

The background features a complex, organic, grey mesh-like structure that resembles a biological or architectural form. A solid blue horizontal band runs across the middle of the image, serving as a backdrop for the text.

Ease the Stress

Wasim Younis
Simulation Manager

Join the conversation [#AULondon](#)

I do not need Simulation


My products are too simple to need Simulation



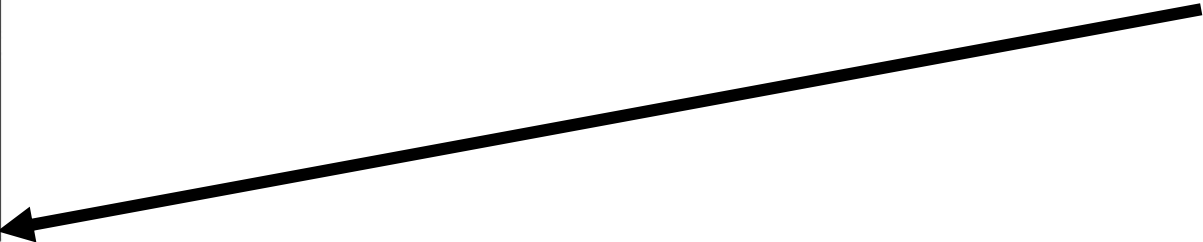
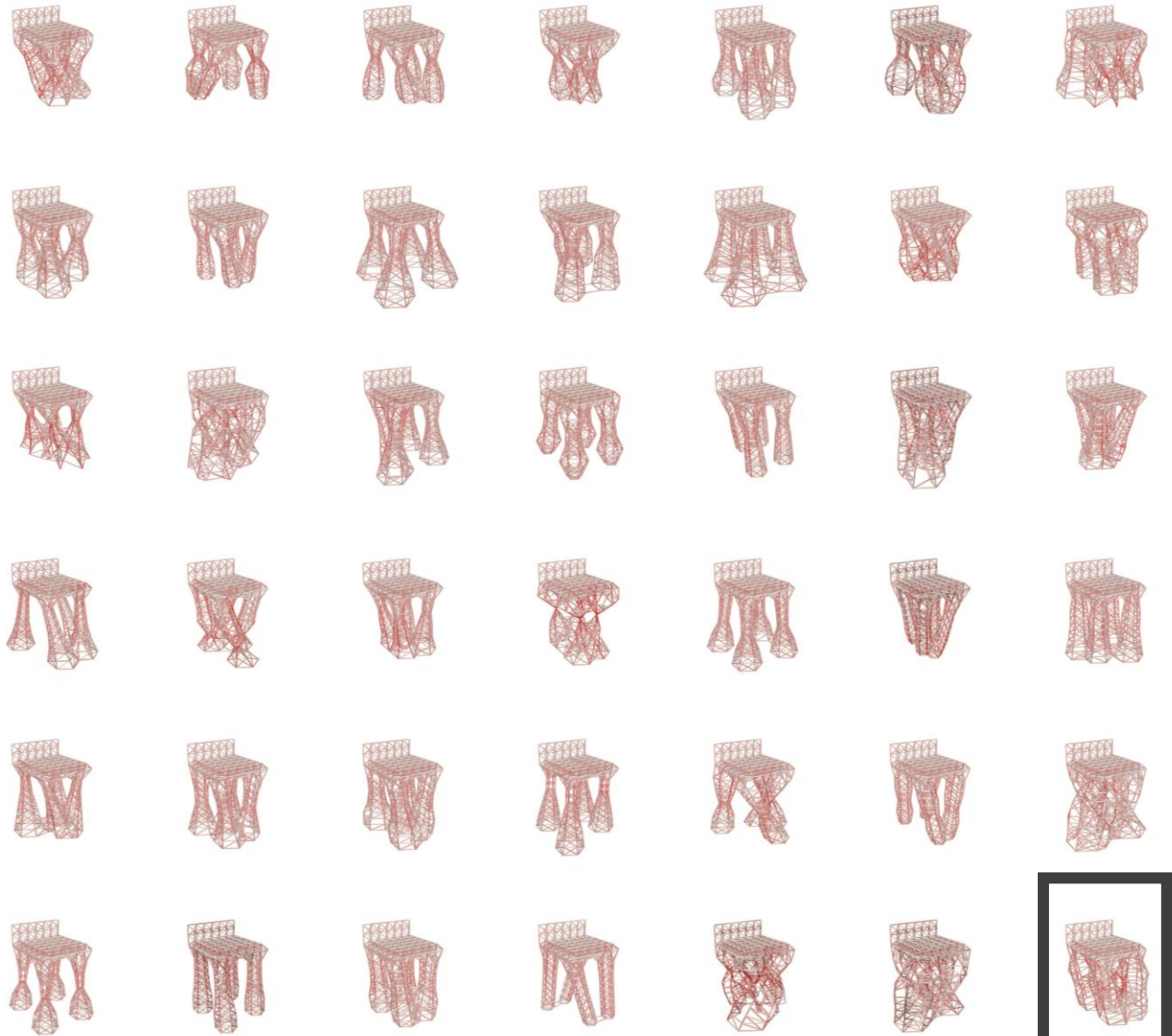
MODEL 1
Solid bars
Traditional design
Weight:
10.3 kilograms
Displacement:
0.8 micrometers



MODEL 2
Uniform lattice
Smart design with ALM
Weight:
... **4.1 kilograms**
Displacement:
... **4.2 micrometers**



MODEL 3
Evolved lattice
Evolutionary design with ALM
Weight:
.... **2.9 kilograms**
Displacement:
.... **6.1 micrometers**




