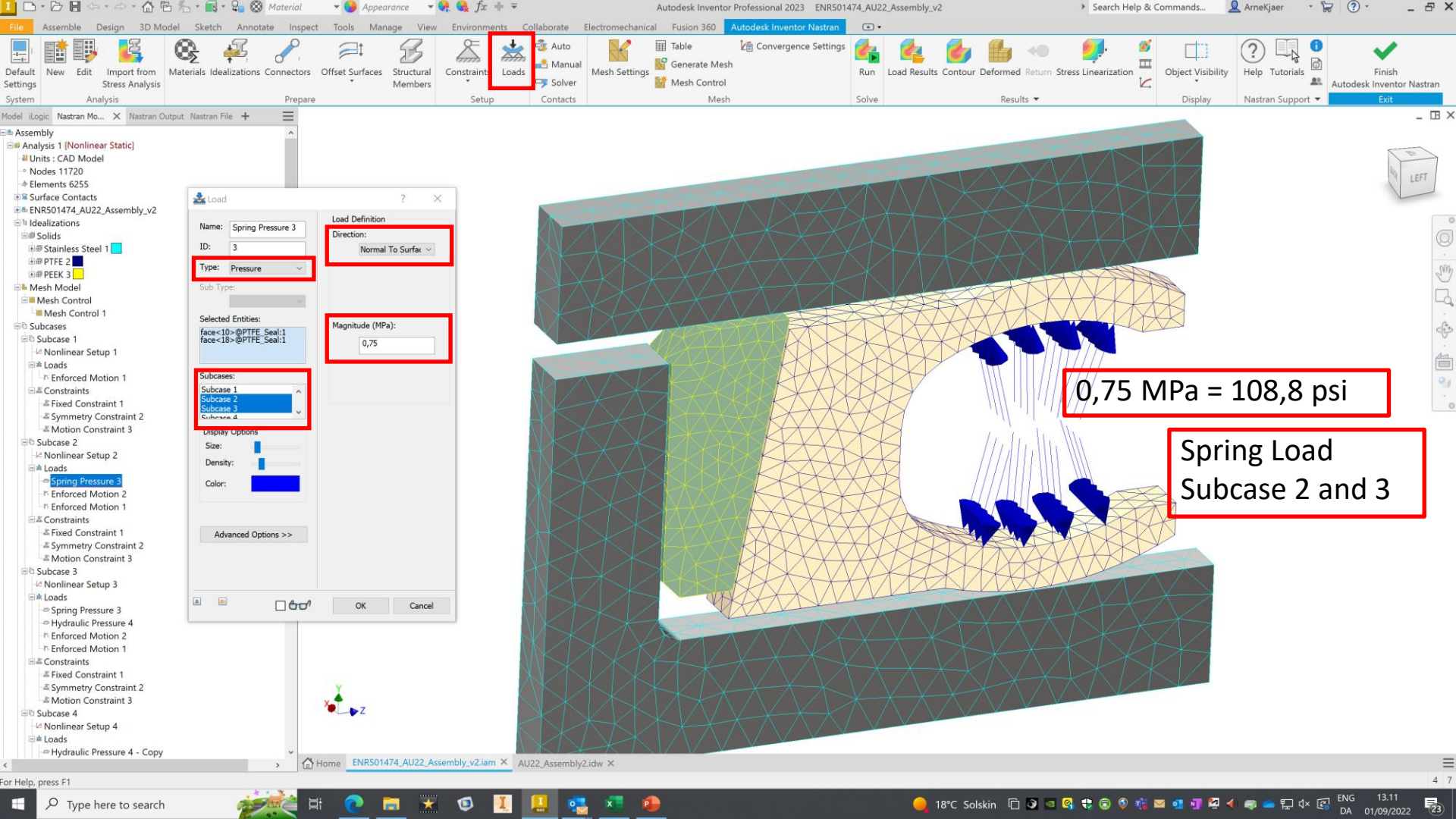
Cylindrical System
ENR501474_AU22_Assembly_v1
Cylindrical System 5
Seal Groove:1
PTFE_Seal:1
PEEK_BUR:1
Top_Plate:1