Simulation is too Expensive



Autodesk Inventor Simulation
+ Shape Generator

Is included in Inventor Professional



Autodesk Fusion 360

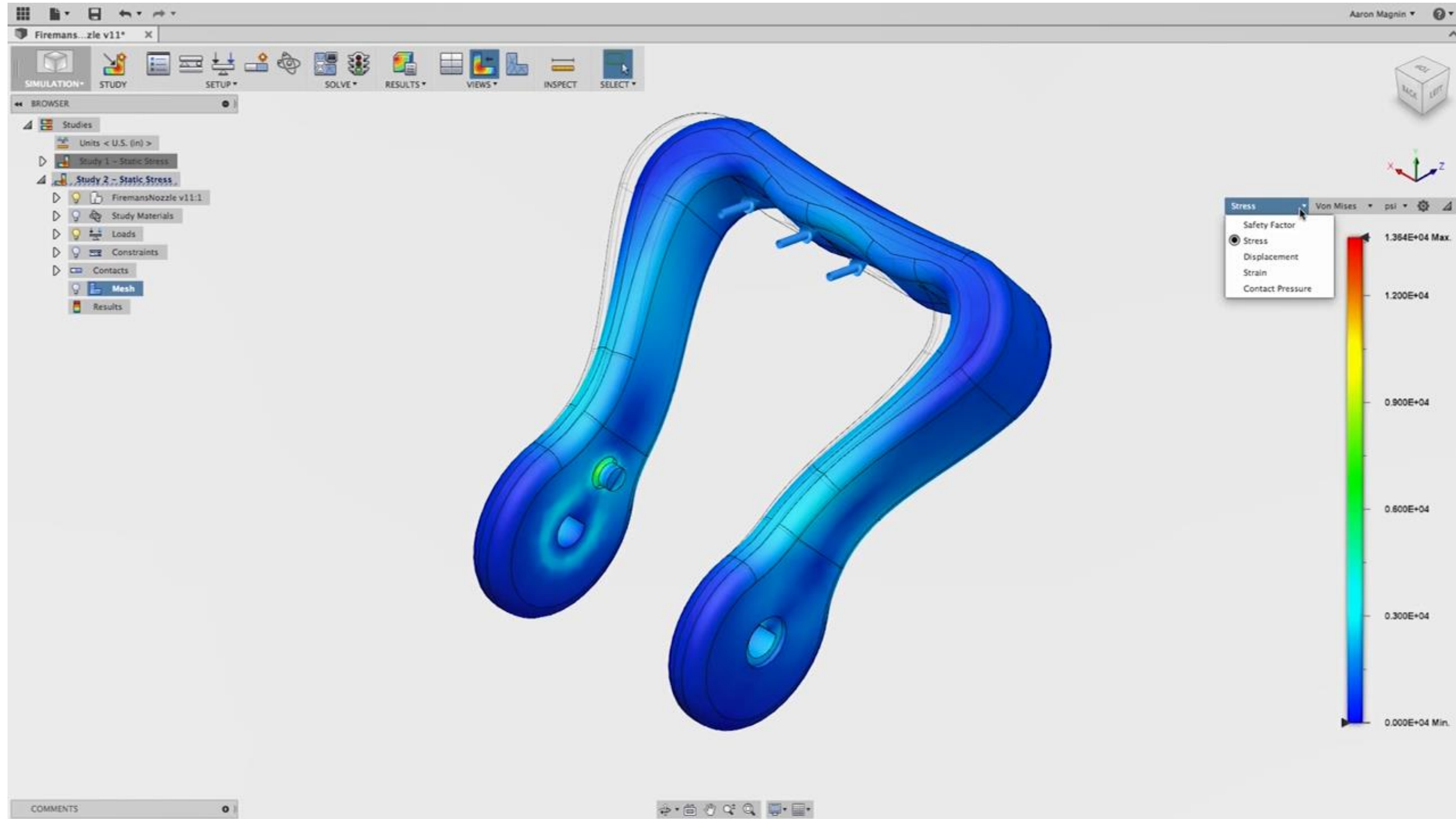
£276/year to £1,350/year



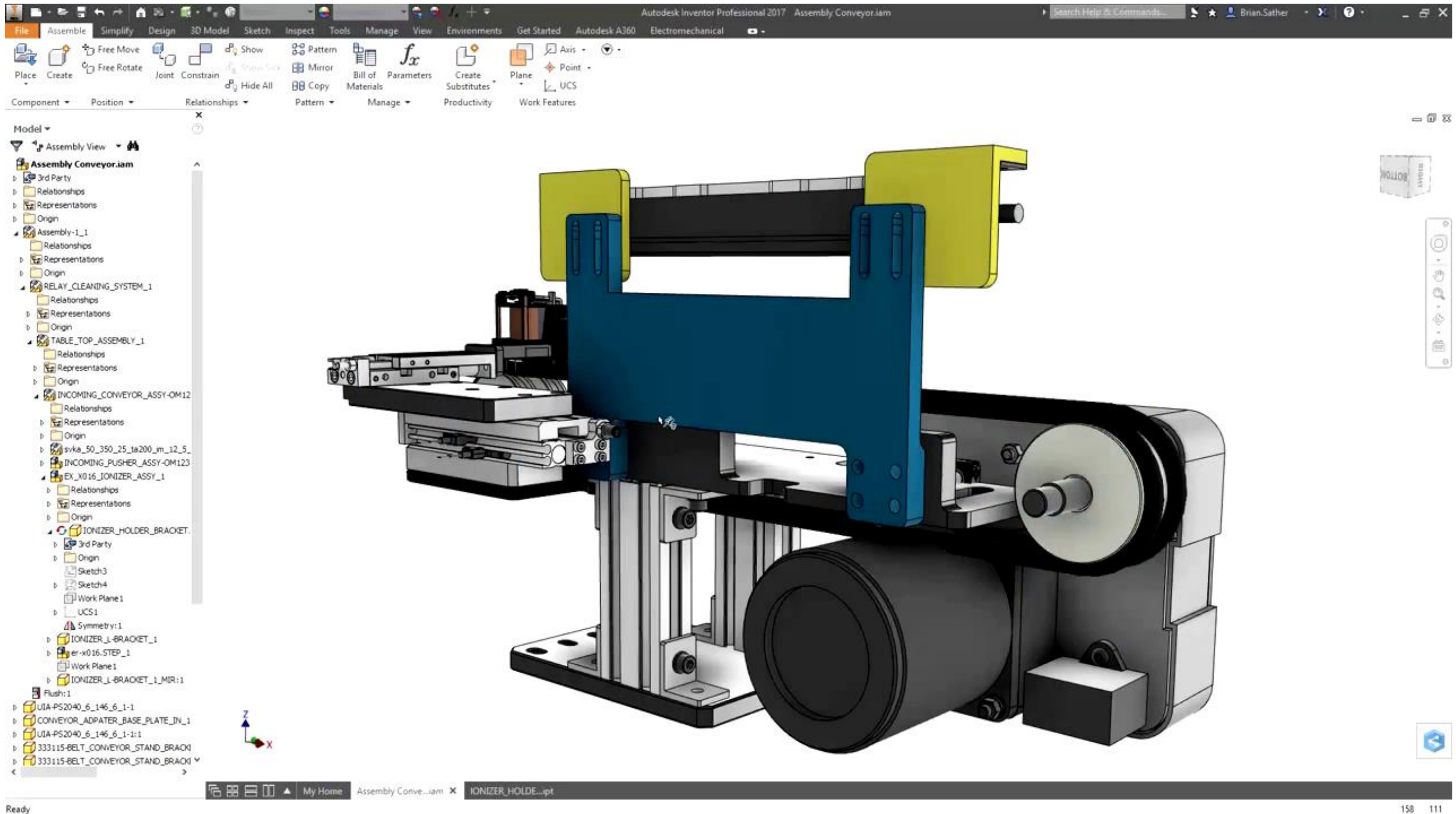
Autodesk® Nastran® In-CAD

£3325/year

Simulation is Difficult



Simulation is only for predicting failure

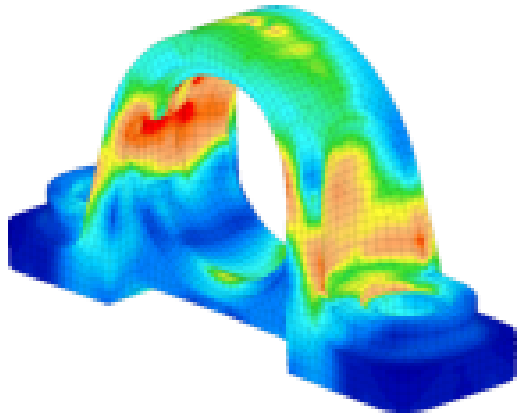


So lets look at solutions available today

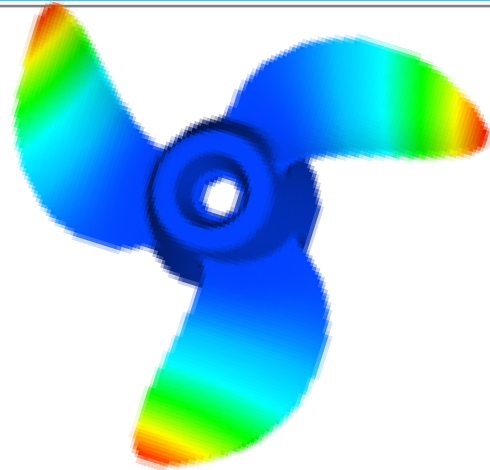
To help us make better informed decisions