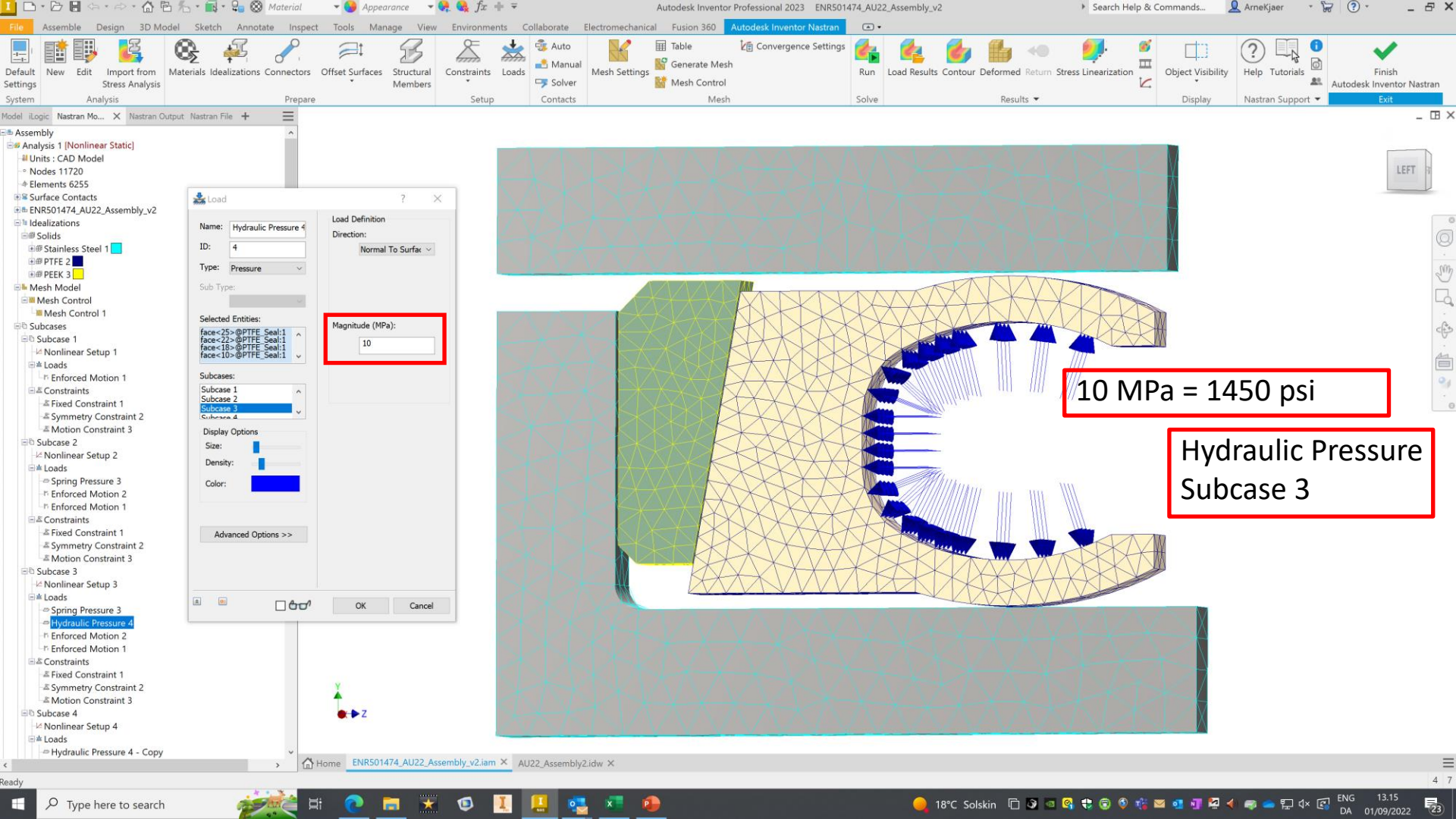
Magnitude:
T_x
T_y
T_z -0,15

0,15 mm = 0,00591 inch
0,30 mm = 0,01181 inch
0,45 mm = 0,01772 inch

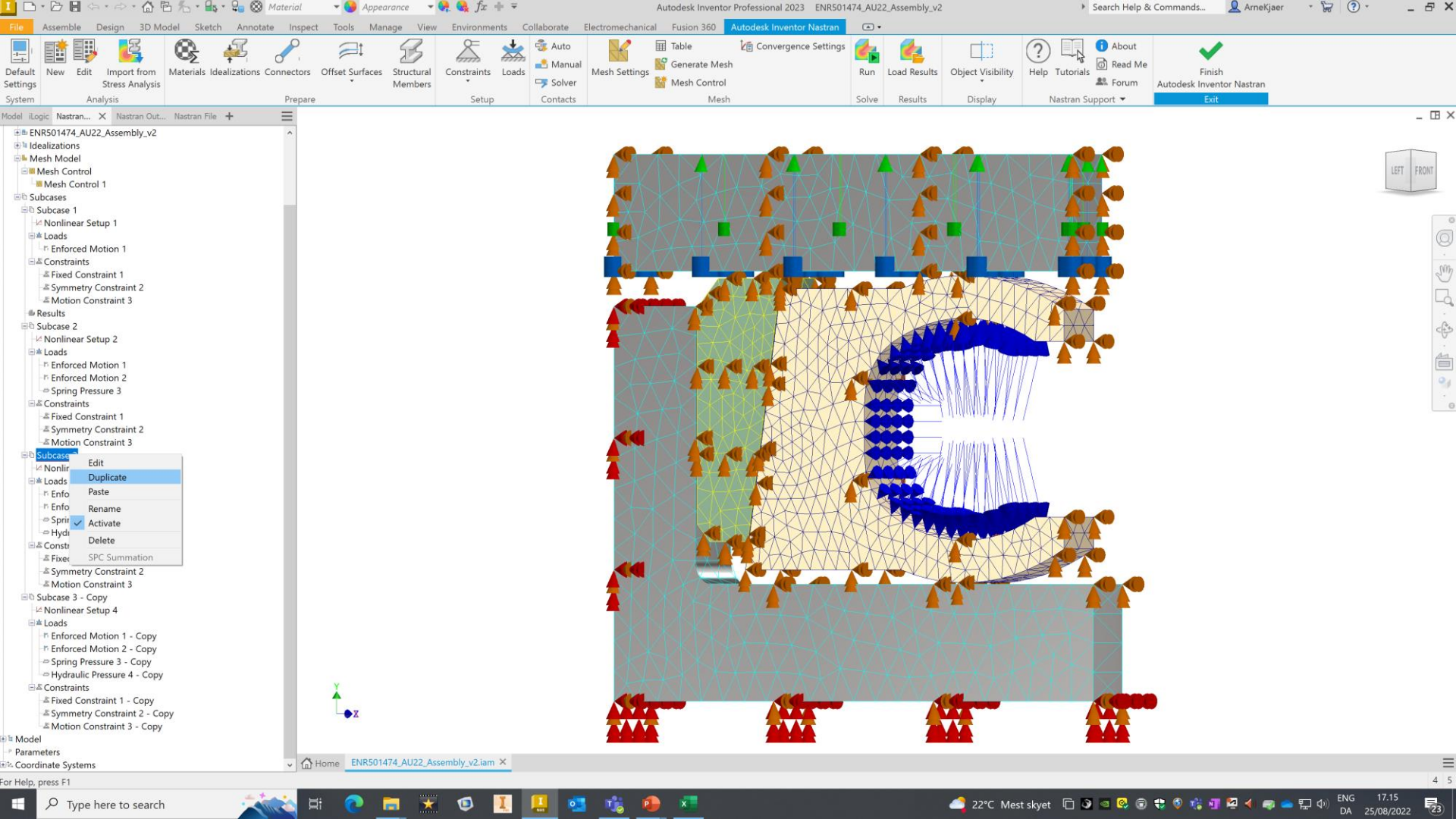


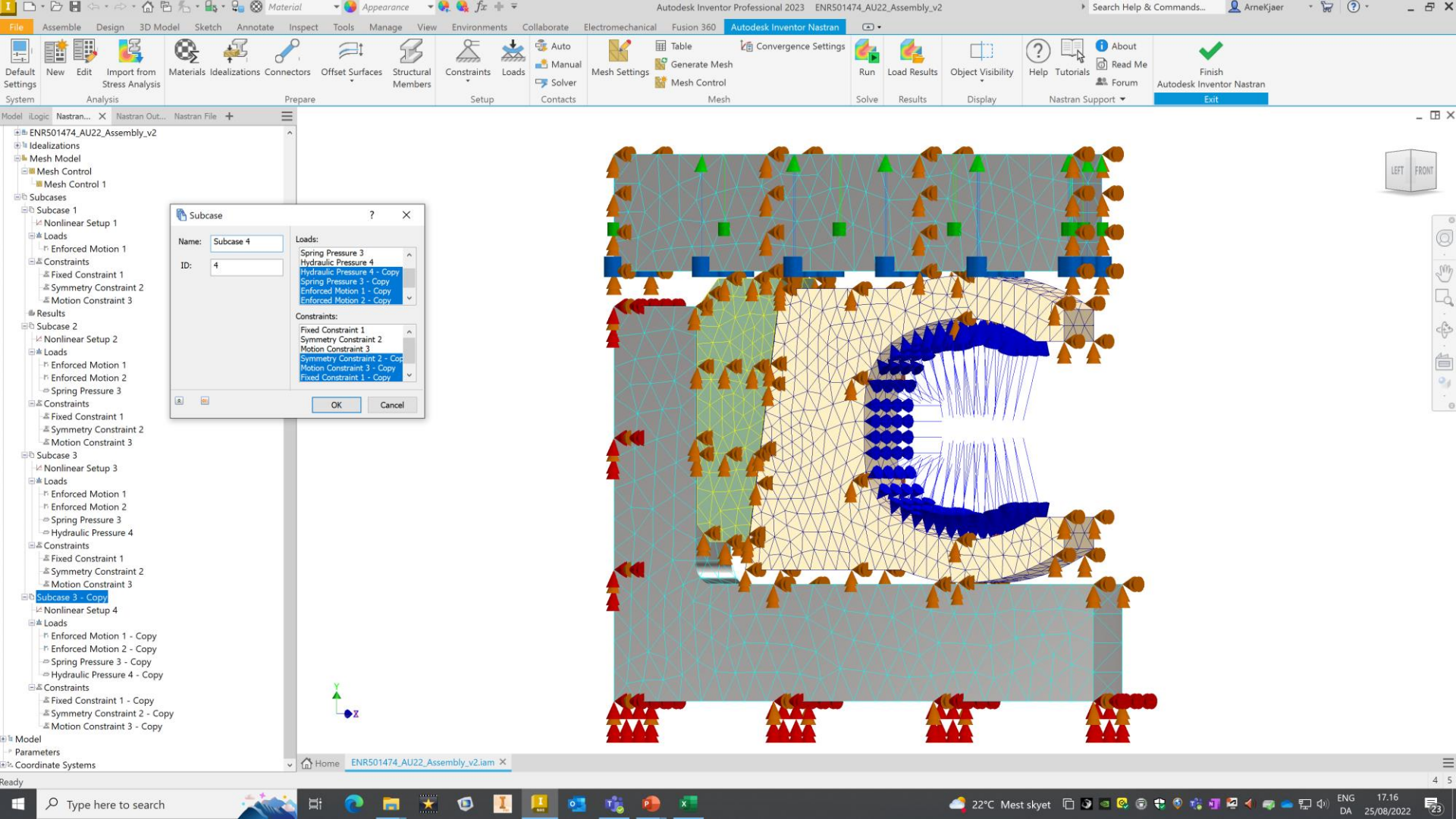


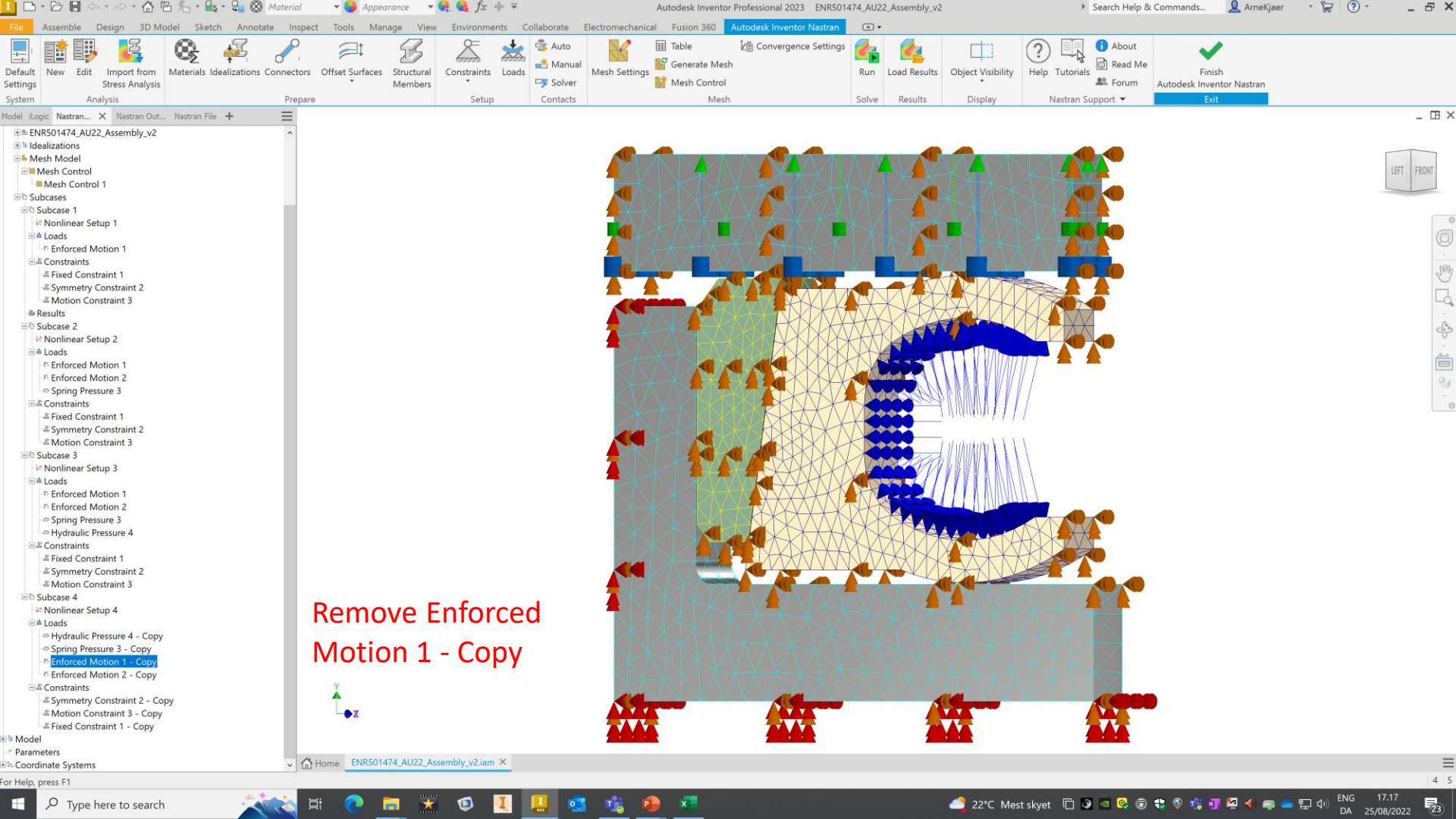


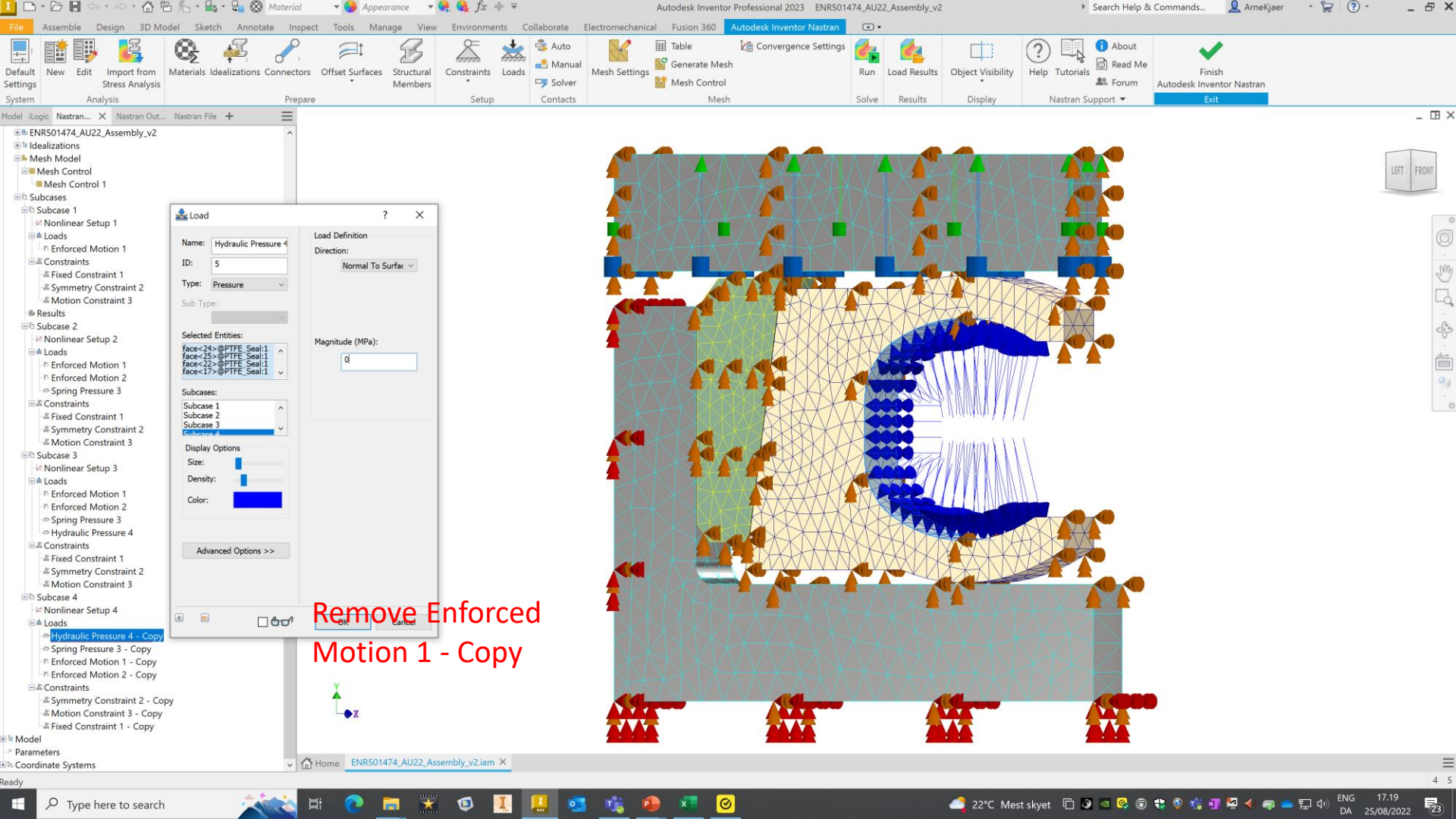


Subcase 4

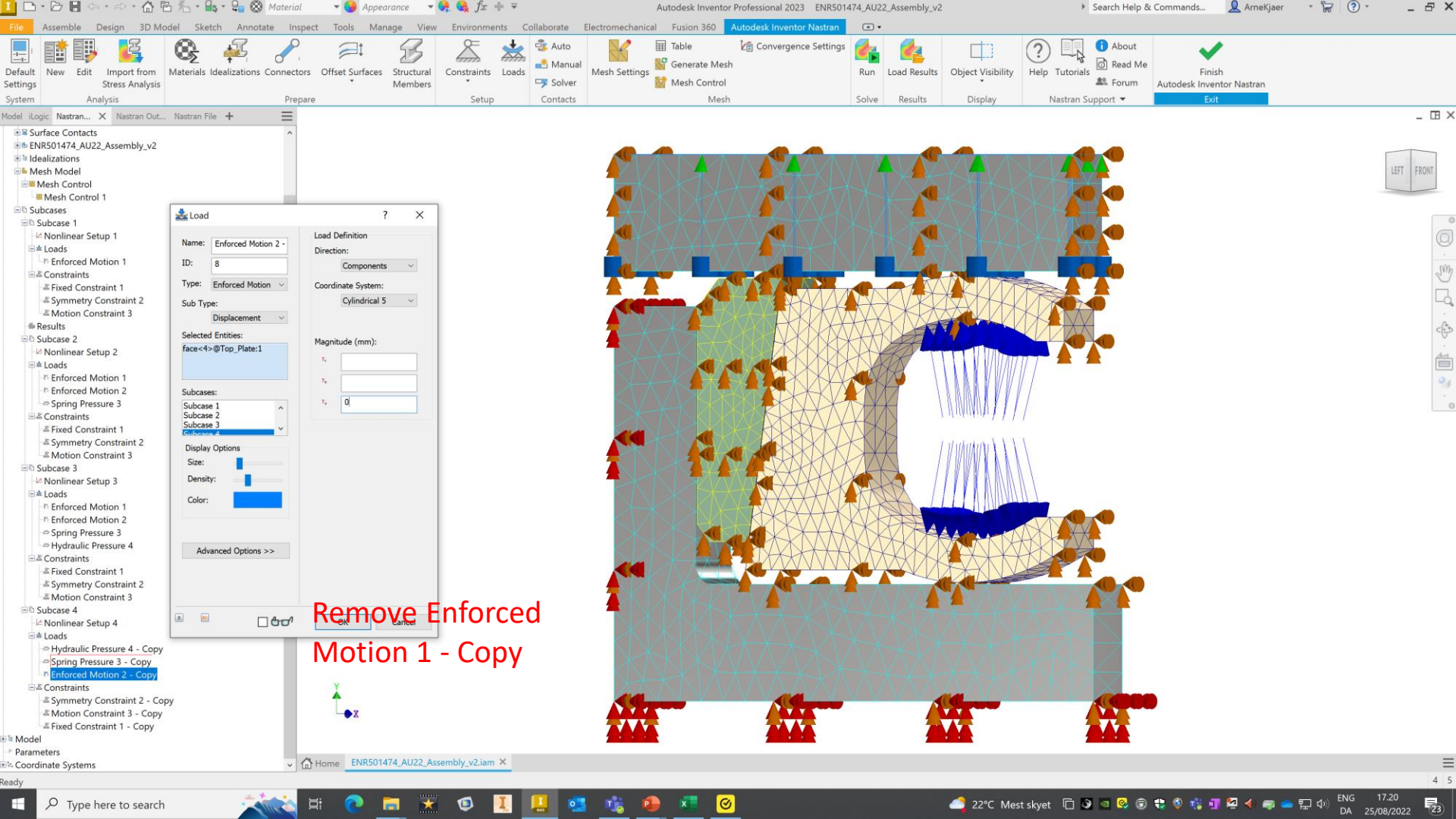








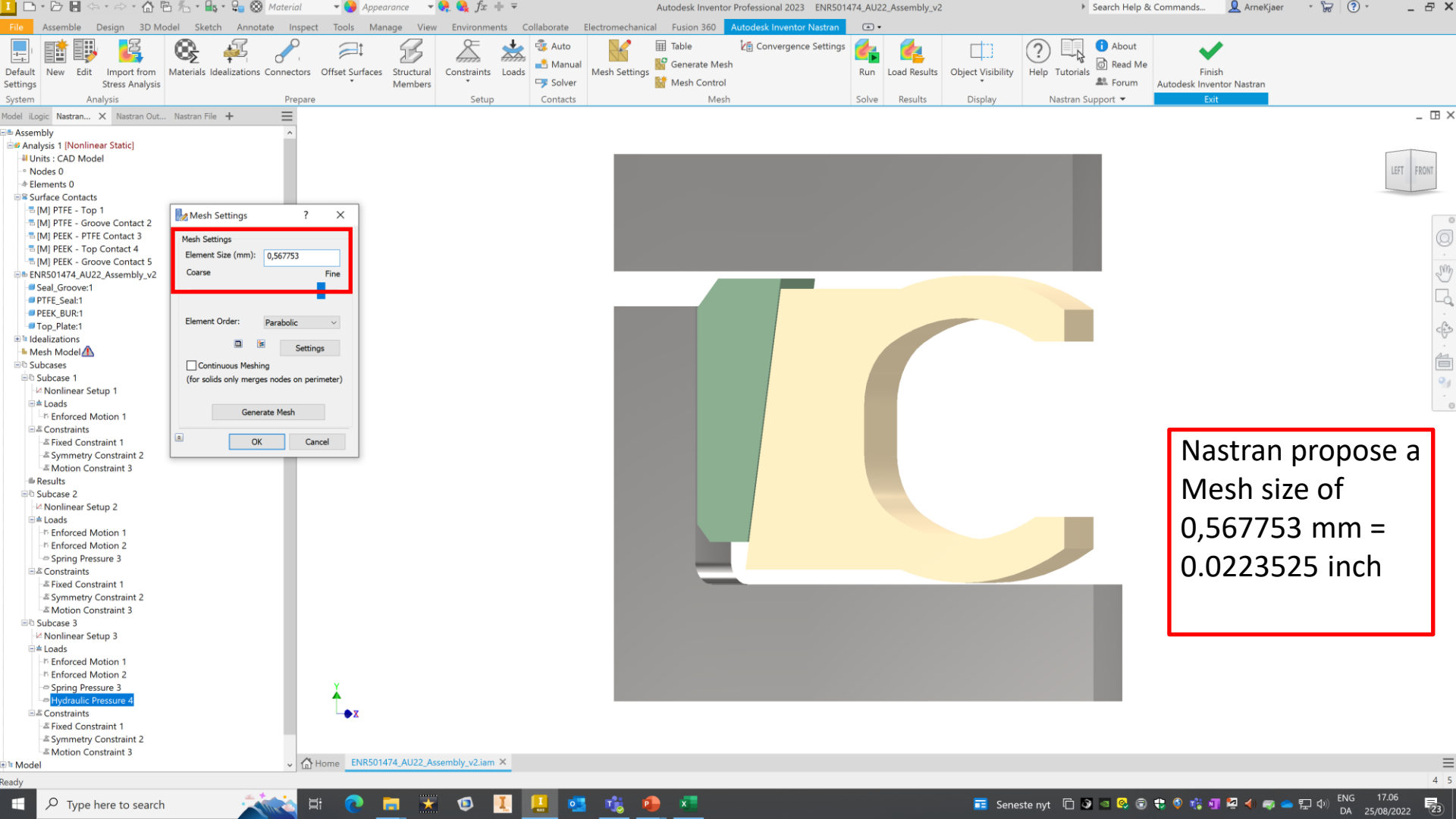
Remove Enforced
Motion 1 - Copy



Remove Enforced
Motion 1 - Copy

Mesh

Mesh Control



Mesh Settings

Element Size (mm): 0,567753

Coarse ☒ Fine

Element Order: Parabolic

☐ Continuous Meshing
(for solids only merges nodes on perimeter)

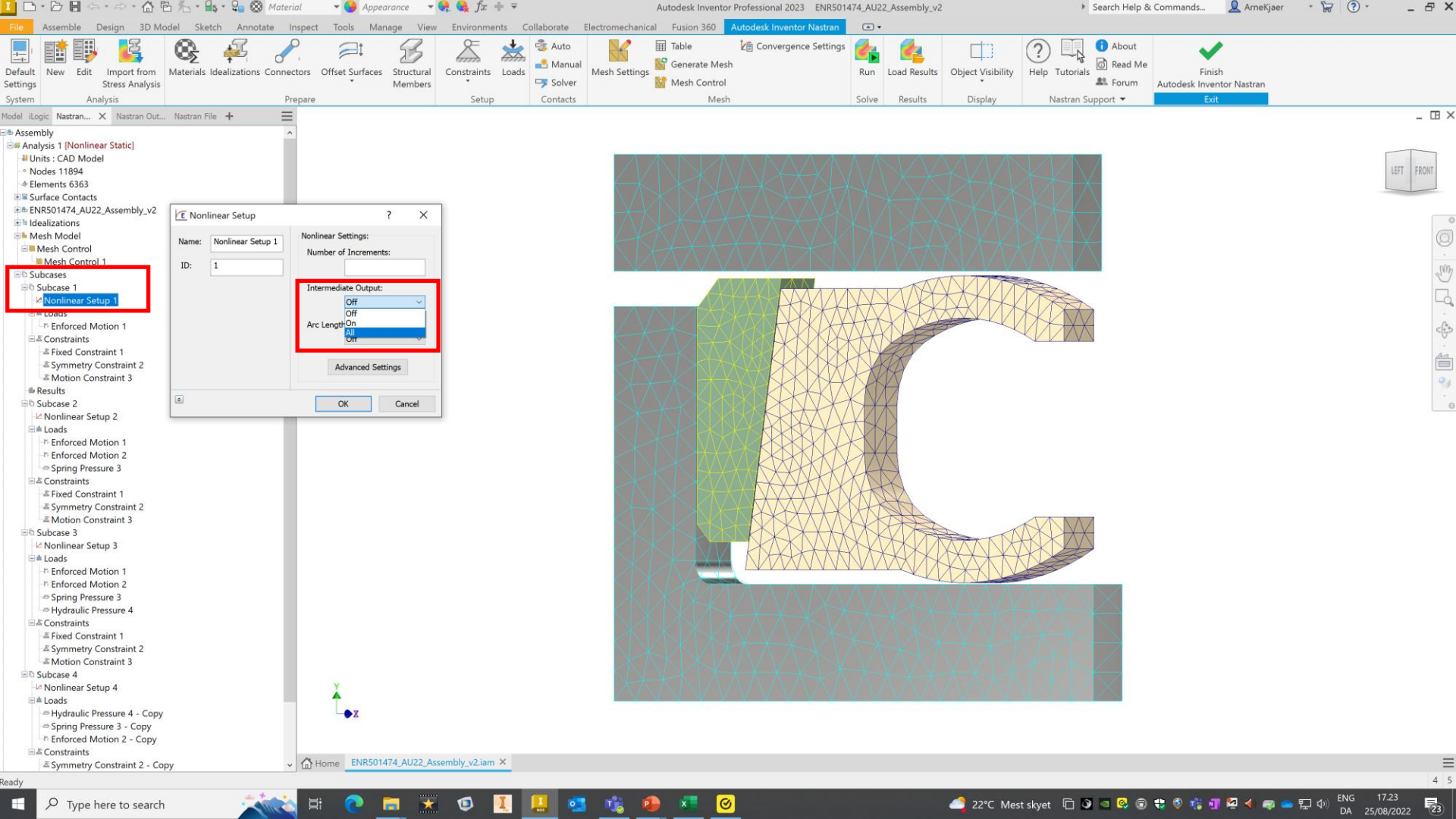
Generate Mesh

OK Cancel

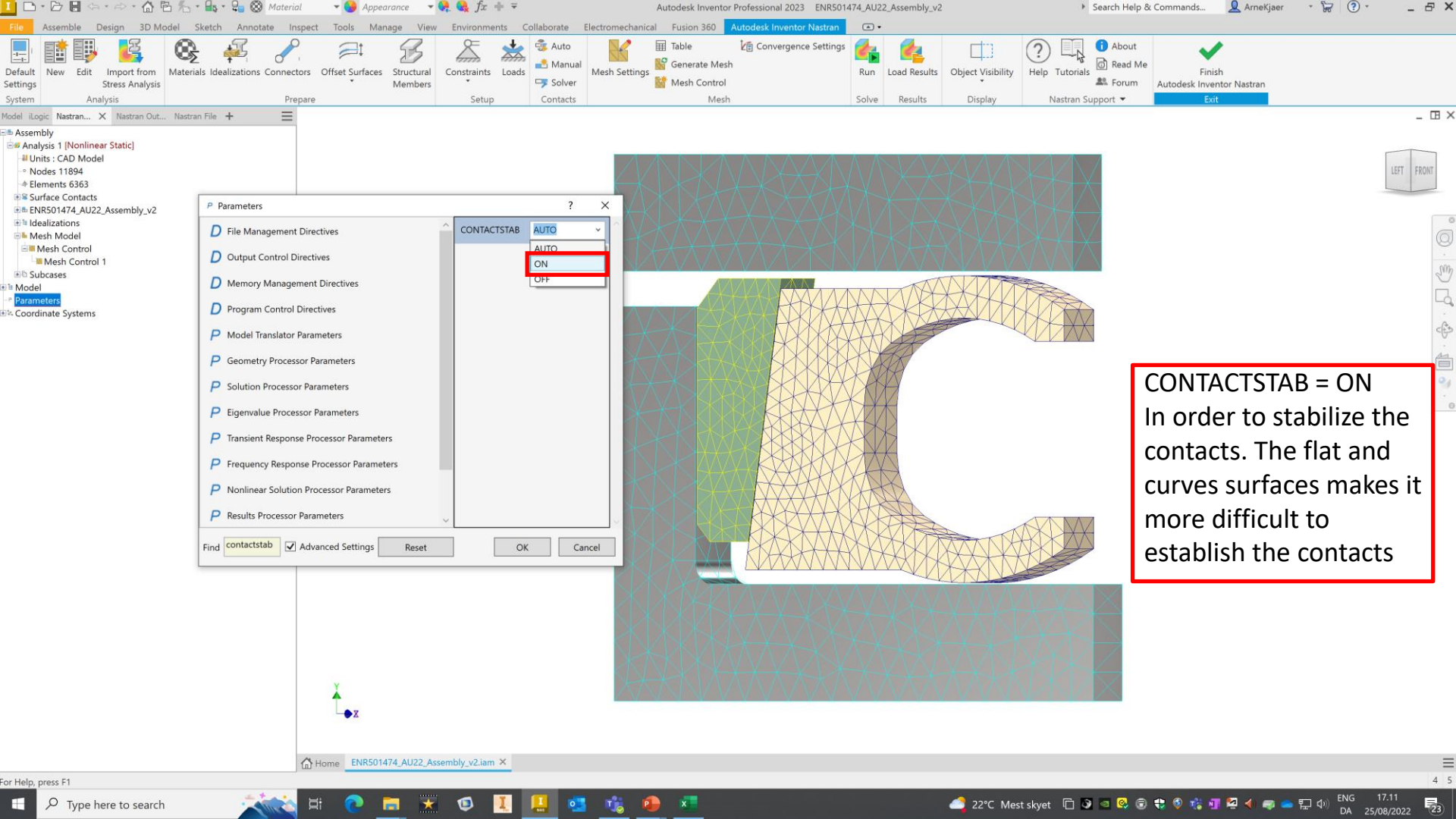
Nastran propose a
Mesh size of
0,567753 mm =
0.0223525 inch

Relative	Mesh	Mesh Control	Nodes	Elements	Max Stress	Wall clock time
100%	0,5190	0,3035	11567	6150	22,4	344,99
100%	0,5190	0,3035	11567	6150	22,25	311,83
500%	0,3035					
175%	0,4307					
150%	0,4534					
125%	0,4818					
120%	0,4884					
110%	0,5028					
100%	0,5190	NA	6857	3503	26,54	260,8
90%	0,5376					
80%	0,5591					
75%	0,5712					
50%	0,6539					
25%	0,8239					
15%	0,9768					
10%	1,1182					
5%	1,4088					

Nonlinear Setup



Parameters

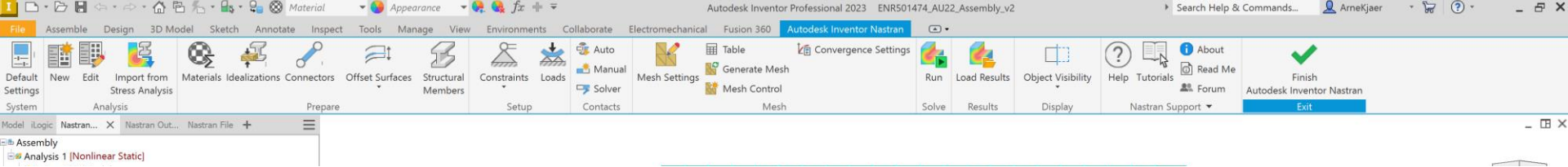


Parameters

CONTACTSTAB **ON**

Find **contactstab** ☒ Advanced Settings

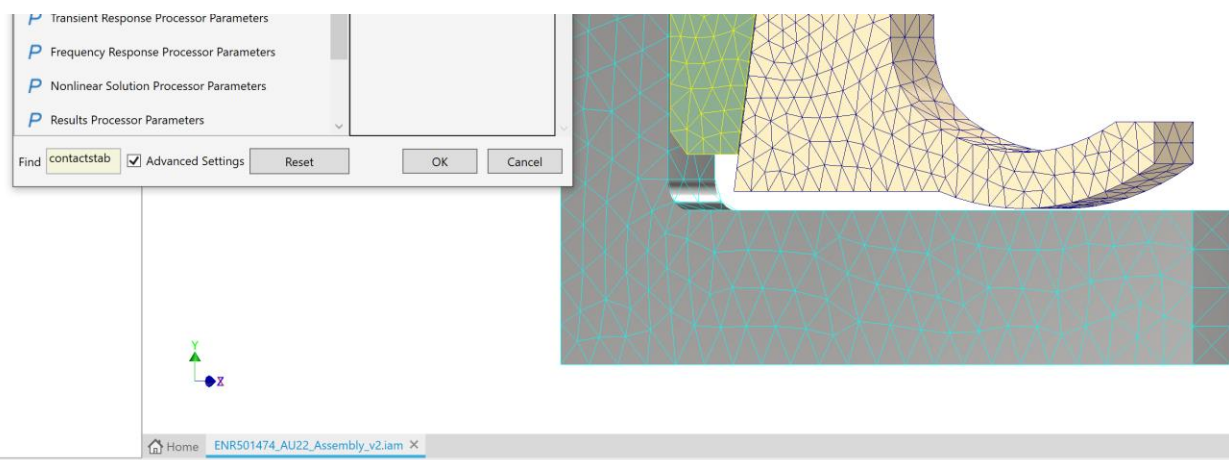
CONTACTSTAB = ON
In order to stabilize the contacts. The flat and curves surfaces makes it more difficult to establish the contacts



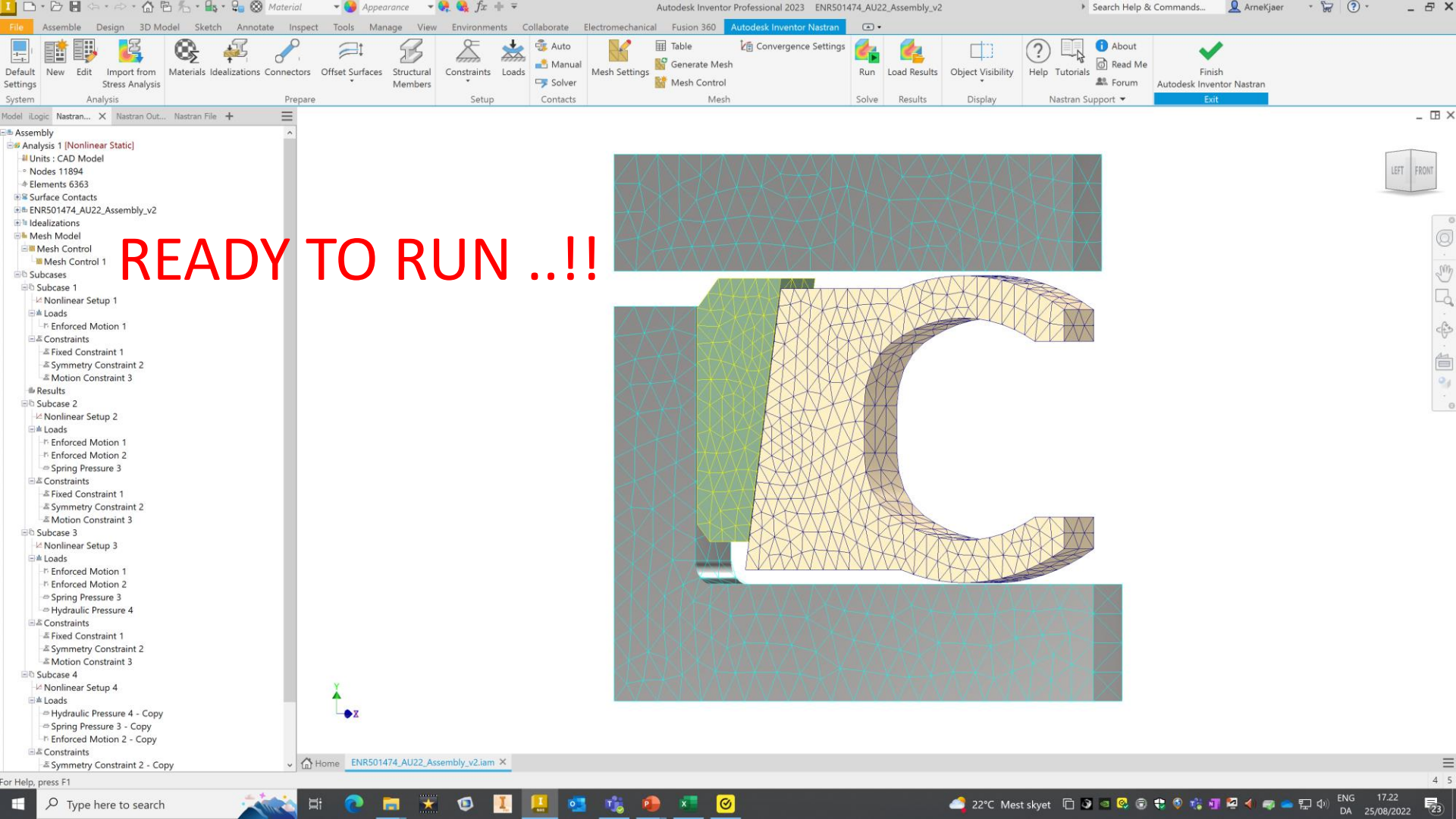
CONTACTSTAB

Description	Type	Default
Surface contact solution stabilization option. When set to ON, will generate stabilization spring stiffness via the model parameters <u>NLKDIAGSET</u> , <u>NLKDIAGAFAC</u> , and <u>NLKDIAGMINAFAC</u> on the contact boundary. The default AUTO setting will automatically detect and stabilize all surface contact in the model with a significant initial gap (i.e., model reference dimension multiplied by 1.0E-04). The stabilization stiffness used can be controlled by specifying a scale factor which is a multiplier to the stabilization stiffness calculated automatically.	Real ON/OFF AUTO	AUTO

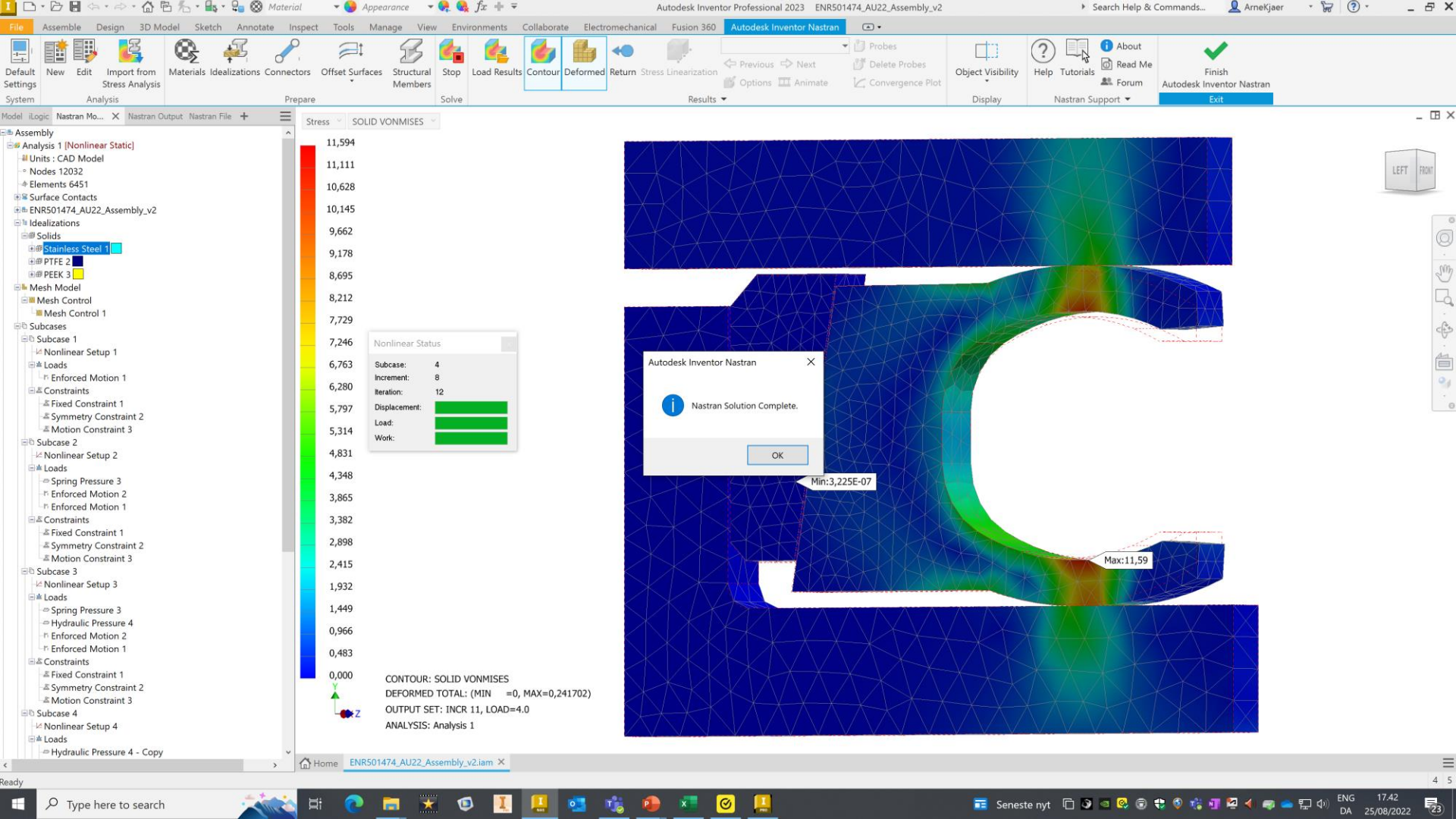
Parent topic: [Nonlinear Solution Processor Parameters](#)