Inventor Simulation - Capabilities

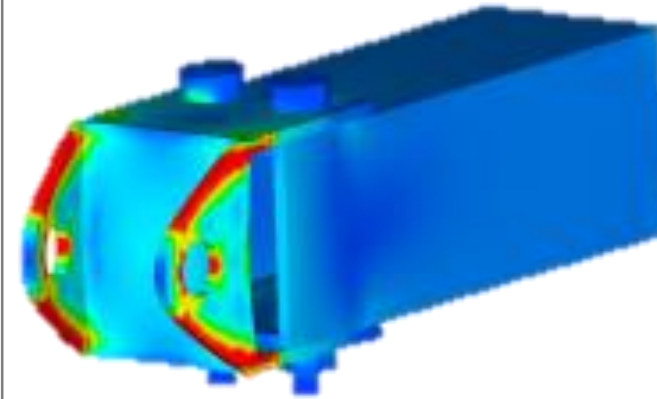
Linear Statics



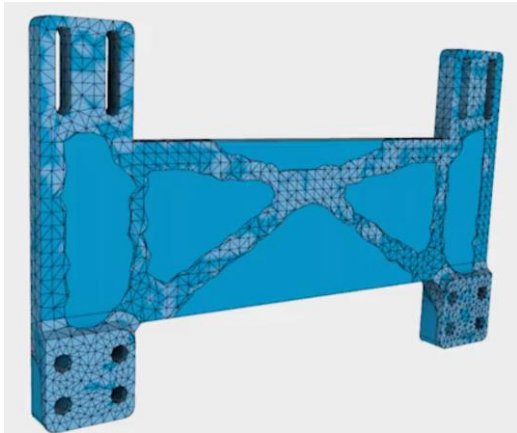
Normal Modes



Assembly Modeling with
Contact – No friction

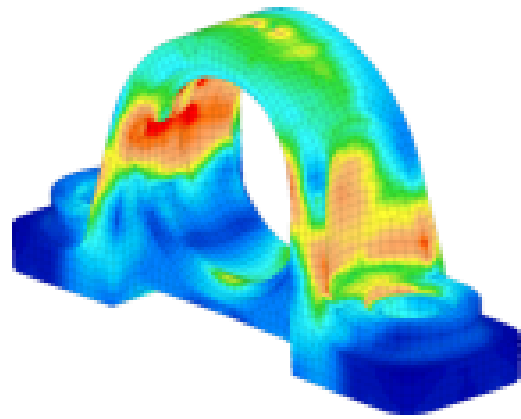


Shape Generator

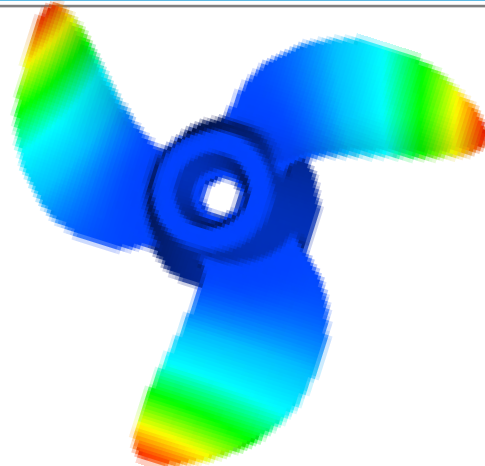


Nastran In-CAD - Capabilities

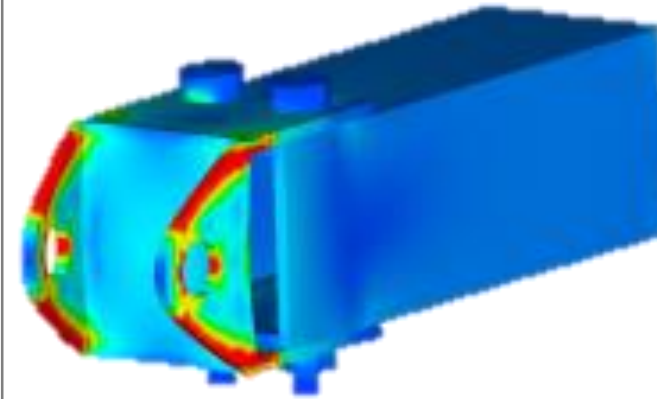
Linear Statics



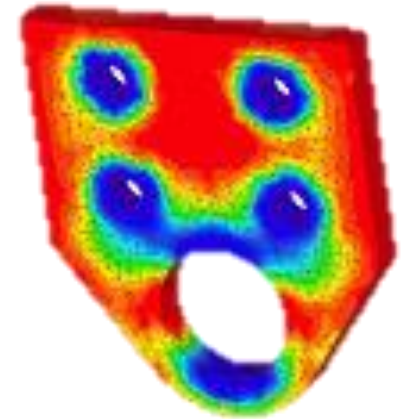
Normal Modes



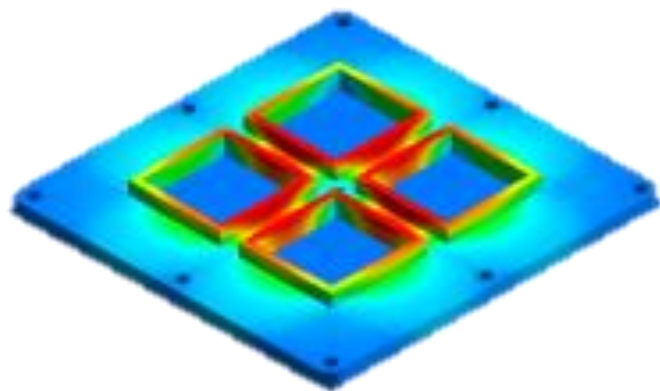
Assembly Modeling with Contact – with friction