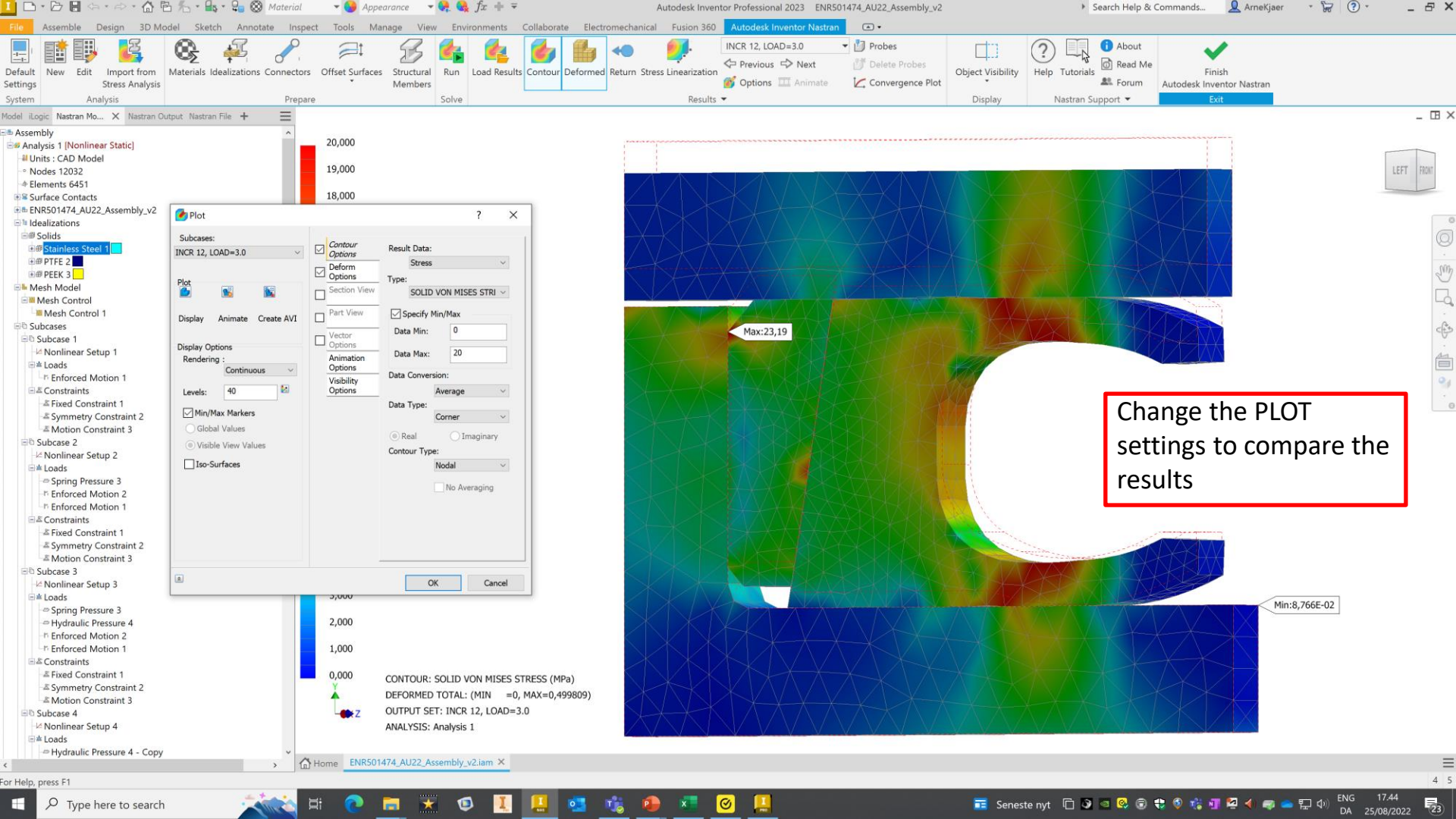


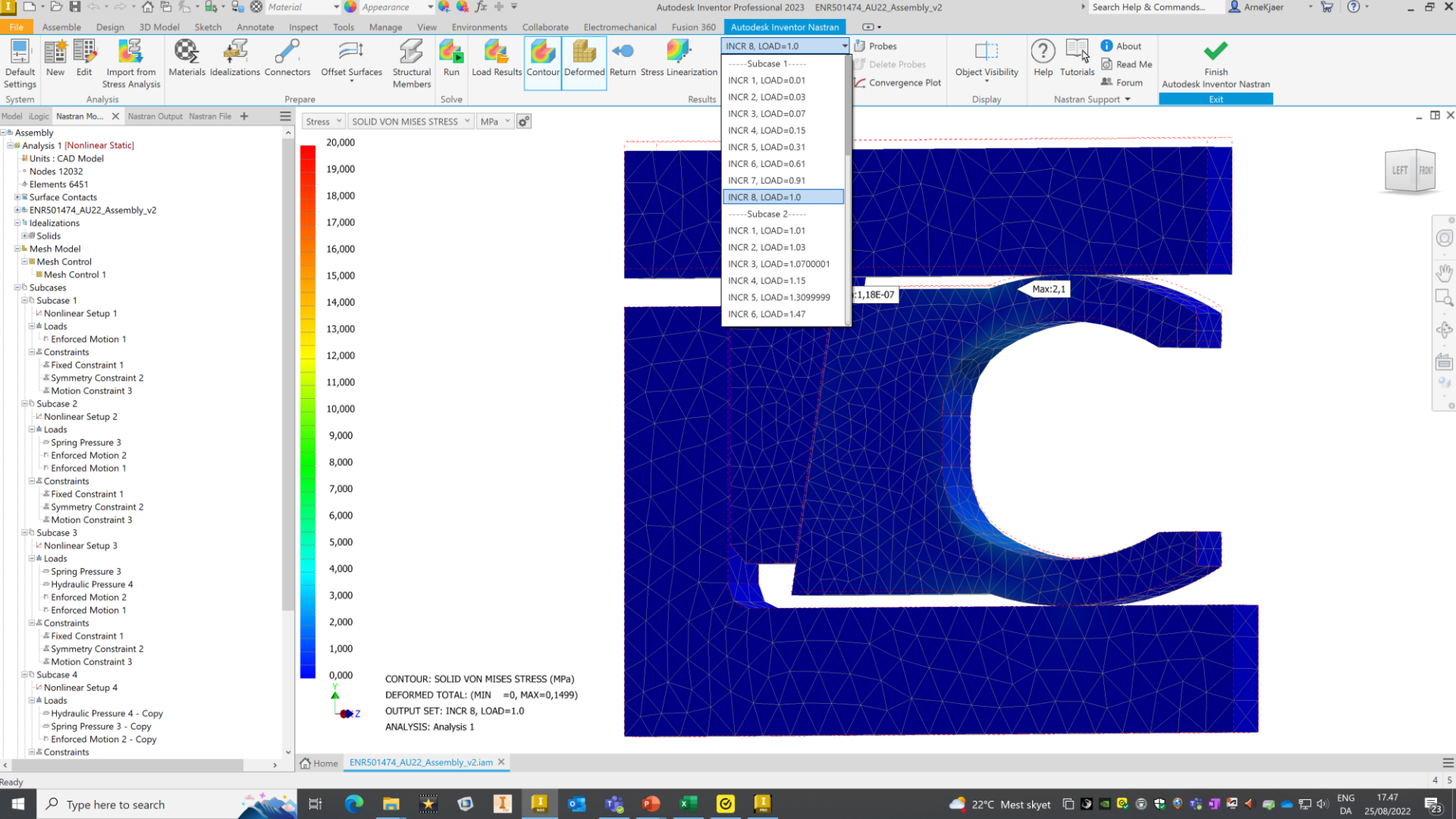
contacts. The flat and curves surfaces makes it more difficult to establish the contacts

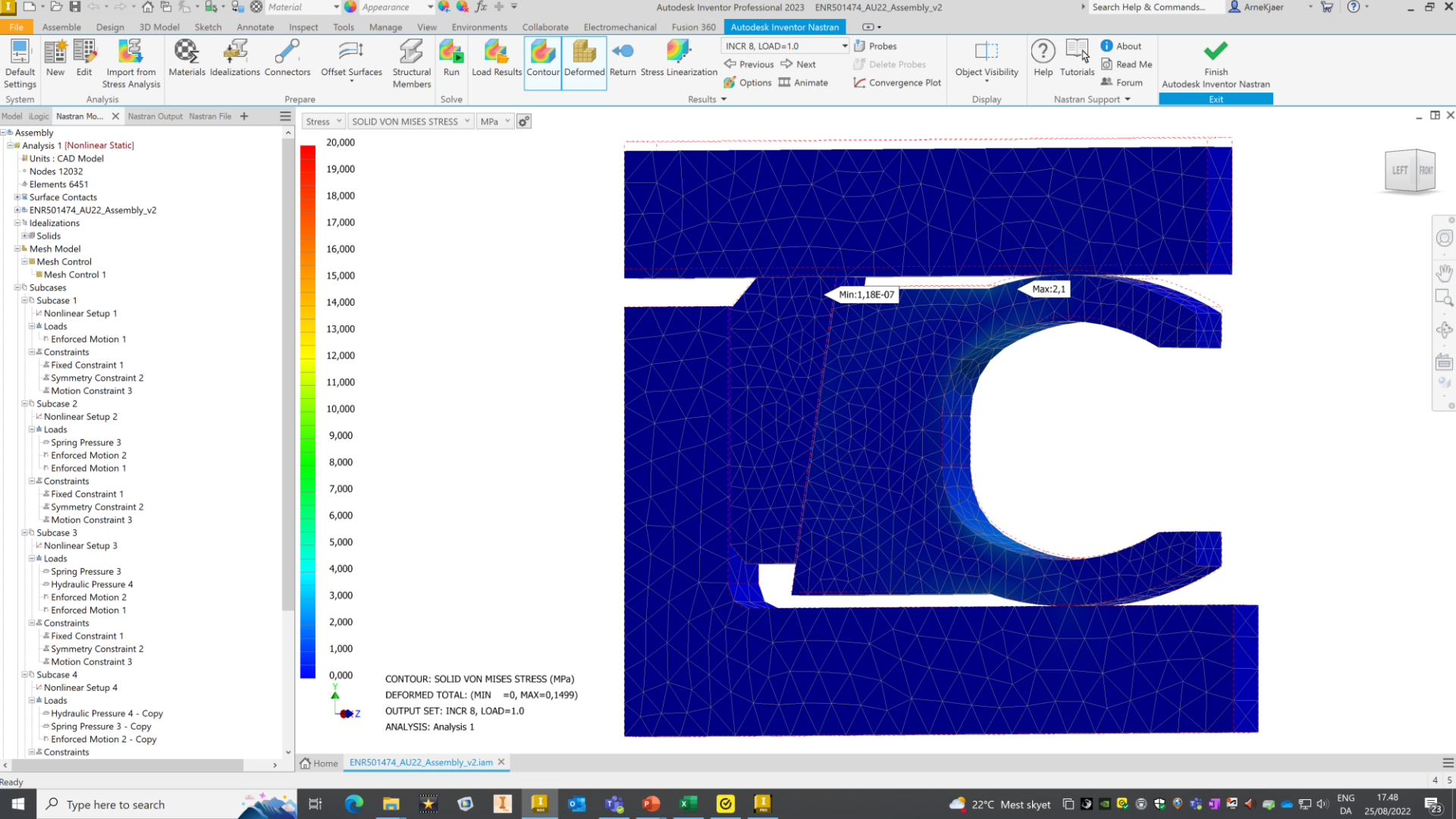


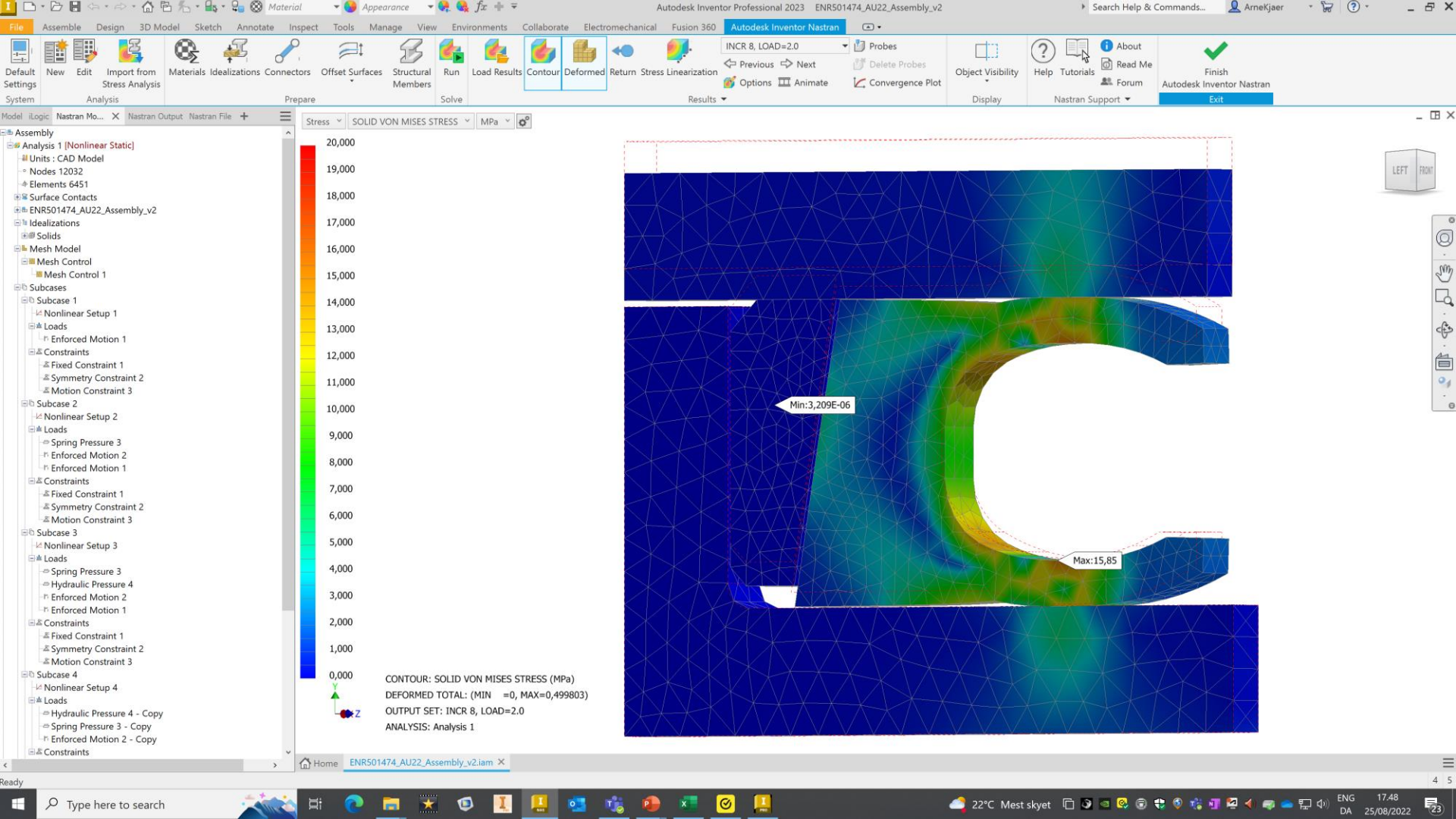
Run the Analysis





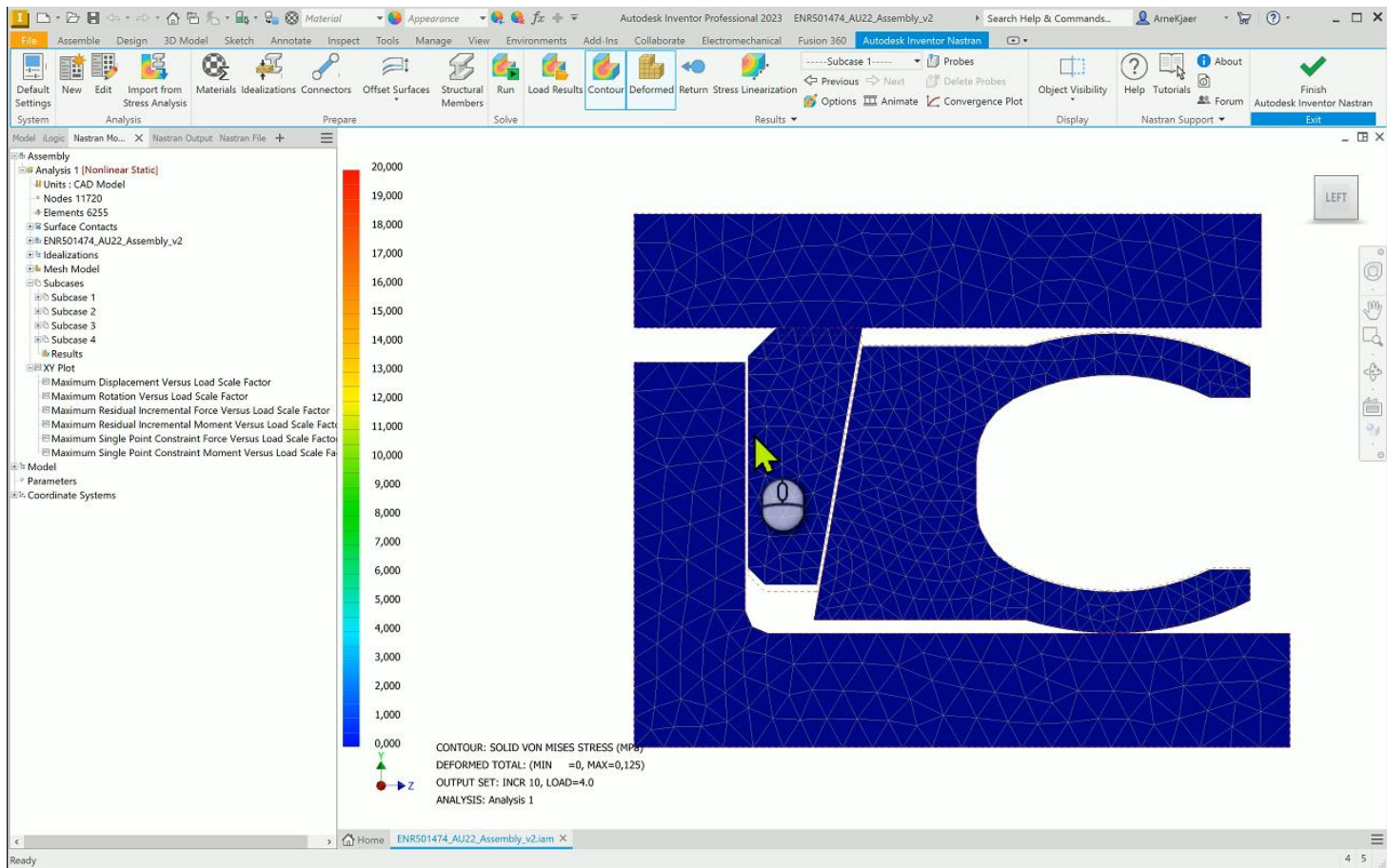


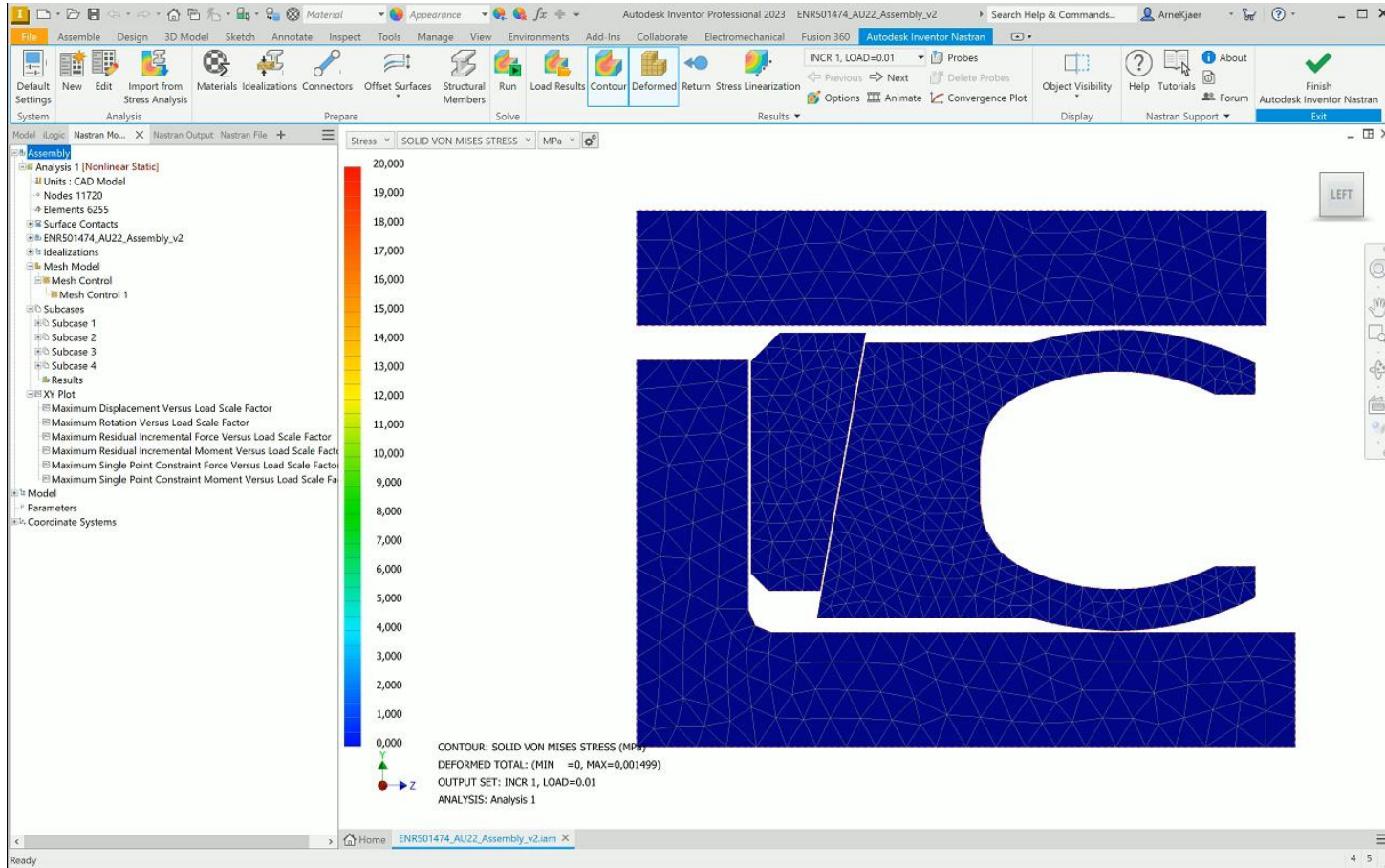




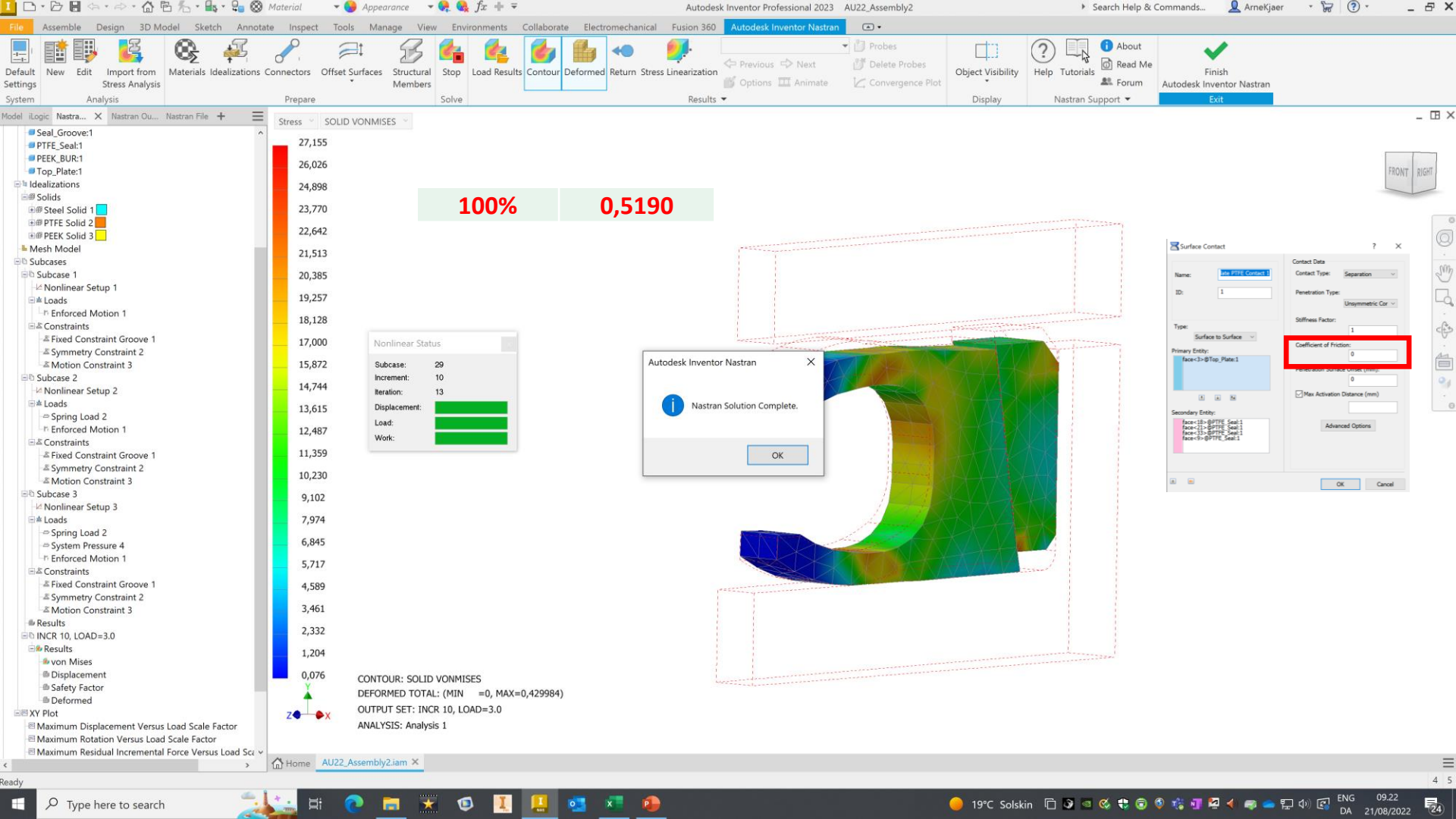


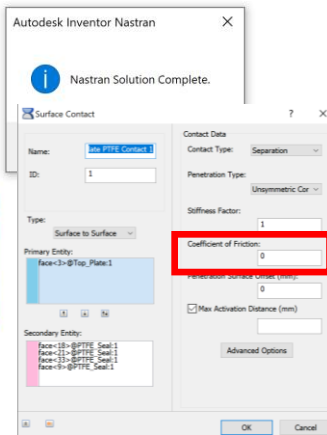
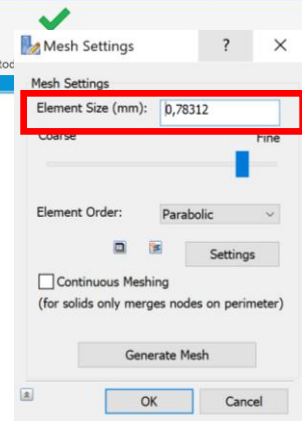
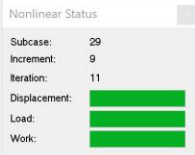
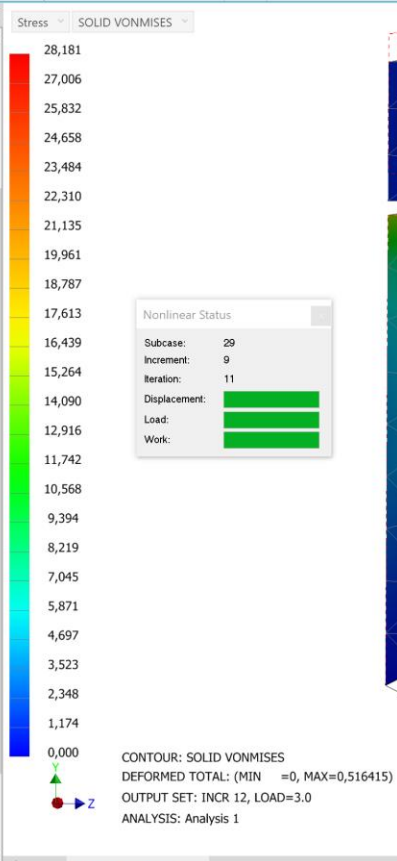
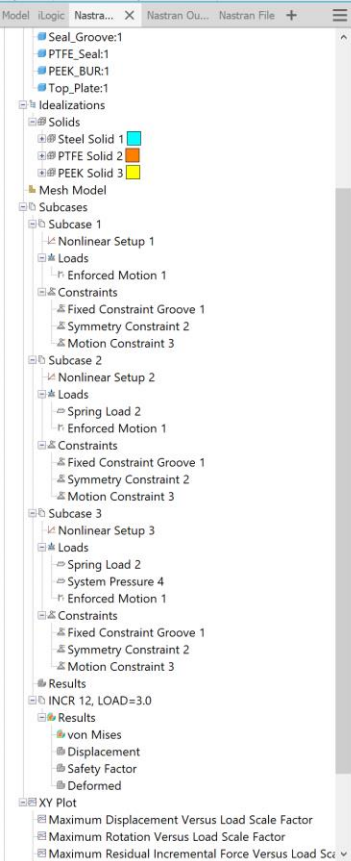
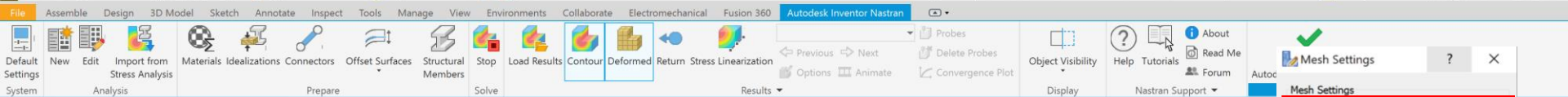