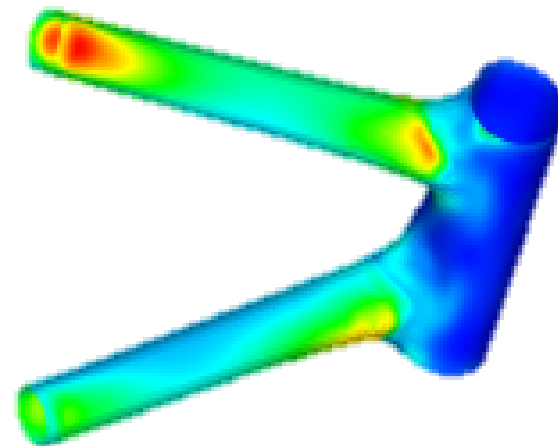
Pre-stress Static and Normal Modes



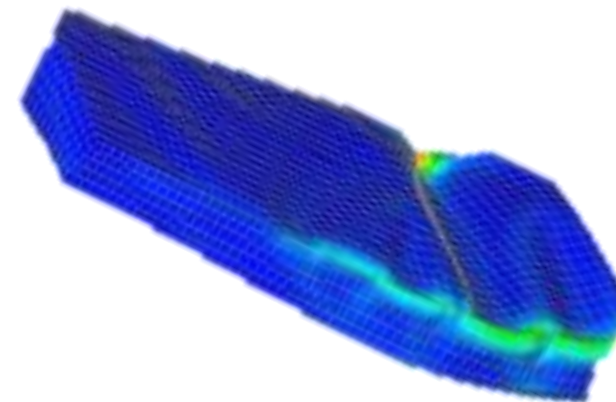
Linear Steady State Heat Transfer



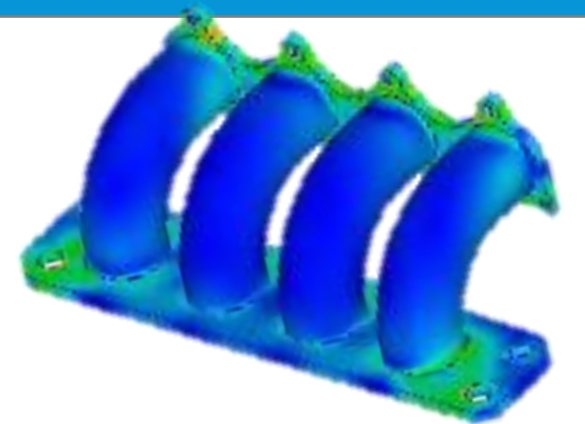
Composites



Buckling

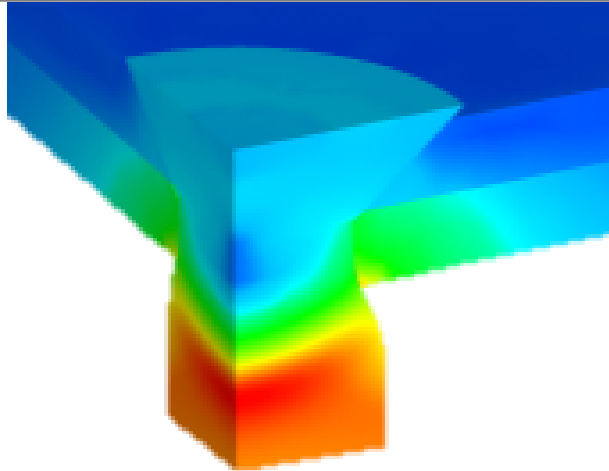


Thermal Stress

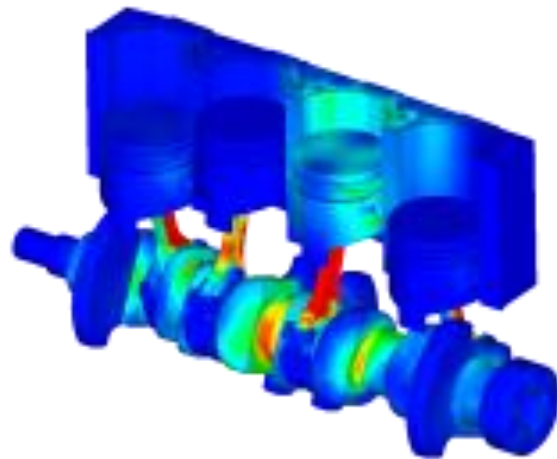


Nastran In-CAD - Capabilities

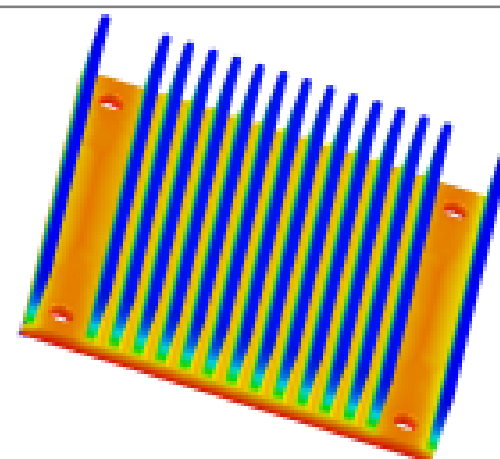