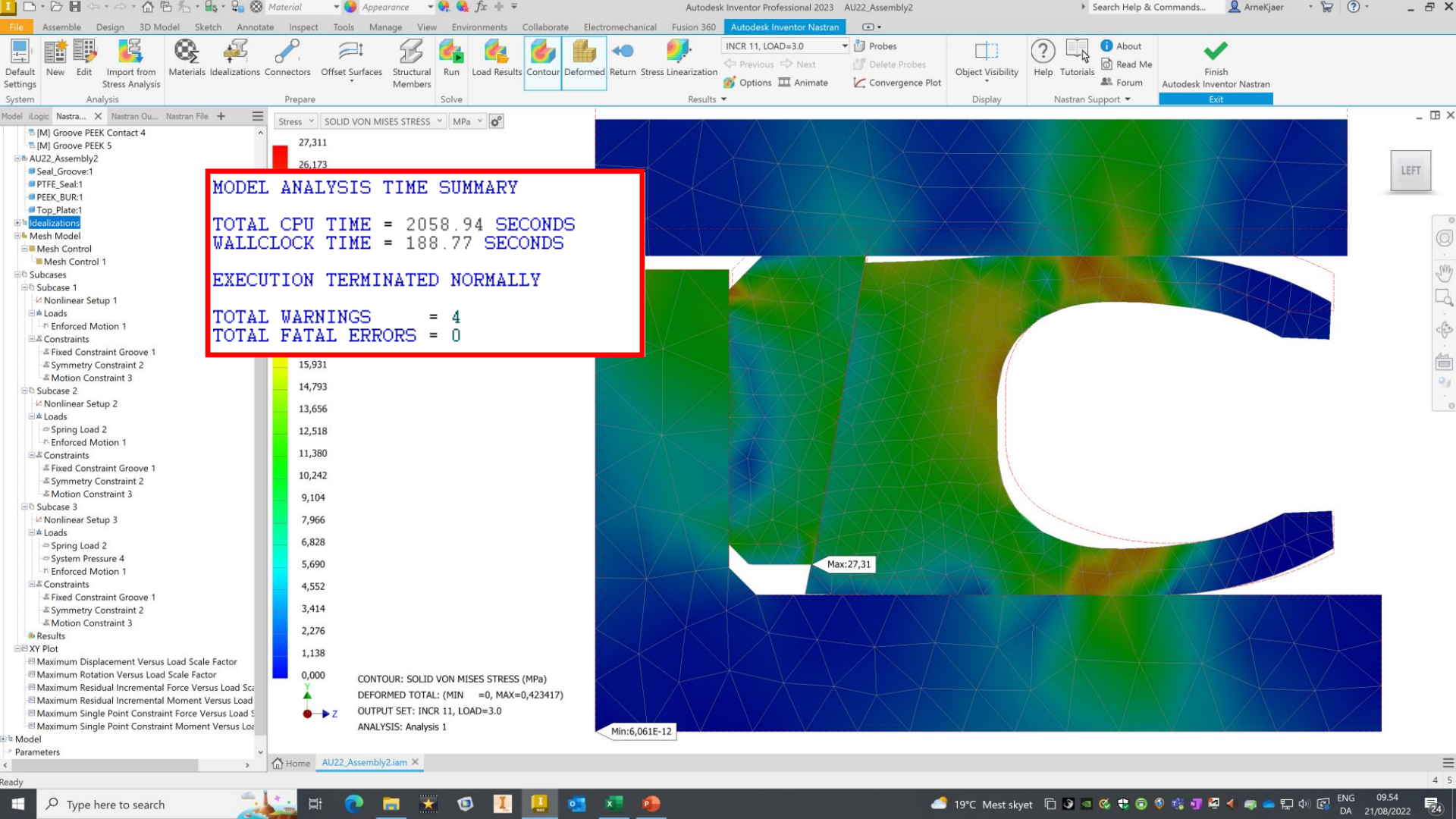


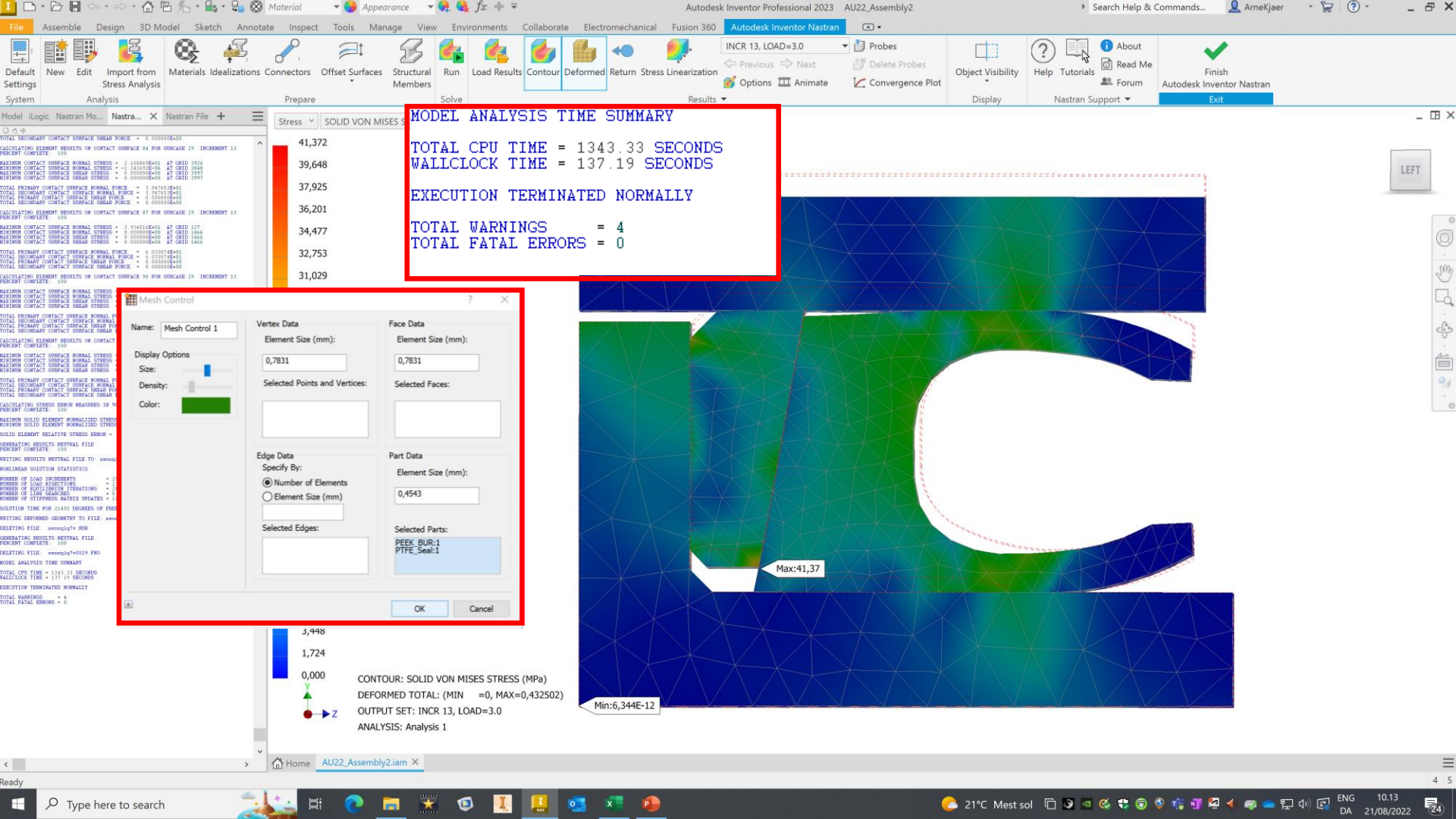


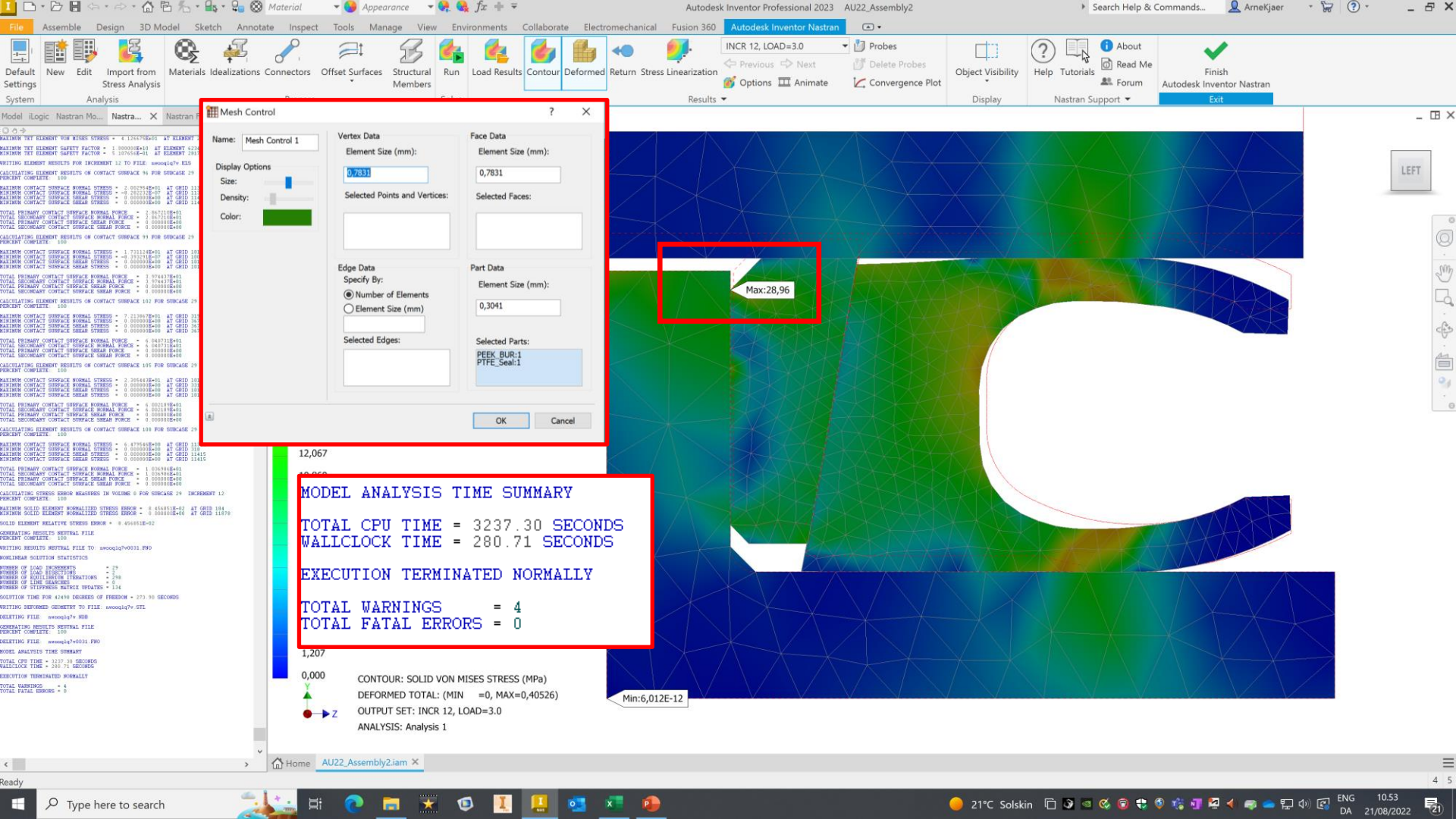
Run the Analysis with Different Mesh

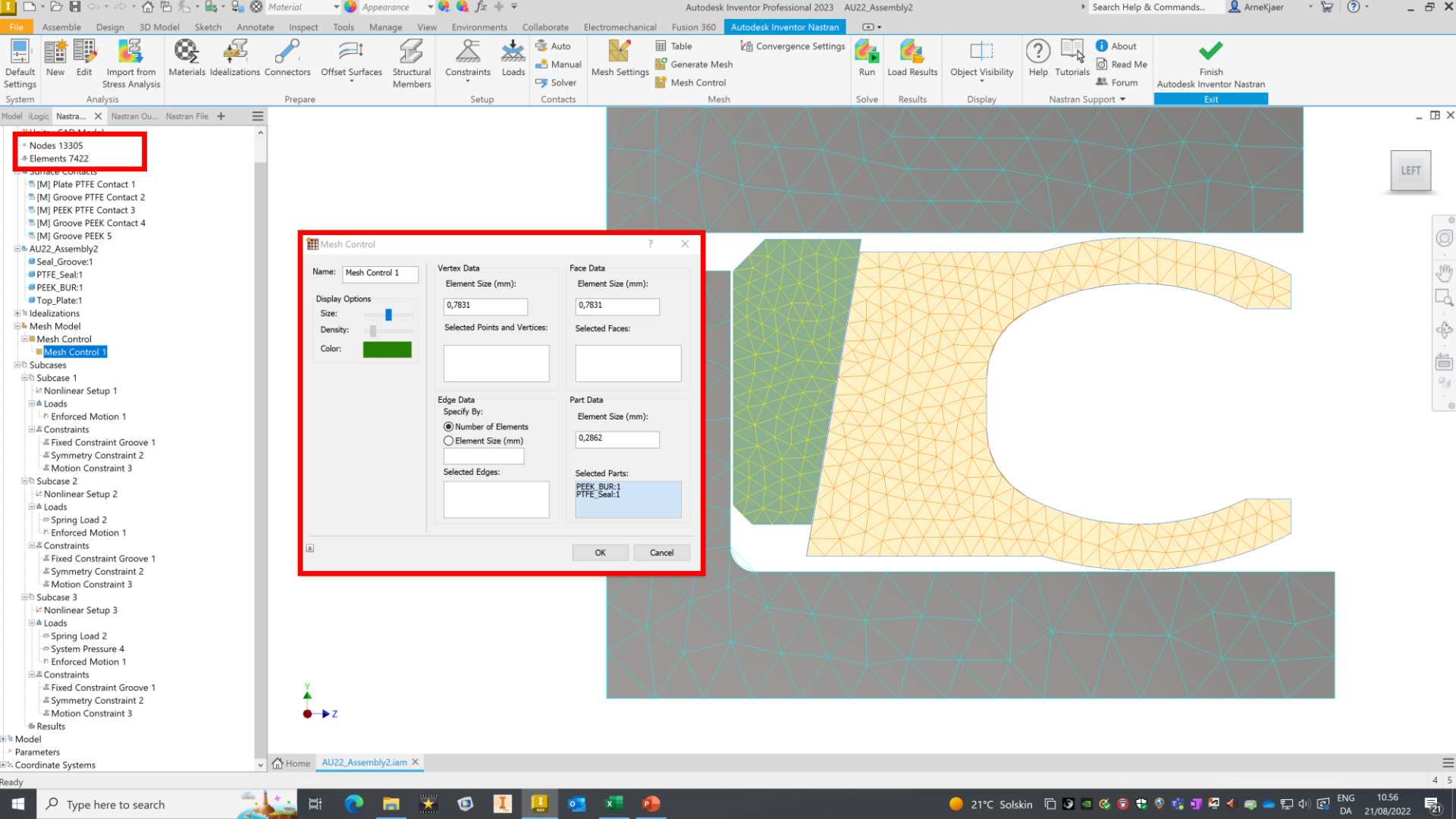


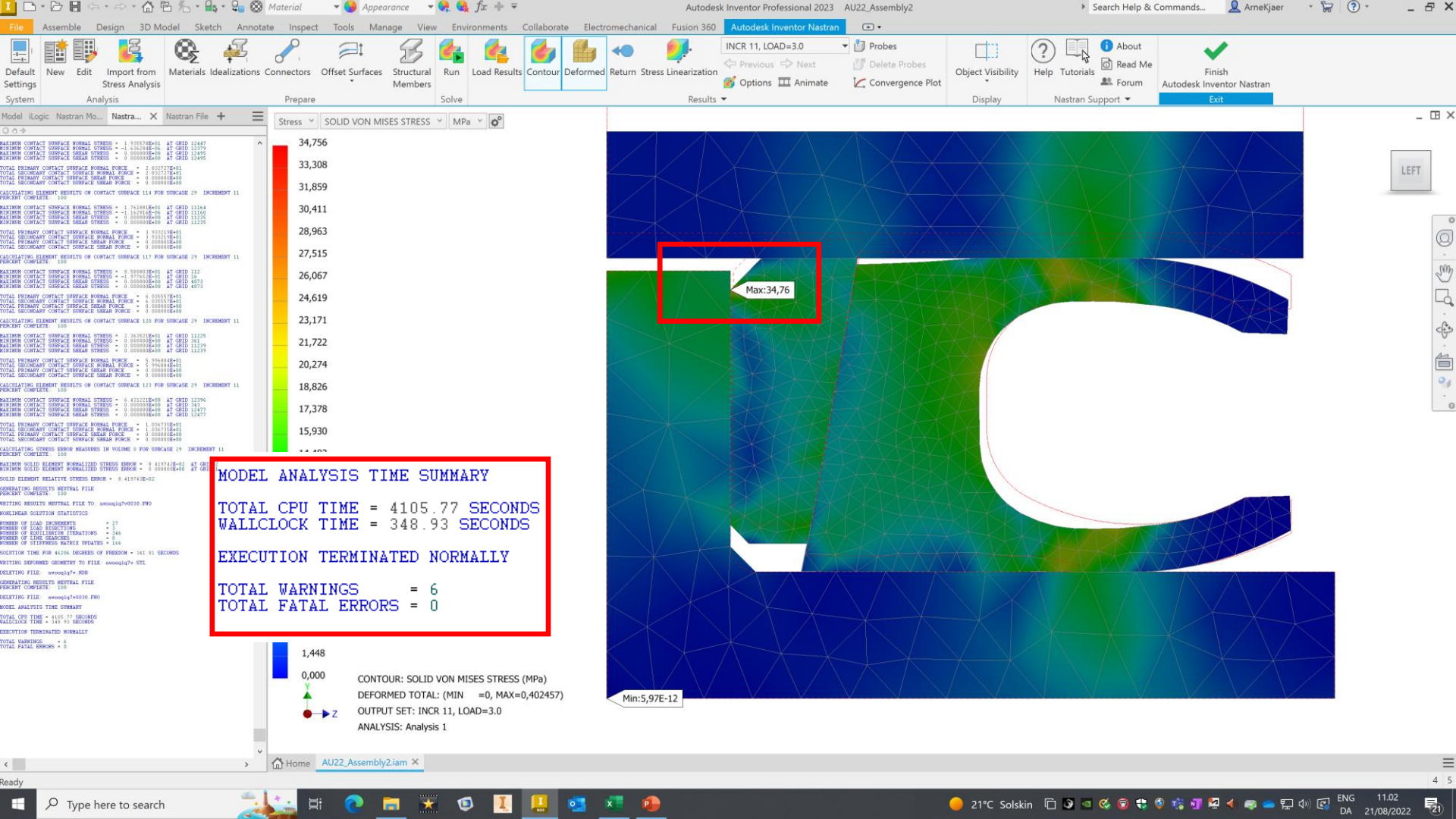


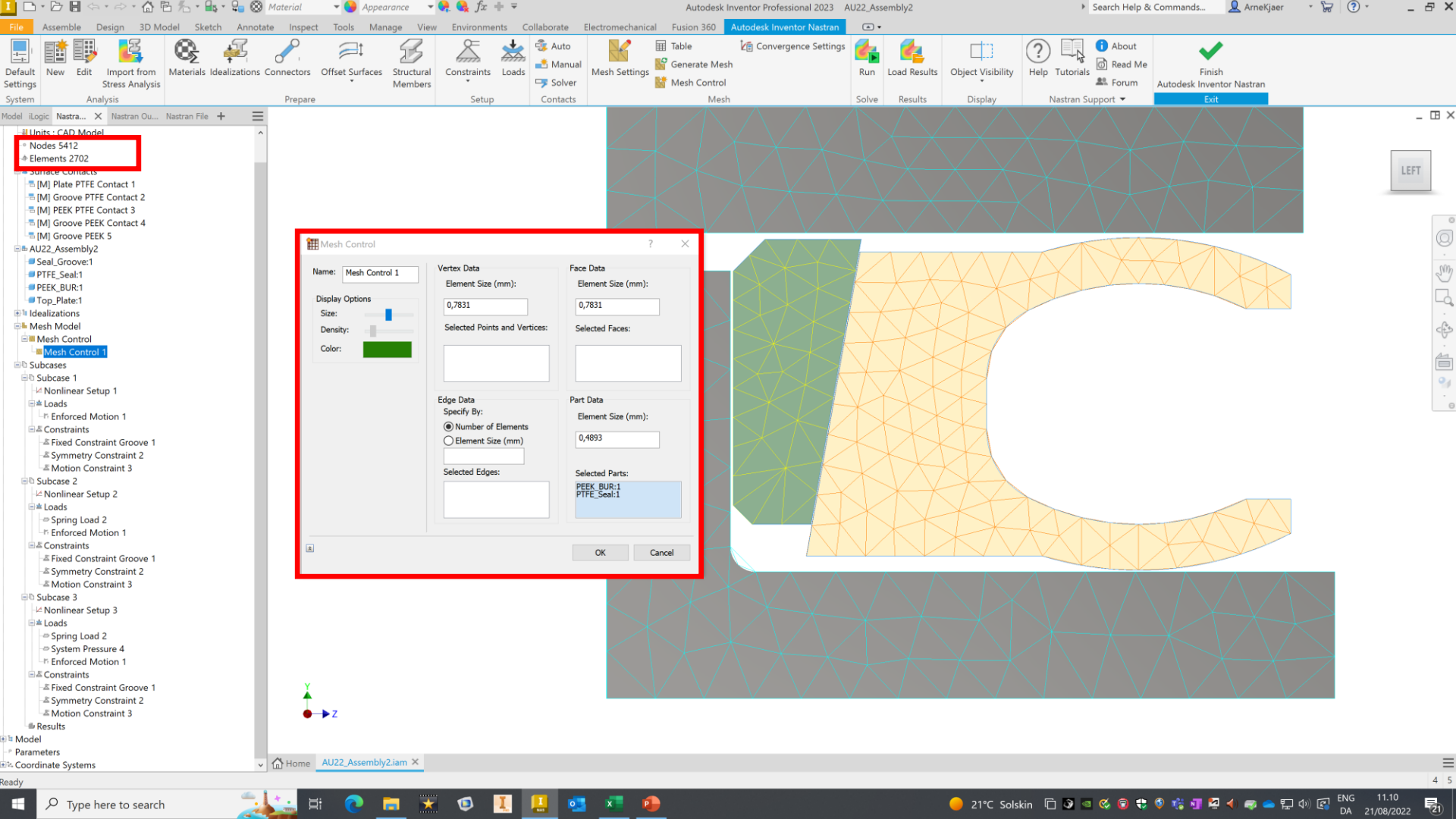


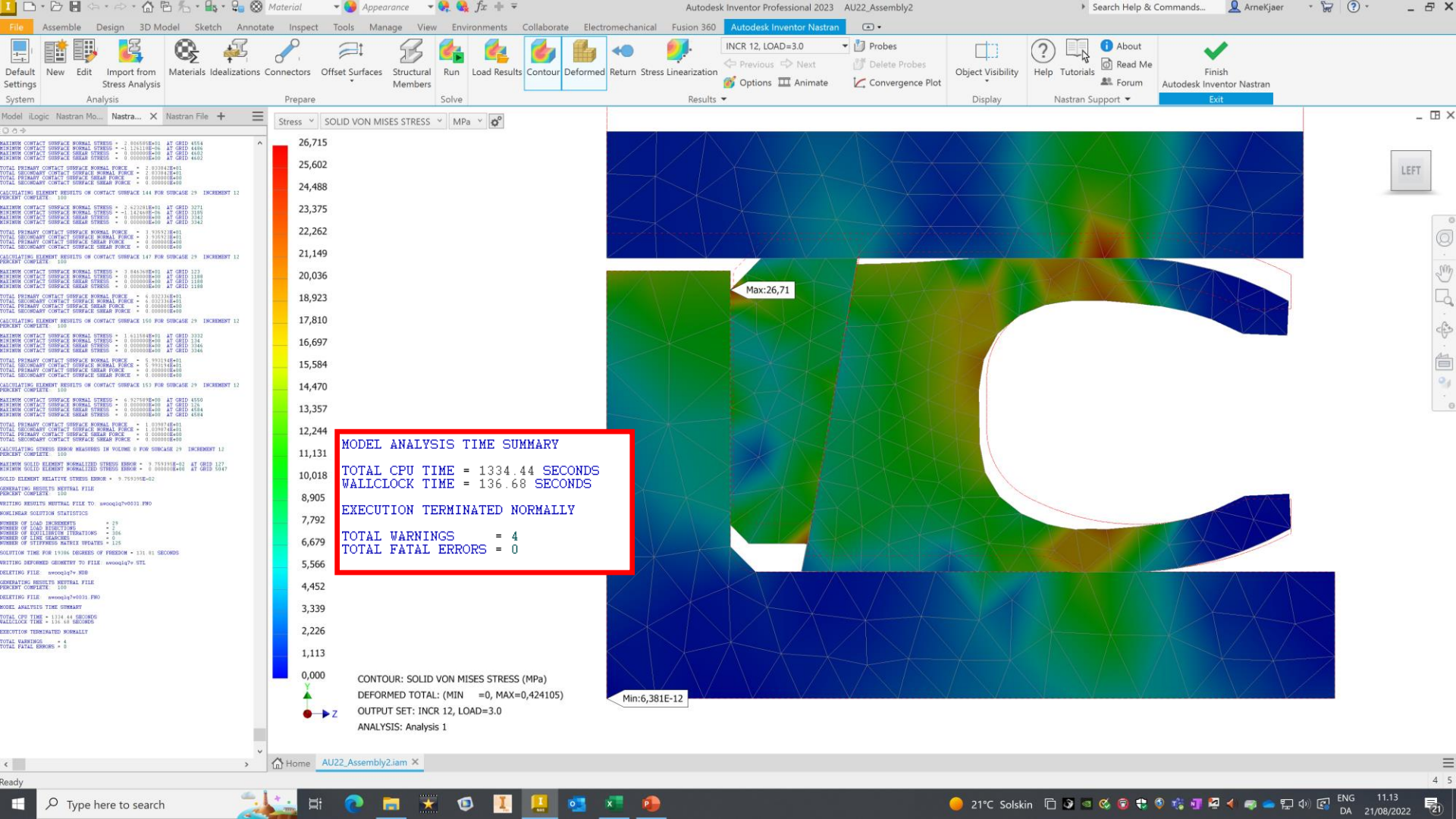


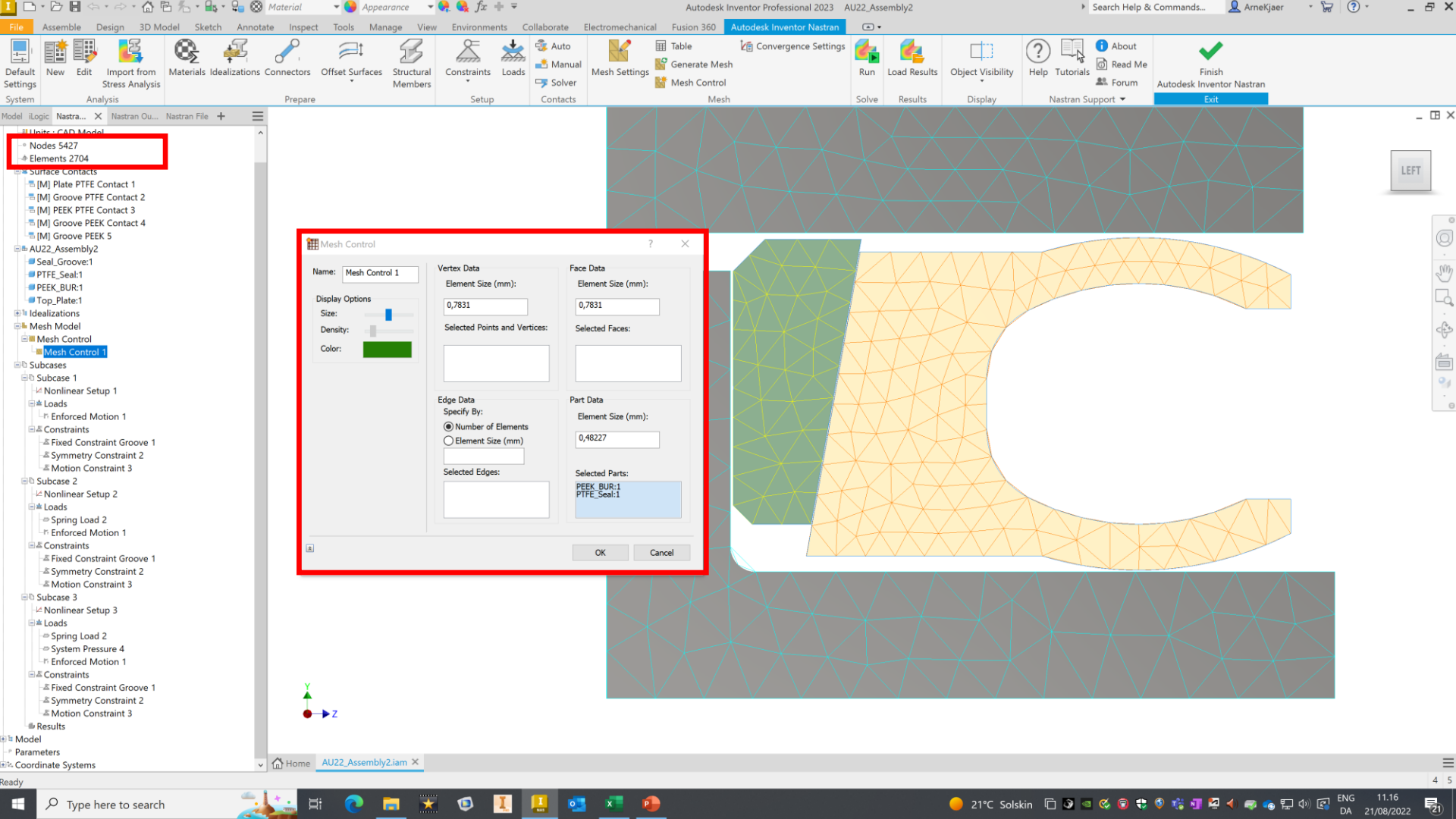


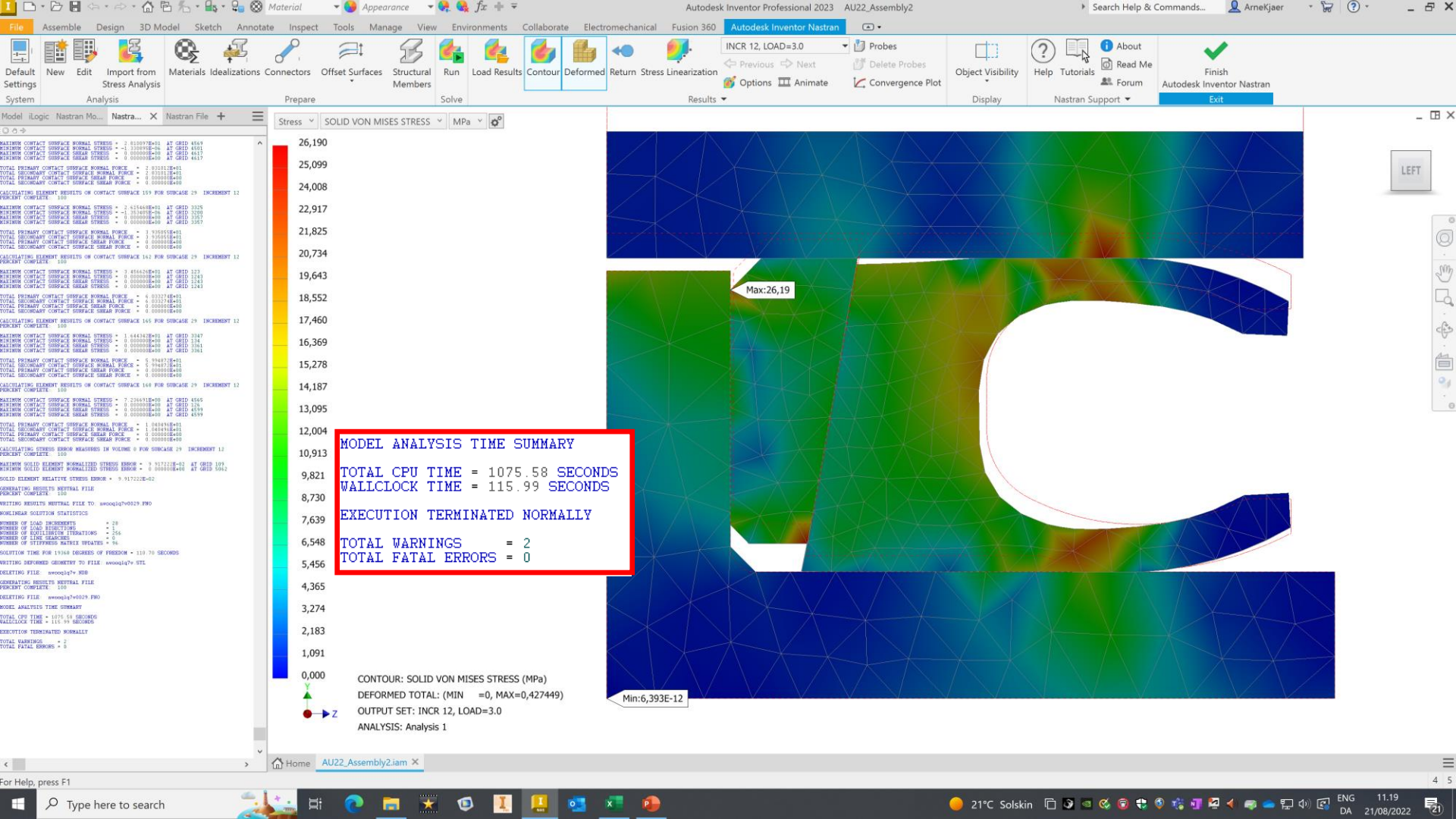


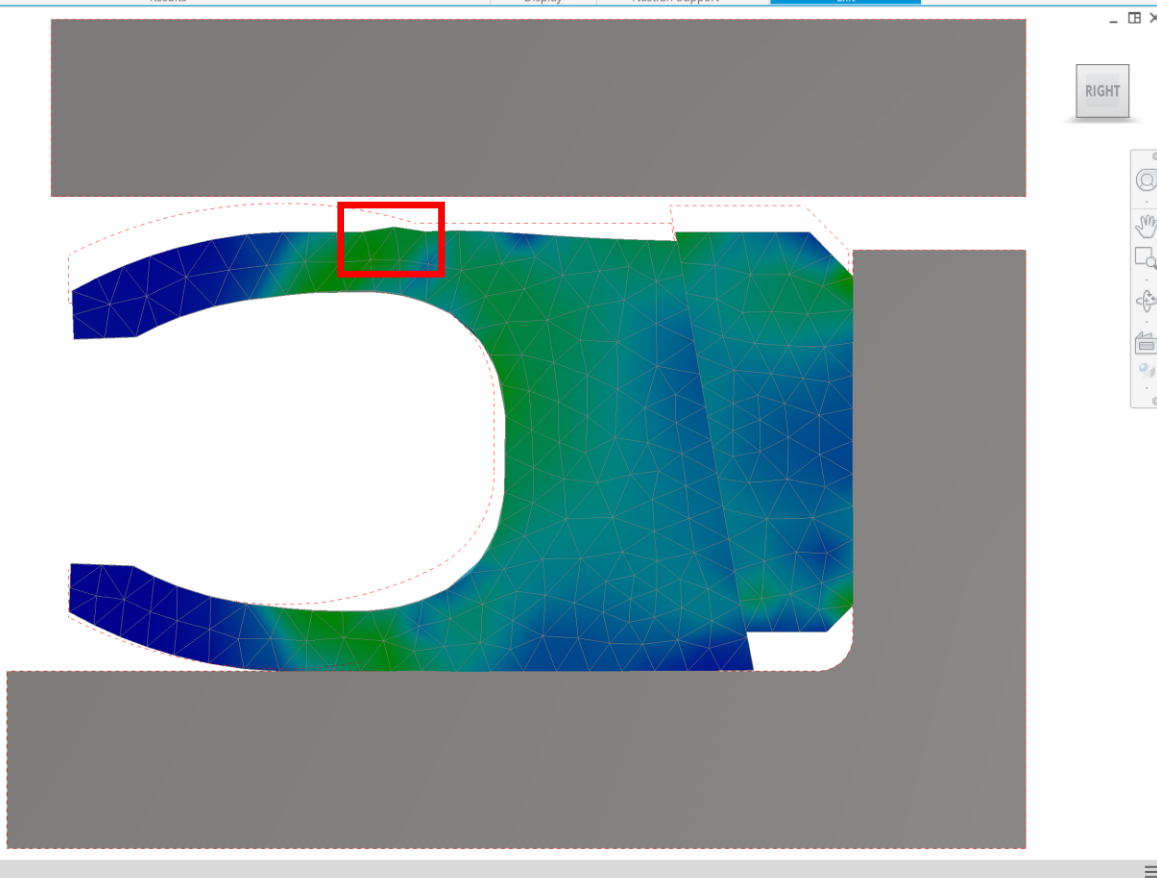


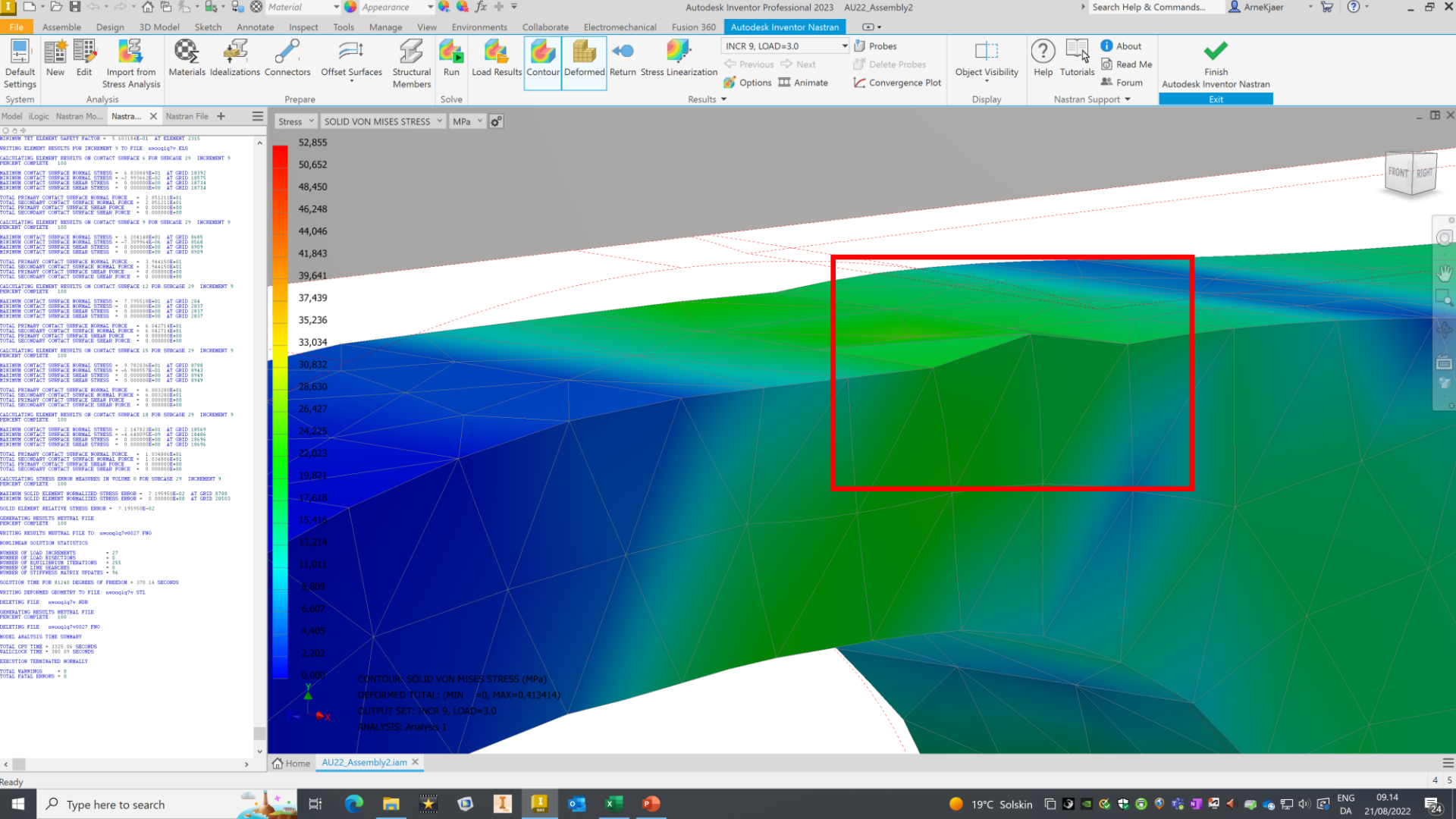










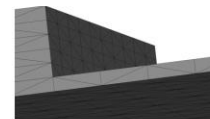


Mesh Aspect Ratio

- Data on the thin beam w/ contact experiments (with ENHCONTACTRSLT=OFF):
 - Tet Aspect Ratio 8:1 - 77% disp error
 - Tet Aspect Ratio 3:1 - 34% disp error
 - Tet Aspect Ratio 1:1 - 1.9% disp error
- If that aspect ratio is close to 1:1 you should get good displacement results and not need multiple elements through the thickness
- For a 6:1 AR version with 3 layers:
 - Tet Aspect Ratio 6:1 (3 layers) - 10.4% disp error
- Getting good aspect ratio is key for ENHCONTACTRSLT=OFF models

3-Point Bending - Thin

Reference Stress: 4,883 psi
Reference Displacement: 0.037 in

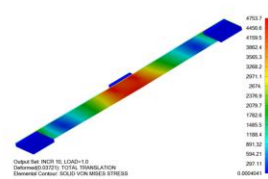


TET10 mesh with ok aspect ratio elements



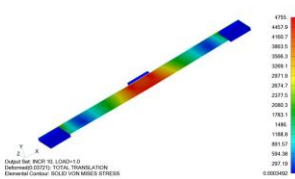
Stress Error: 4.7% (bad distribution)
Displacement Error: 34%

ENHCONTACTRSLT=OFF



Stress Error: 2.7%
Displacement Error: 0.5%

ENHCONTACTRSLT=SEGMENTED



Stress Error: 2.7%
Displacement Error: 0.5%

ENHCONTACTRSLT=PARABOLIC
NSLINESURF DIV=4 or 6

Mesh Aspect Ratio

ENHCONTACTRSLT

Description	Type	Default
Enhances the contact element formulation for parabolic tet elements. When activated, it will subdivide parabolic tet element primary surfaces into 4 separate sub-surfaces and avoid linearizing the element face. If the model does not have contact on parabolic tet elements, this parameter will have no effect on the solution.	ON/OFF AUTO	AUTO

Parent topic: [Results Processor Parameters](#)

Mesh Aspect Ratio

Model with bonded contact between thin parts behaving too stiff in simulation

← SHARE

2018-09-05 | Technical Support

Issue:

A model composed of thin parts does not bend properly, such as multiple layers through the thickness of a printed circuit board (PCB). The displacement is too small. This issues applied to products that are using Nastran solver i.e. Autodesk Nastran, Inventor Nastran, Nastran In-CAD and Fusion 360 Simulation.

Causes:

The bonded contact is acting too stiff.

Solution:

[Option 1: \(Applies to Inventor Nastran, Nastran In-CAD, Nastran\)](#)

If the model is composed of parabolic solid elements (tet elements), change the Parameter ENHCONTACTRSLT to ON. This causes the contact to follow the parabolic elements more accurately. (In Nastran In-CAD, edit the Parameters branch in the browser and find ENHCONTACTRSLT.)

After changing ENHCONTACTRSLT, It may also be necessary to adjust the Stiffness Factor to a smaller value in order to obtain a more accurate solution.

[Option 2: \(Applies to Inventor Nastran, Nastran In-CAD, Nastran, Fusion 360 Simulation\)](#)

If the model is composed of parabolic solid elements (tet elements), use offset bonded contact with activation distance specified.

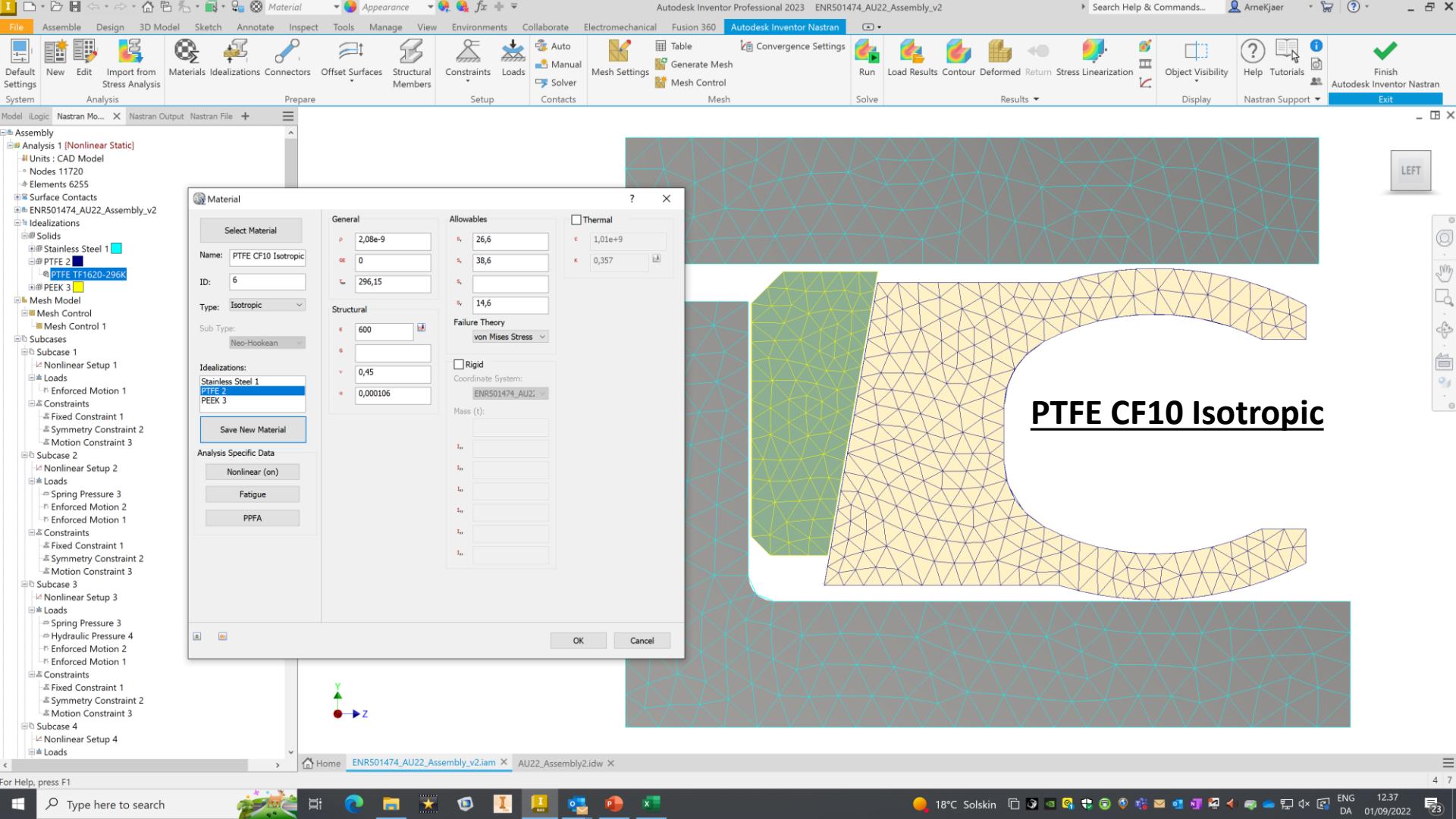
Products:

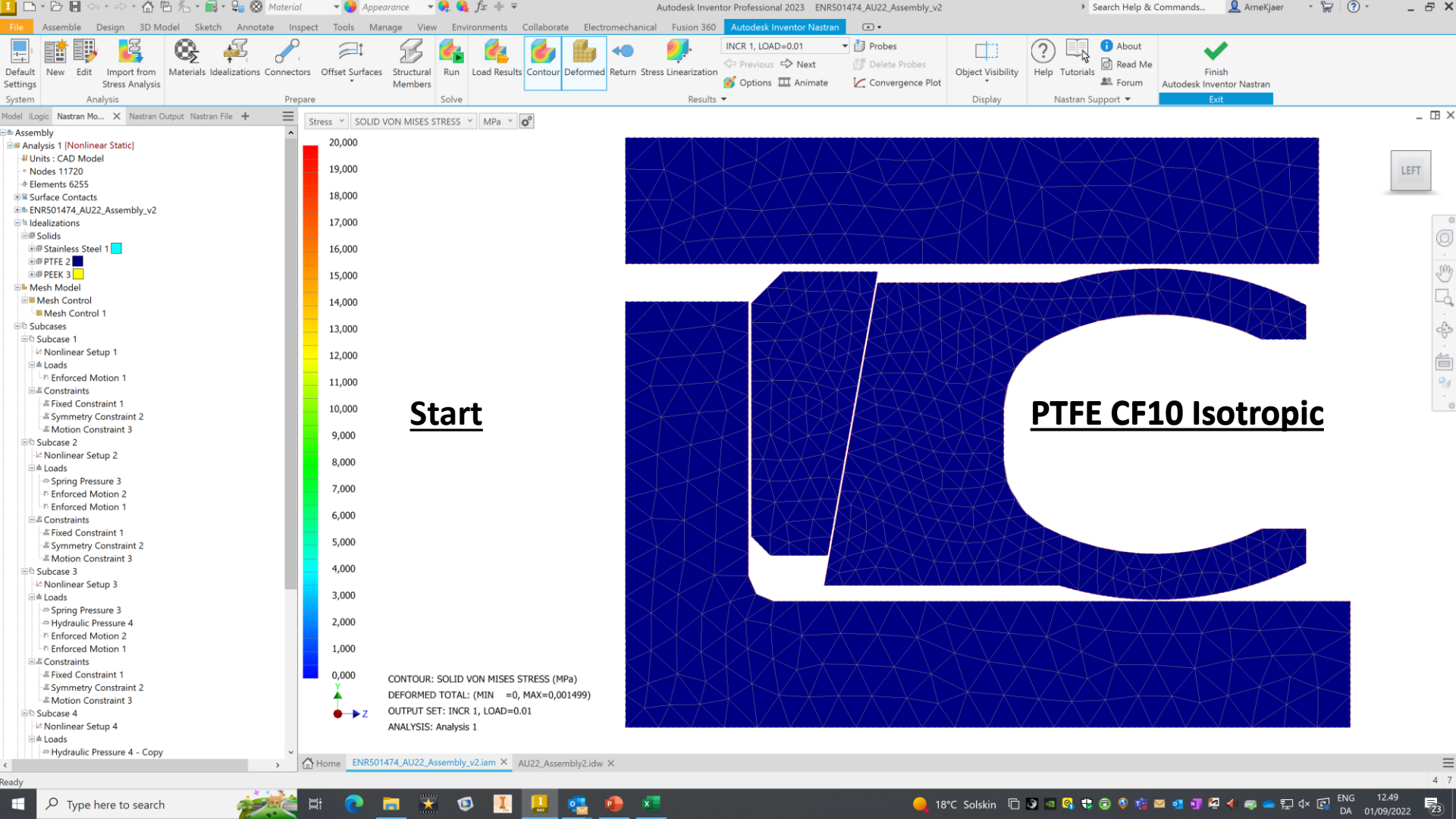
Fusion 360; Nastran; Inventor Nastran;

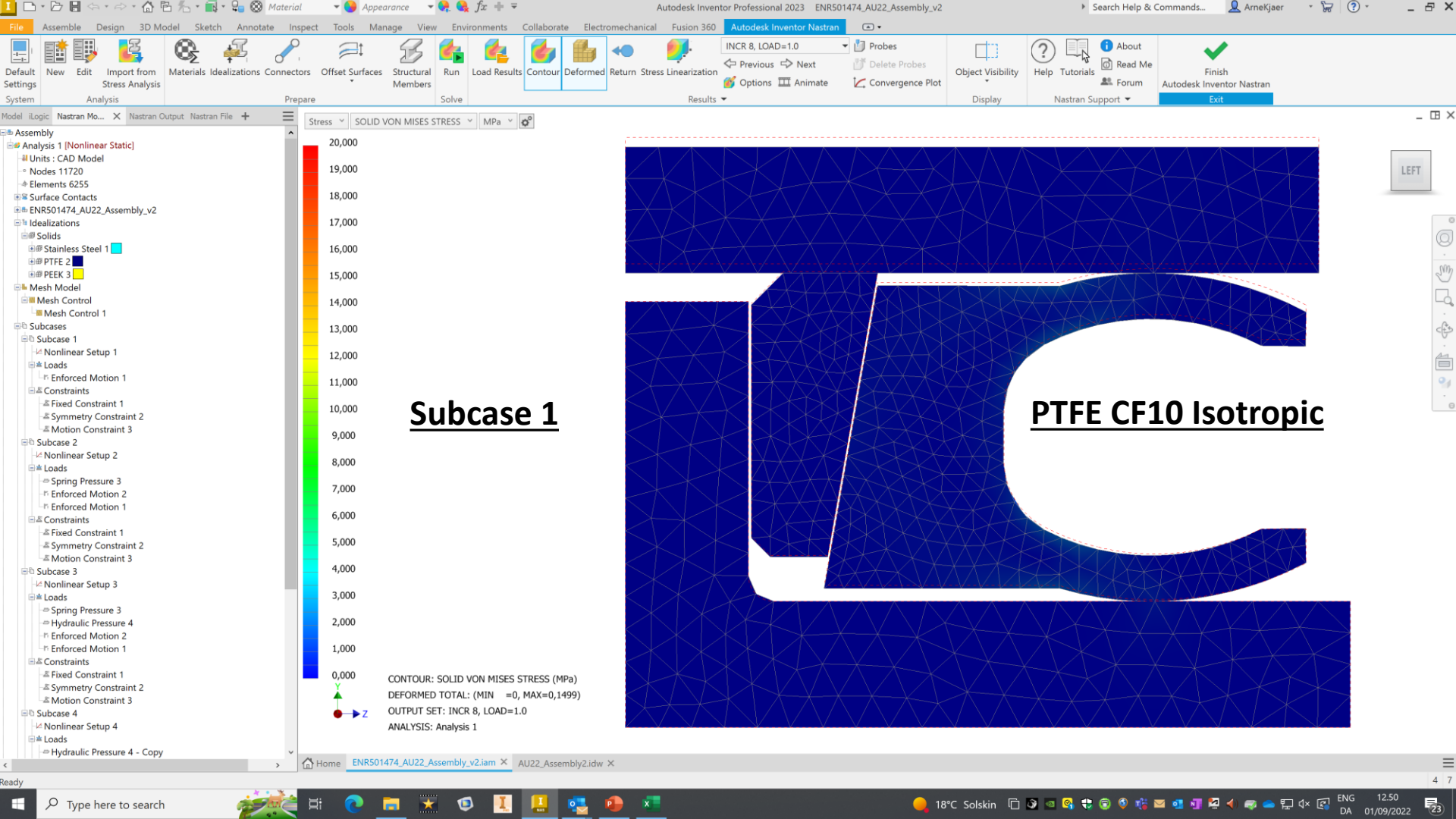
Versions:

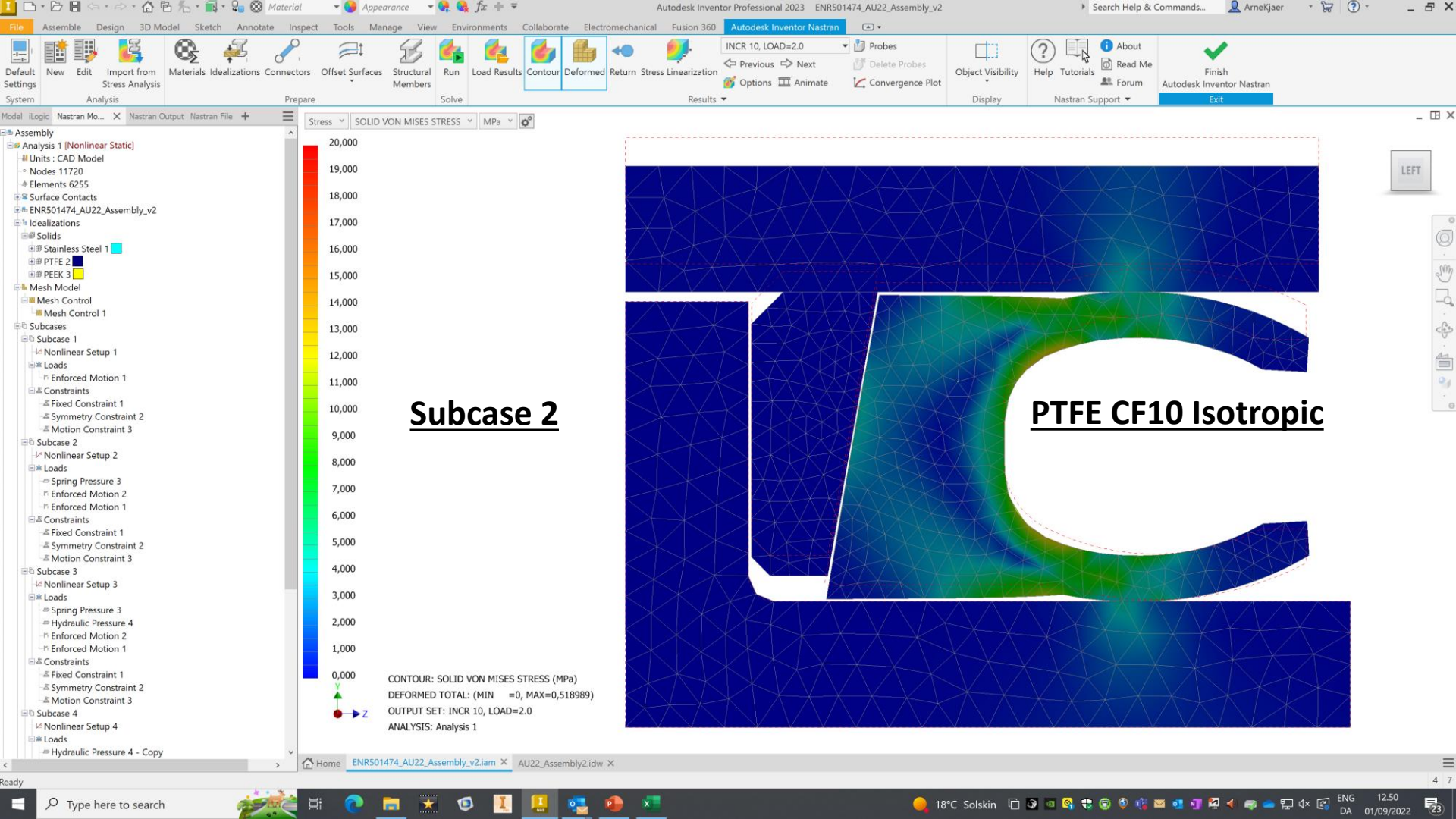
all;