Nonlinear Statics



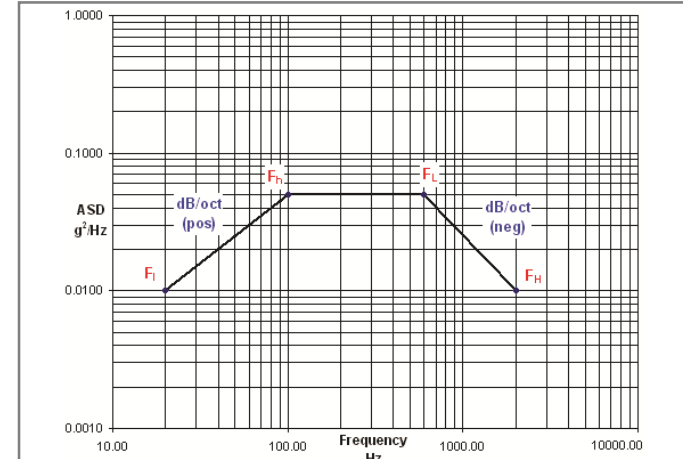
Nonlinear Transient Heat Transfer



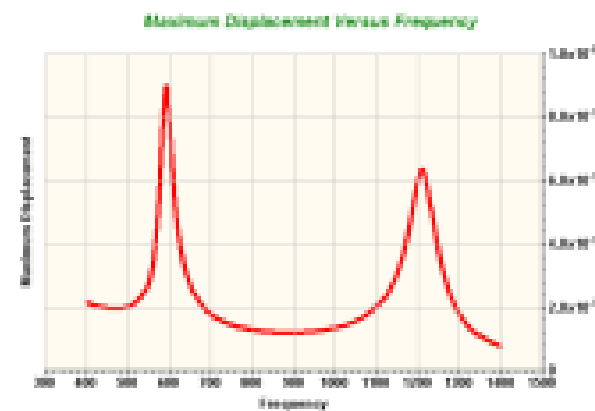
Nonlinear Steady State Heat Transfer



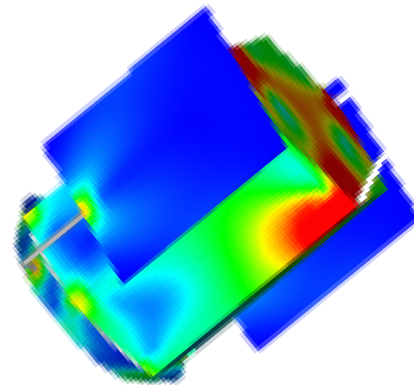
Random Response



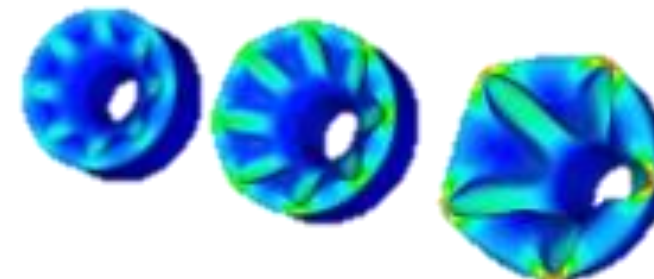
Frequency Response



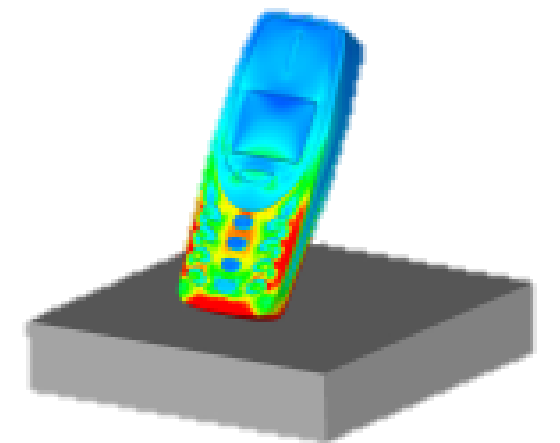
Linear and Nonlinear Transient Response