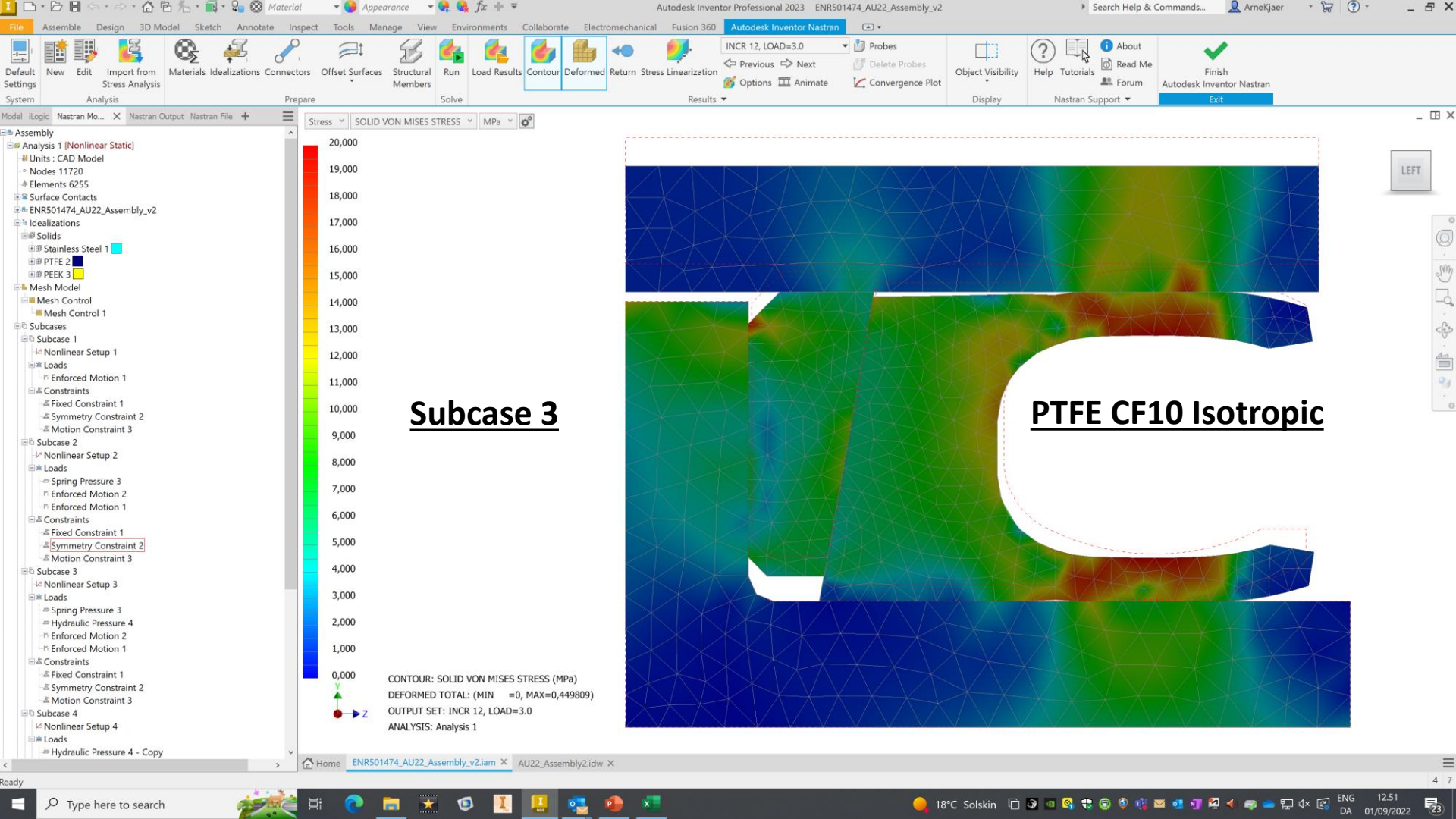
Final Run 1 and Run 2

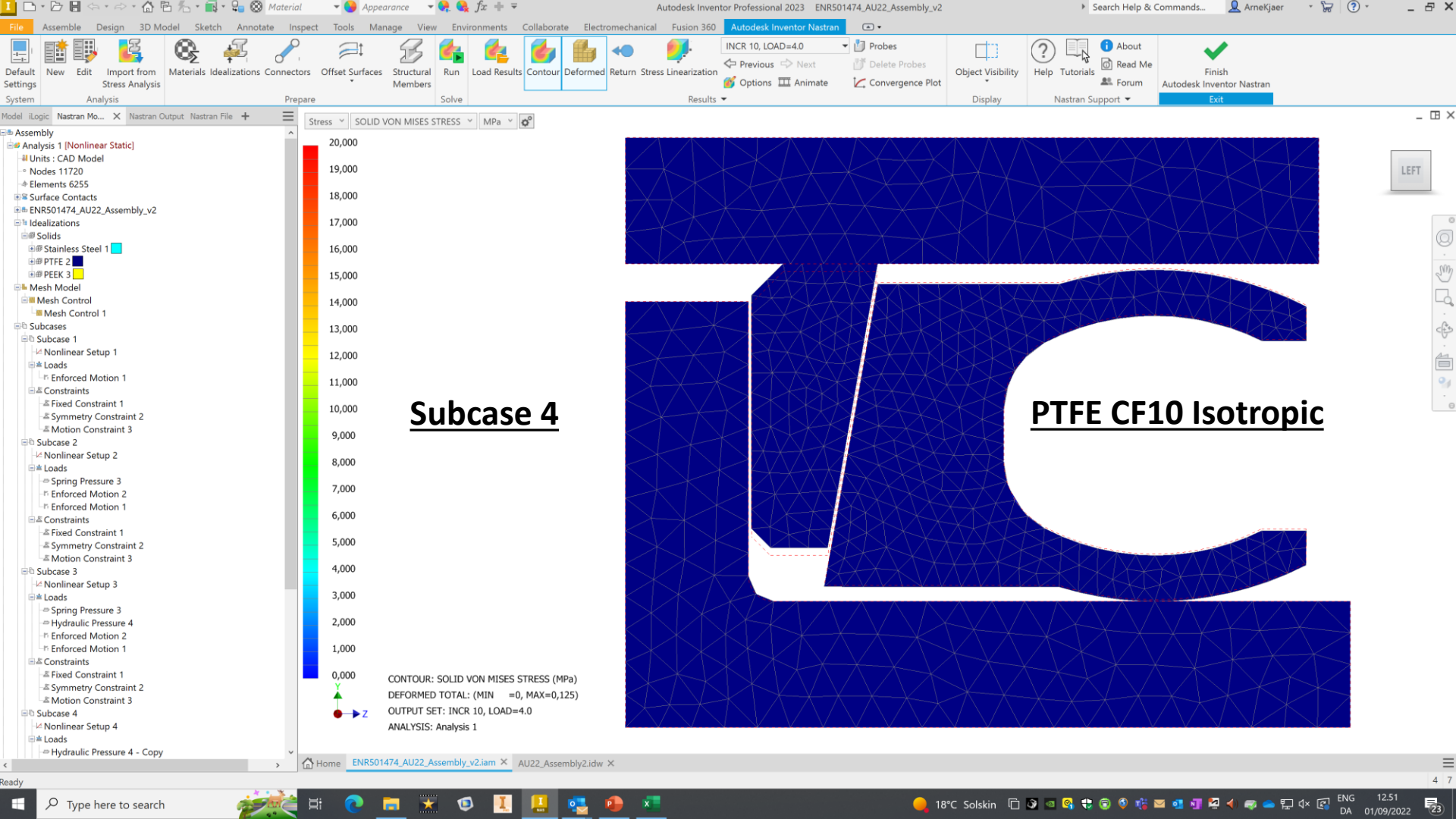


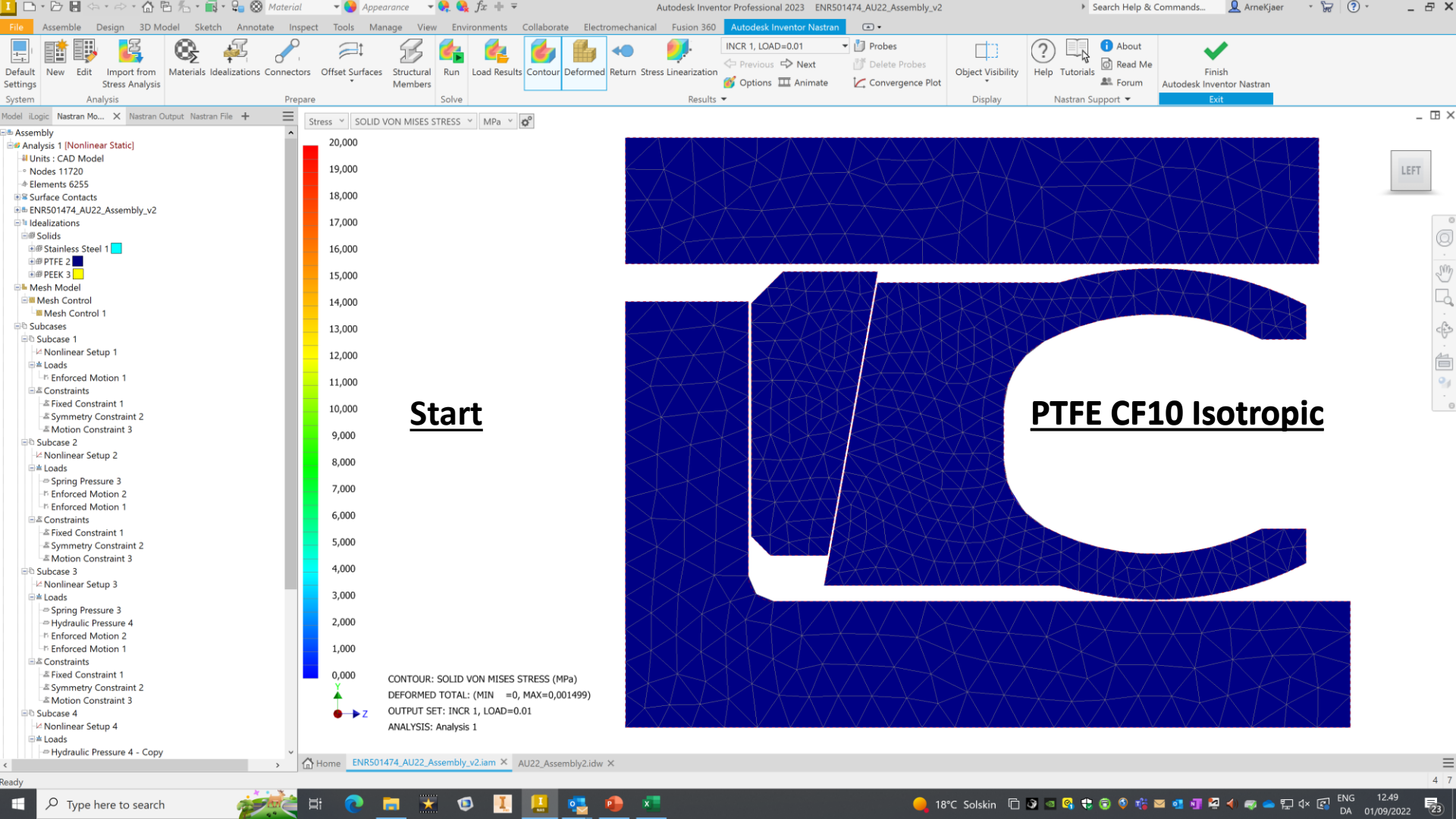


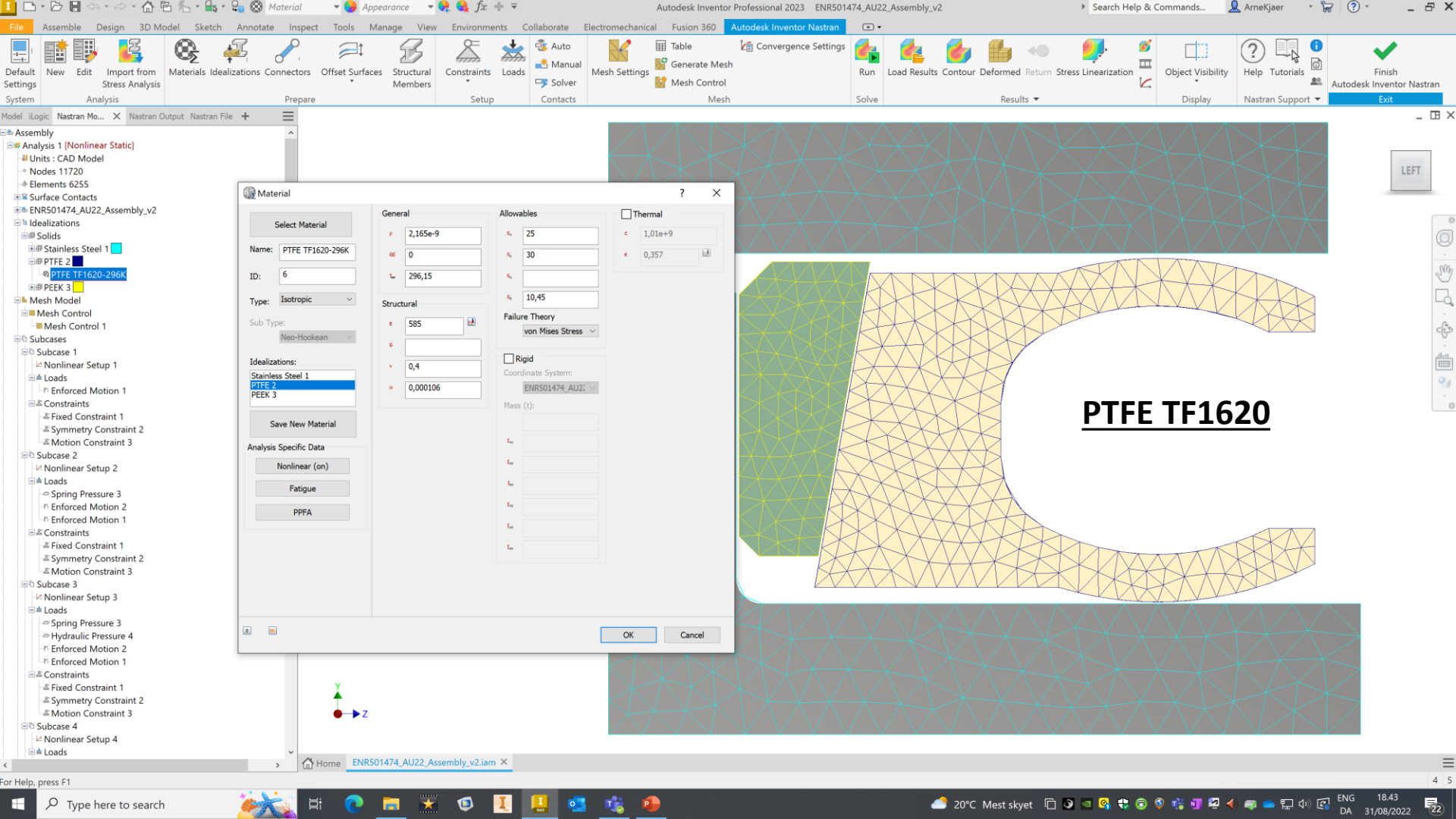


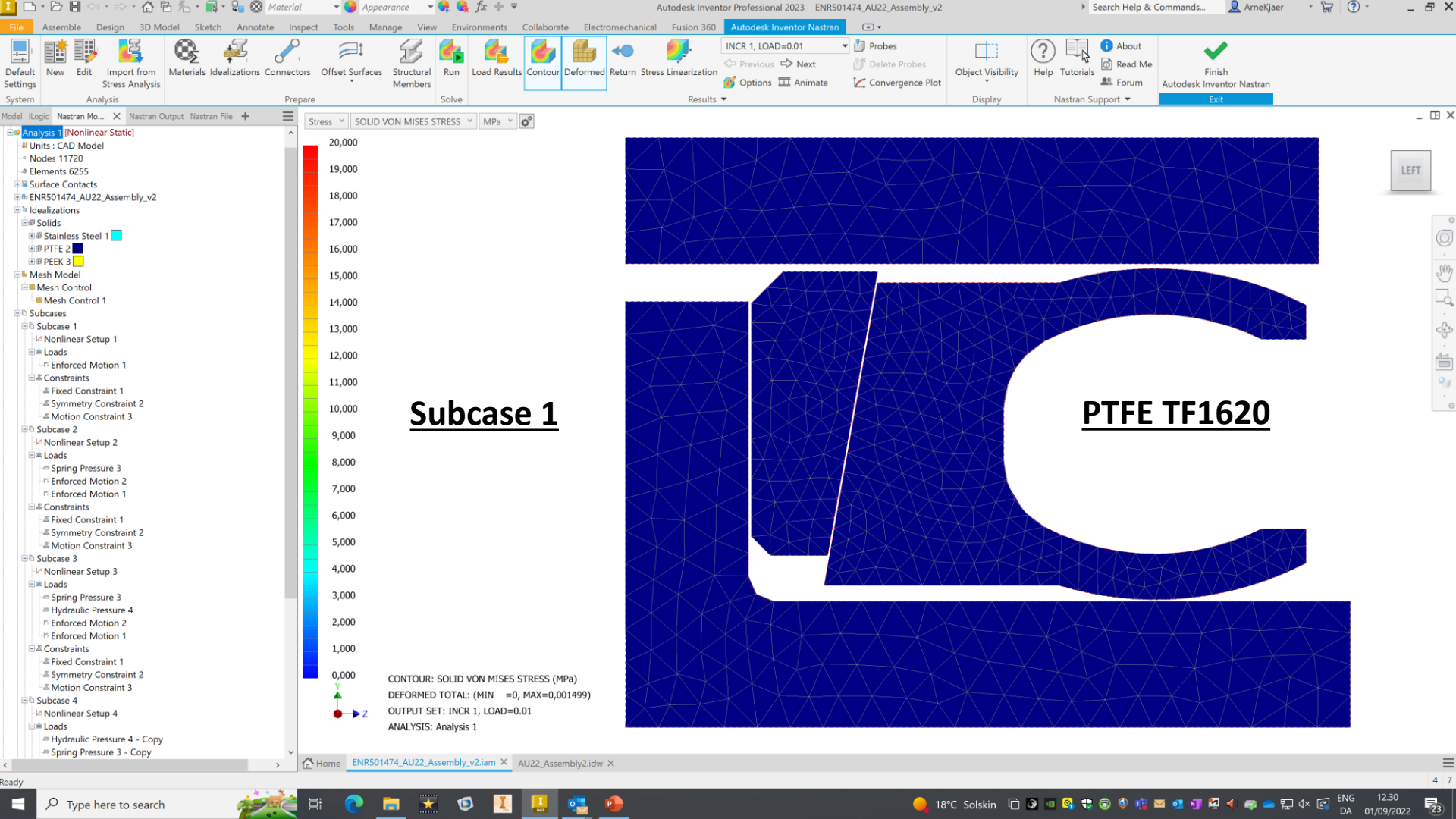


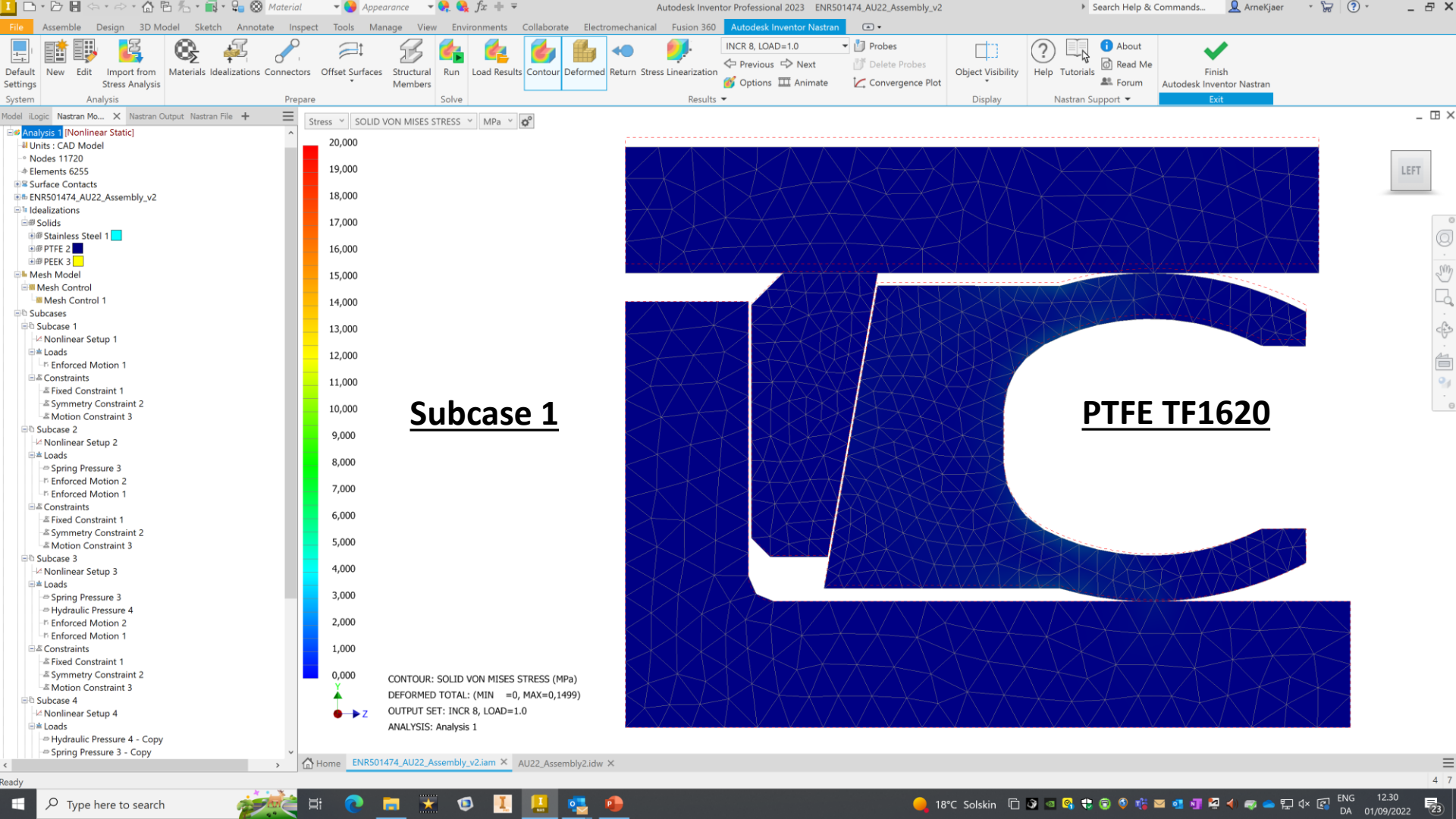


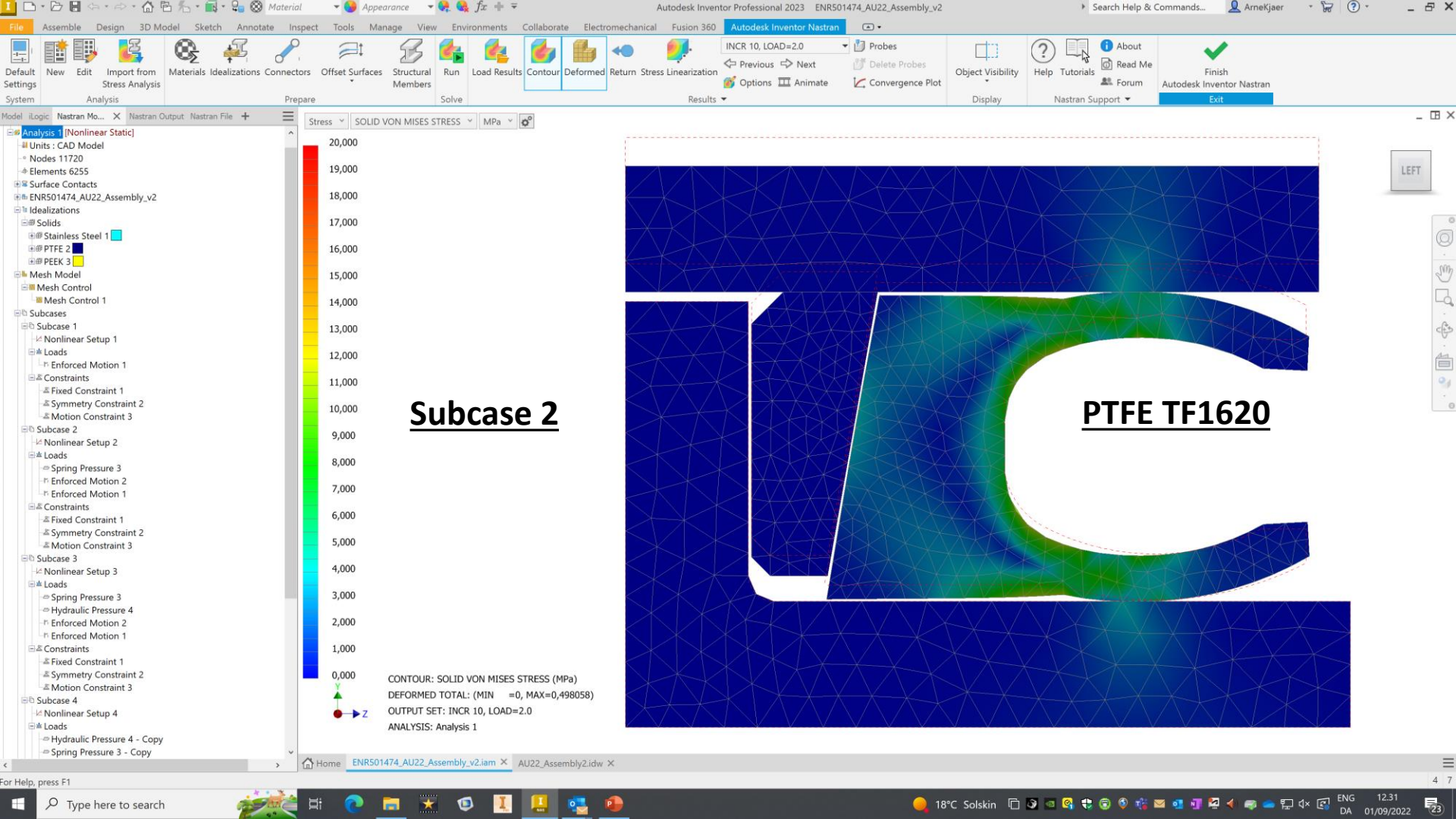


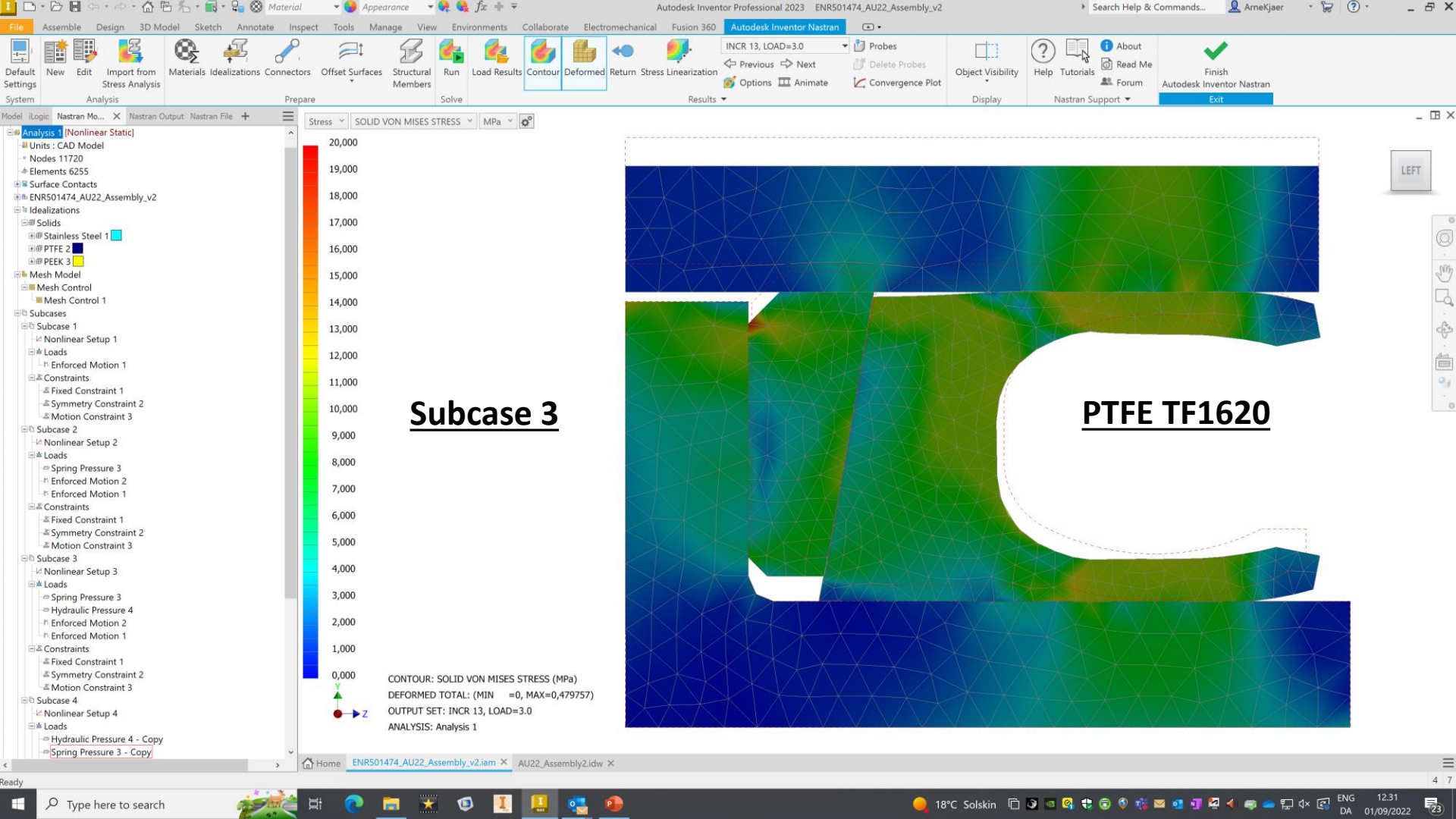


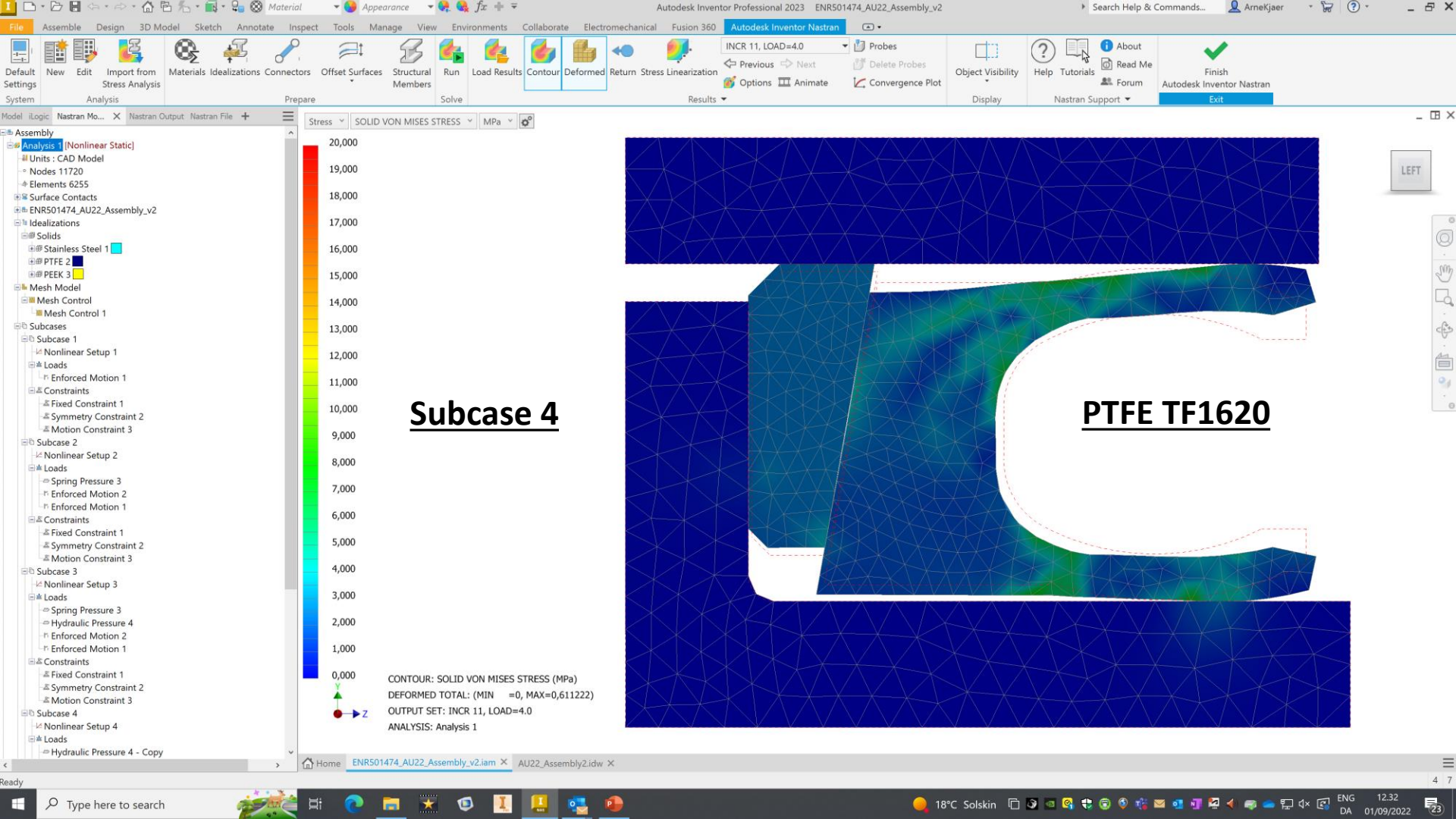


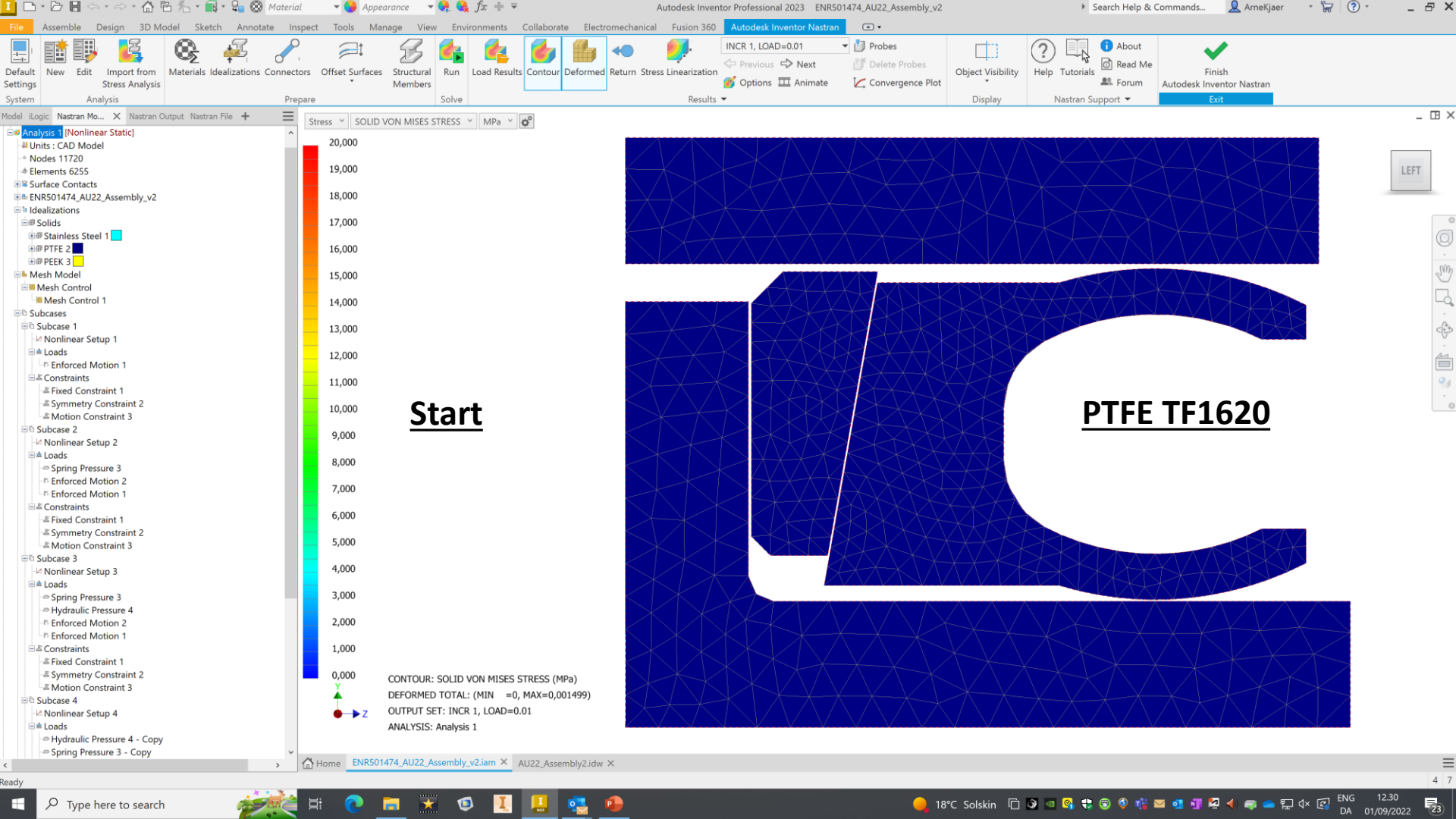


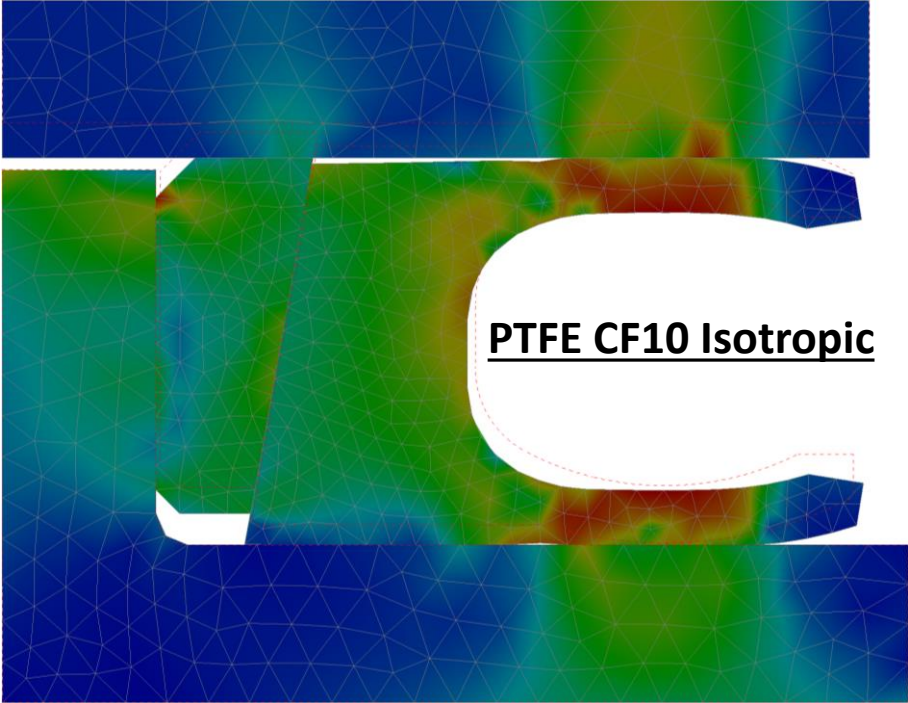













PTFE CF10 Isotropic



PTFE TF1620



PTFE CF10 Isotropic

A 3D model of a mechanical part, possibly a bracket or a connector, rendered with a blue triangular mesh. The part has a central white cutout. The text "PTFE CF10 Isotropic" is displayed in the center of the white cutout.