Advanced Nonlinear and Hyperelastic Materials

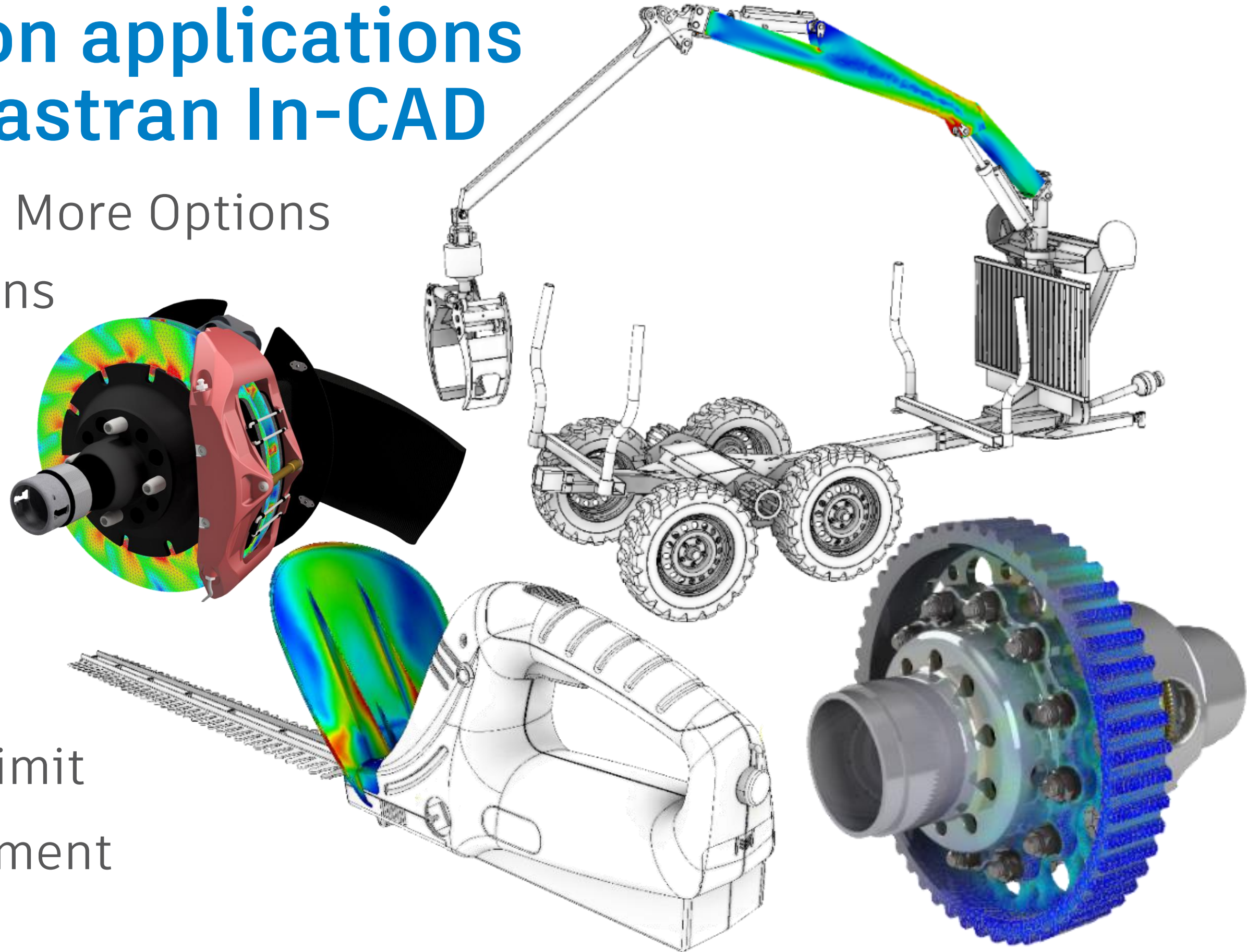


Automated Impact Analysis (AIA) and Drop Test

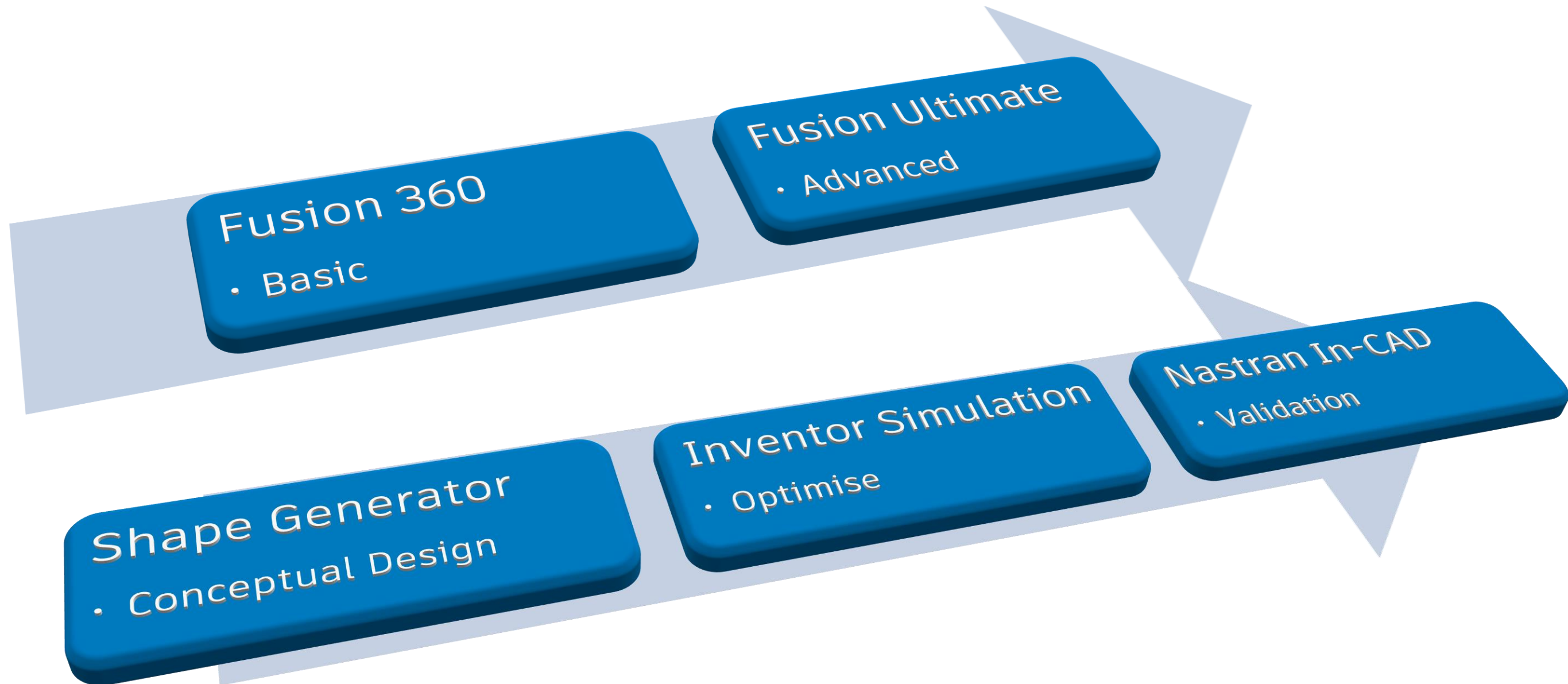


Some common applications to move to Nastran In-CAD

- Linear Analysis – More Options
- Bolted Connections
- Buckling
- Thermal Stress
- Fatigue
- Drop-test
- Non-Linear
 - Beyond Yield Limit
 - Large Displacement