PTFE TF1620

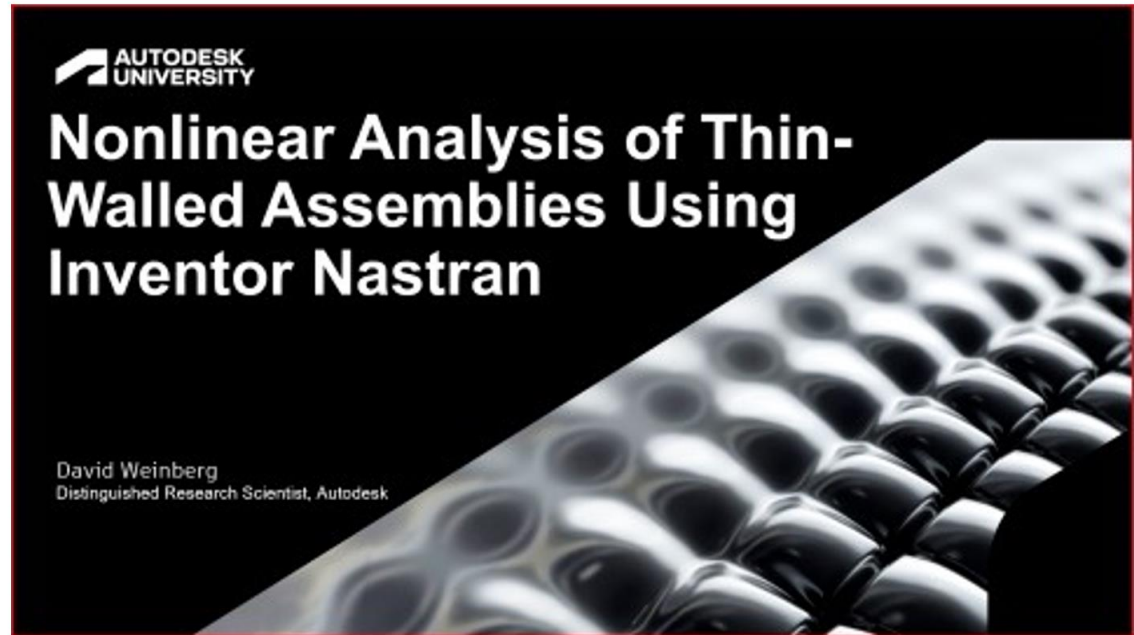
A 3D model of the same mechanical part as the left image, rendered with a blue triangular mesh. The part has a central white cutout. The text "PTFE TF1620" is displayed in the center of the white cutout. The model shows a green and yellow stress distribution on the right side of the part, indicating a different material property or loading condition compared to the left image.

**We are now happy to answer
your
QUESTIONS**



For More Information Please Attend...

- The Presentation will cover additional information on contact and nonlinear static analysis in Inventor Nastran
- Wednesday, 28 Sep, 430pm



Thank you



More Materials



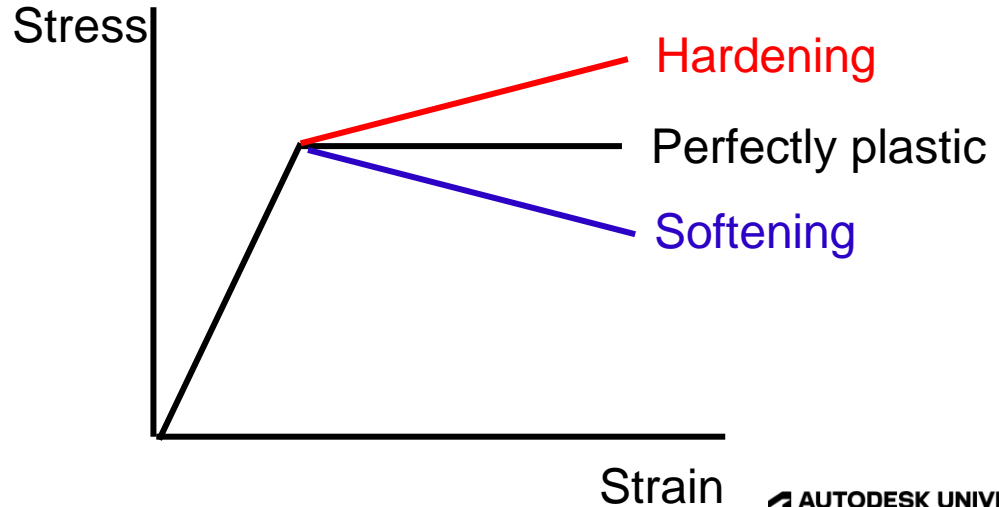
Strain Hardening, Work Hardening

- More stress is required to continue yielding
- Yield strength is a function of plastic strain
- Yield strength \sim Plastic strain

$\sigma_Y(\epsilon^p)$

↑

Hardening model



Isotropic hardening model

- Yield strength increases for both tension and compression
- Yield strength \sim Plastic strain

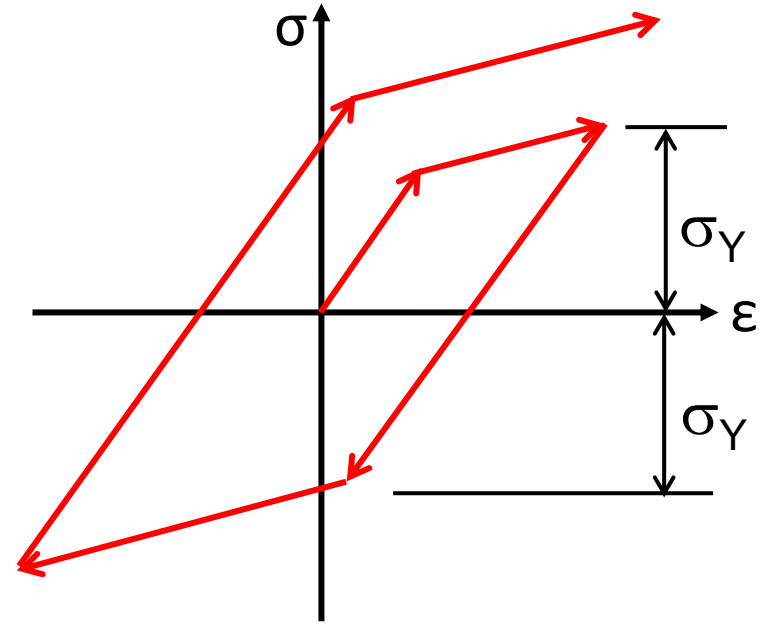
$$\sigma_Y(\varepsilon^p) = \sigma_Y^0 + H\varepsilon^p$$

Initial
yield strength

Plastic
modulus

- Yield condition

$$|\sigma| \leq \sigma_Y(\varepsilon^p)$$



Kinematic hardening model

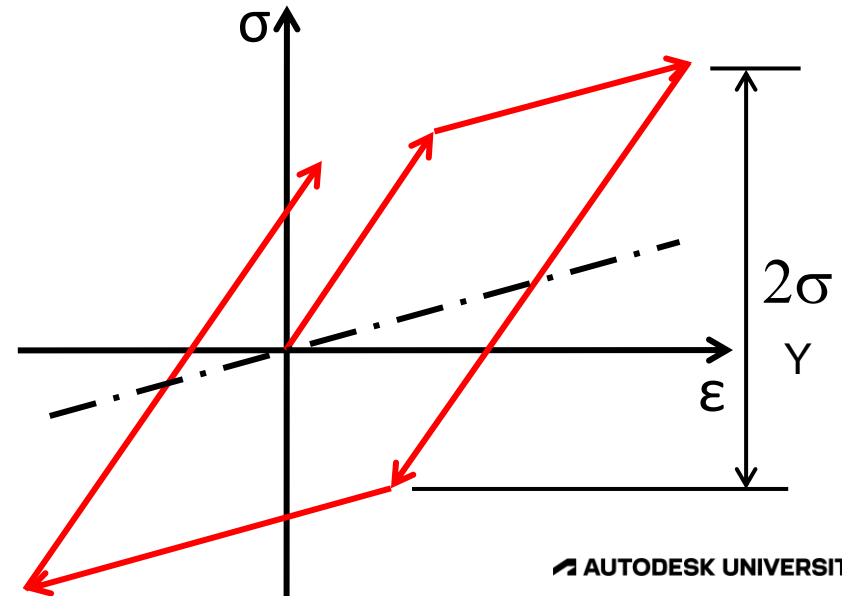
- The range of yield strength remains constant
- The center of yield strength moves along with plastic strain
- Center of yield ~ plastic strain

$$\alpha(\varepsilon^p) = H\varepsilon^p$$

Center of yield Plastic modulus

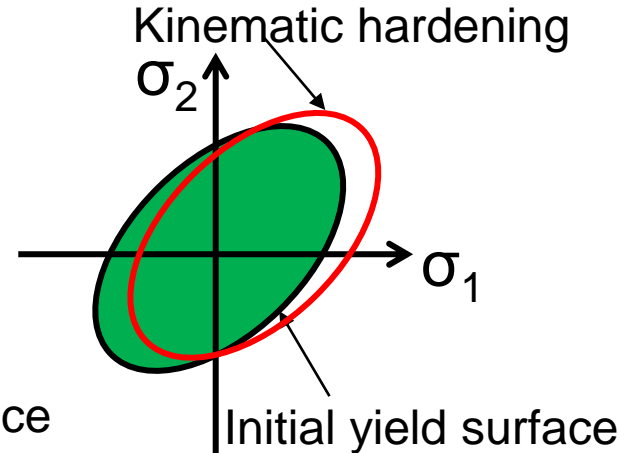
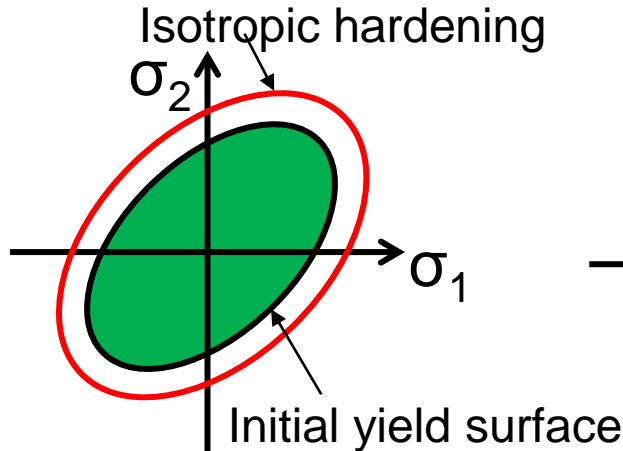
- Yield condition

$$|\sigma - \alpha(\varepsilon^p)| \leq \sigma_Y^0$$



Hardening model in 3D space

- Yield region as a surface (yield surface)
- Isotropic hardening: the radius of yield surface increases
- Kinematic hardening: the center of yield surface moves



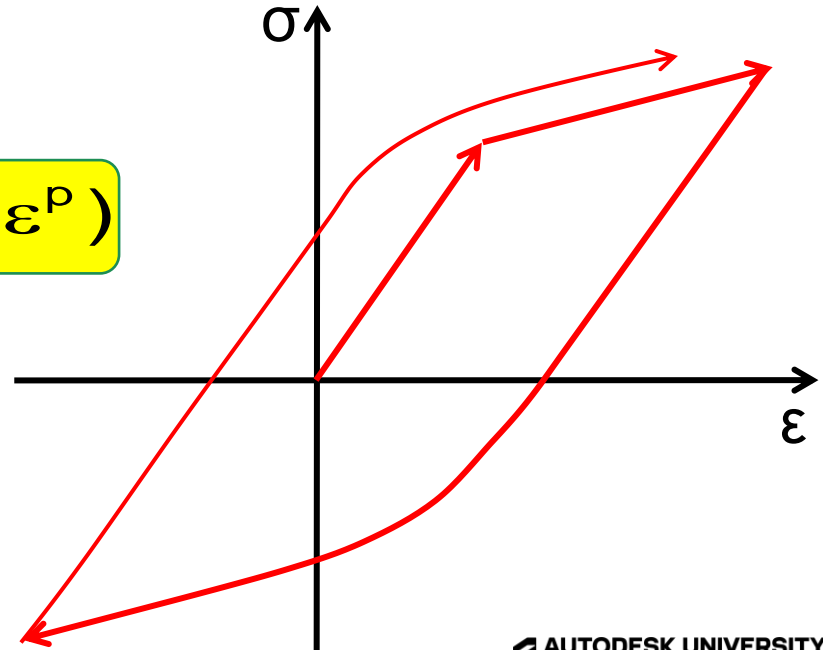
Bauschinger effect

- Many metals shows a reduced yield strength when loading direction changes
 - Due to the accumulation of dislocation
- Combined hardening model

$$|\sigma - \beta \alpha(\varepsilon^p)| \leq (1 - \beta) \sigma_Y(\varepsilon^p)$$

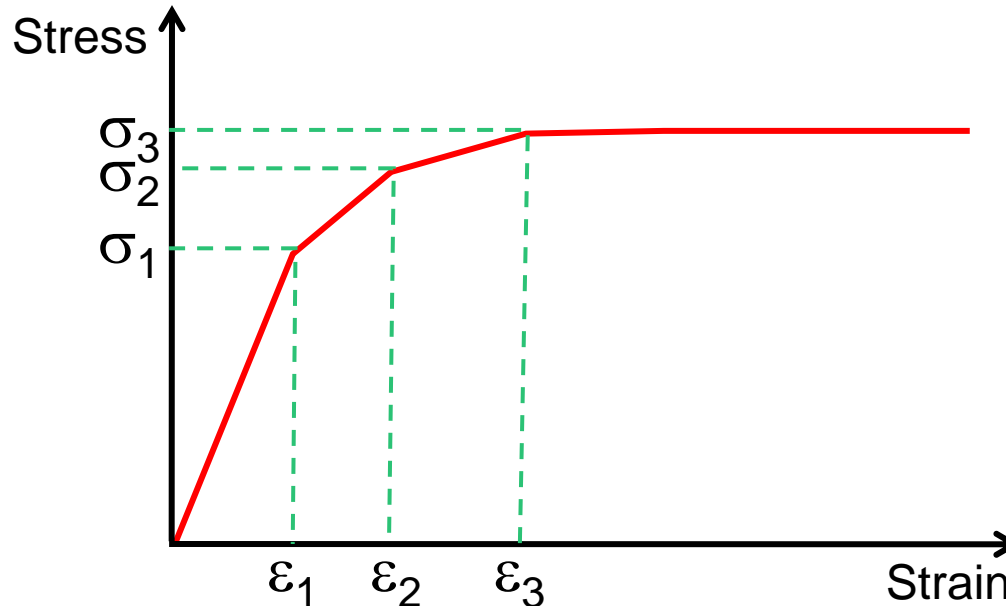
$$0 \leq \beta \leq 1$$

- $\beta = 0$: Isotropic hardening
- $\beta = 1$: Kinematic hardening



Strain-hardening model in Nastran

- Incrementally linear hardening model
- The slope of initial yield (ϵ_1, s_1) must be Young's modulus



Nastran Material Model from your own test data

Isotropic Plastic Material Model – Nastran Material Data Input

In order to build up your own polymer material model you will need some information's regarding your polymer material behavior

In this example I am showing here I build up a polymer material model representing, a PTFE material reinforced with Carbon Fiber

Most of the needed information's you will have to measure yourself or have a professional laboratory to measure the data for you

Here its very important to decide on how many different temperatures and testing speed you will need to measure in order to cover the range of your application

In order to have relevant information's we have also produced the test parts in order to have full knowledge about the production parameters which in many cases have an influence on the internal structure of the polymer and therefor also the strength

Nastran Material Model from your own test data

Isotropic Plastic Material Model – Nastran Material Data Input

General

- Mass Density
- Damping Coefficient
- Reference Temperature

Allowables

- Tensile Limit
- Compressive Limit
- Shear Limit
- Yield Limit

Structural

- Elastic Modulus (Table with Temperature Dependence)
- Shear Modulus calculated as $E/(2 \times \text{Poisson's Ratio})$
- Poisson's Ratio

Failure Theory

- None
- Von Mises Stress
- Principal Stress

Nastran Material Model from your own test data

Isotropic Plastic Material Model – Nastran Material Data Input

Thermal

- Specific Heat
- Thermal conductivity

Nastran Material Model from your own test data

Isotropic Plastic Material Model – Nastran Material Data Input

Hardening Rule

- Isotropic
- Kinematic
- Isotropic + Kinematic

Nonlinear

- None
- Nonlinear Elastic
- Elasto-Plastic (Bi-Linear)
- Plastic

Yield Criterion

- Von Mises
- Tresca
- Mohr – Coulomb
- Drucker – Prager

Data Input

Strain

0

Yield

xxx

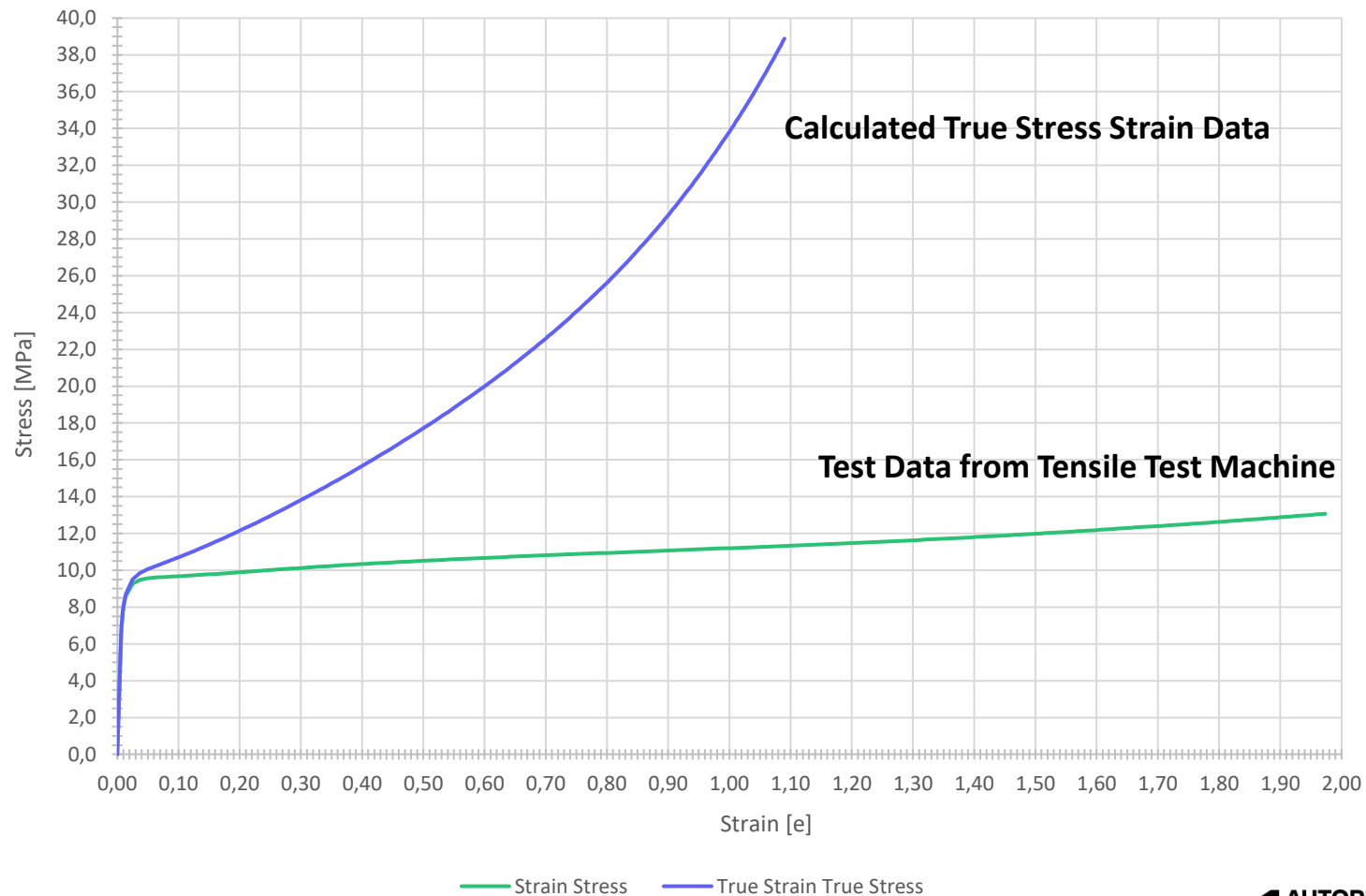
Stress

0

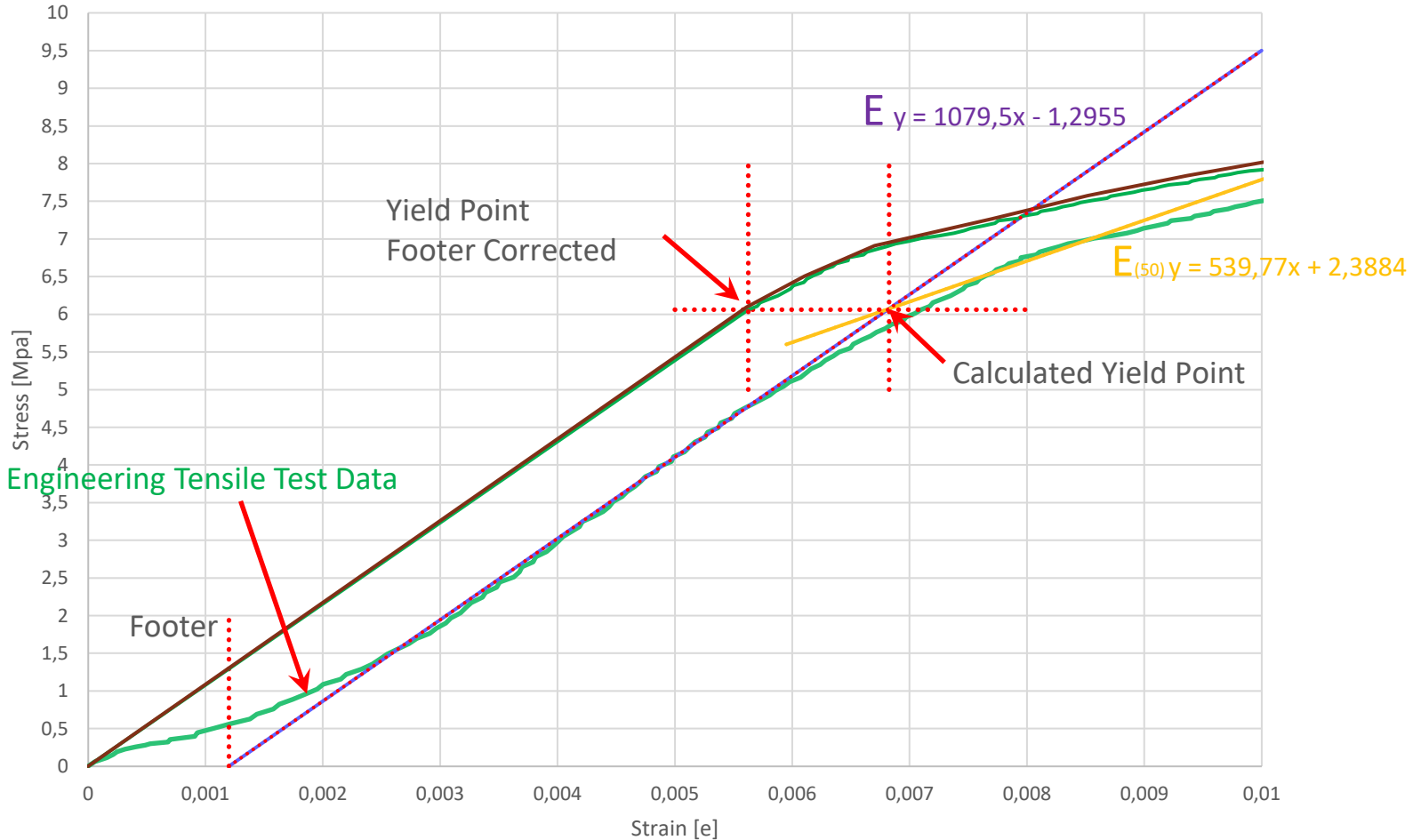
Yield

yyy

PTFE Reinforced 23°C ; Strain Rate 0,01 s⁻¹ ; Isotropic Elastoplastic material model



PTFE Reinforced 23°C ; Strain Rate 0,01 s⁻¹ ; Elastoplastic material model



Nastran Material Model from your own test data

Isotropic Plastic Material Model

- Using your Engineering Tensile Test Data measured at a temperature and strain rate
- Insert the data in an empty Excel Sheet and make a graph of the stress strain curve
- Overlay the curve with a line to illustrate the Youngs Modulus or Elastic Modulus
- Make a line with (I typically us 50% of the Elastic Modulus) as tangent to the measured curve
- Excel can show you the mathematic of the two lines and from those you calculate the crossing point between the lines this is the calculated Yield Point
- Also calculate the Elastic modulus lines crossing at $y=0$, this it the footer
- Now you correct the measured data with the footer offset

Nastran Material Model from your own test data

Isotropic Plastic Material Model

- Now you correct the measured data with the footer offset and make the first point @ 0;0 and the second point as the corrected Yield Point
- The rest of the curve I typically reduce to have only 1 point for each 100 measured points
- I then calculates the Trues Stress Strain curve using the recognized transformation
- True Strain = $\text{LN}(1 + \text{Engineering Strain})$
- Trues Stress = Engineering Stress * $(1 + \text{Engineering Strain})$
- The Nastran Input will then be Trues Strain ; True Stress

Thank you