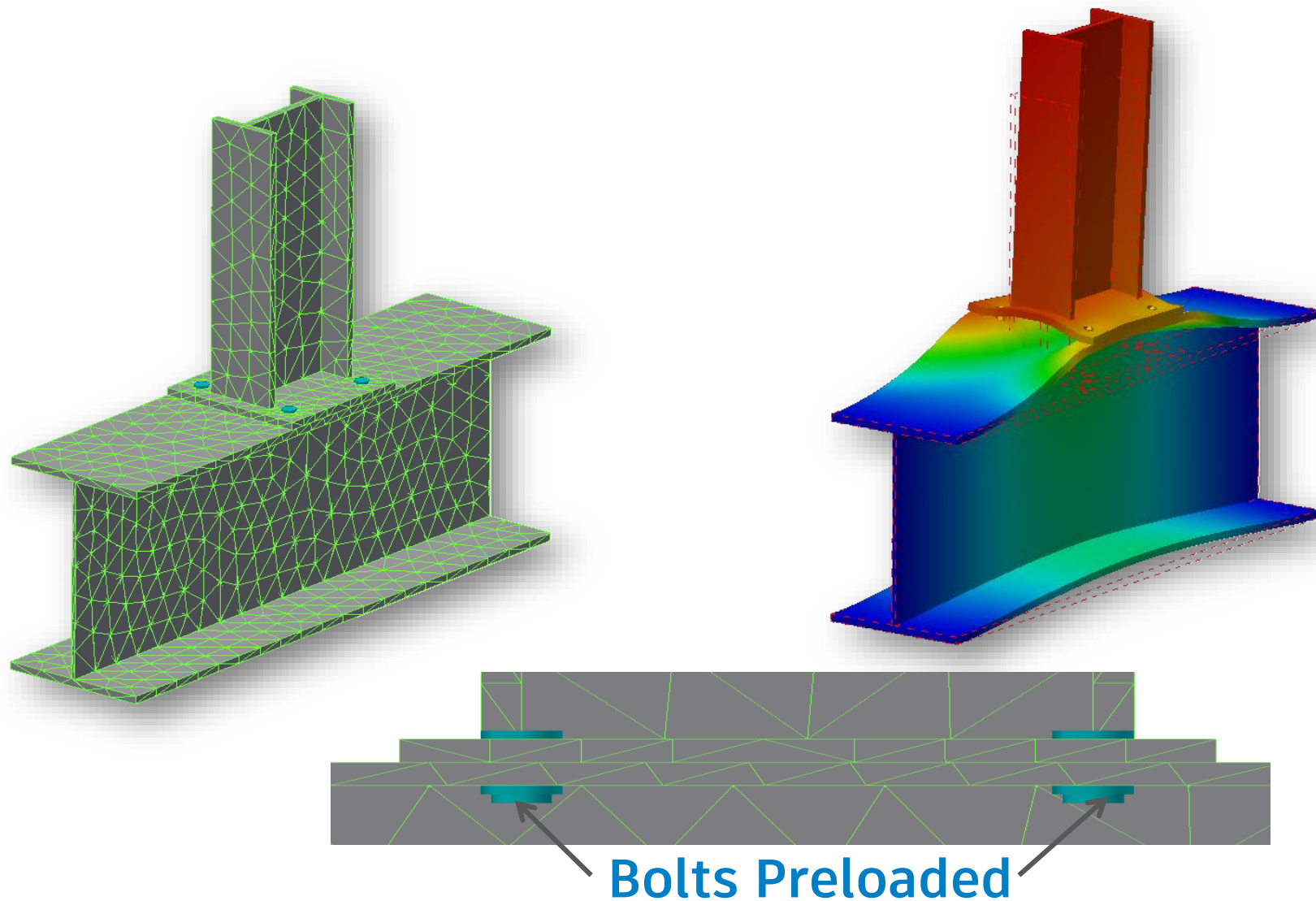
Technologies to help design with confidence



Technologies to help design with confidence

Design Example – DEMO

Inventor Simulation + Nastran In-CAD



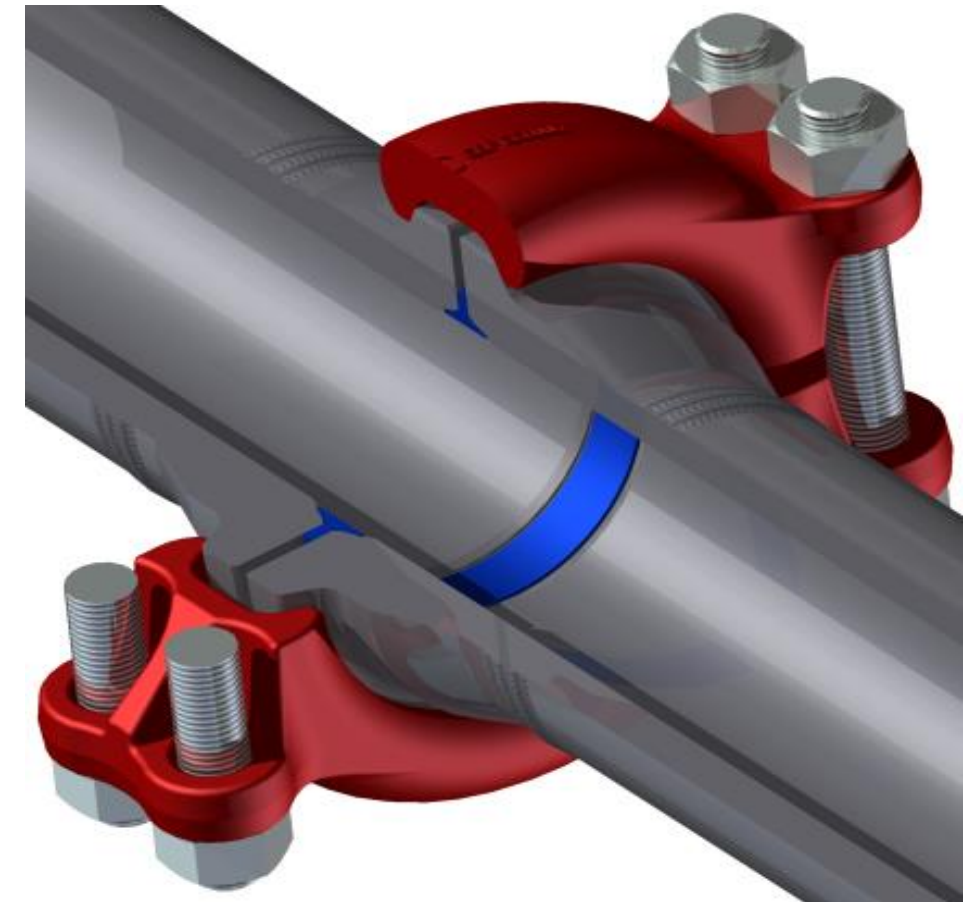
Some Customer Examples

How they have used simulation to make better informed decisions early on

Destec Engineering Ltd

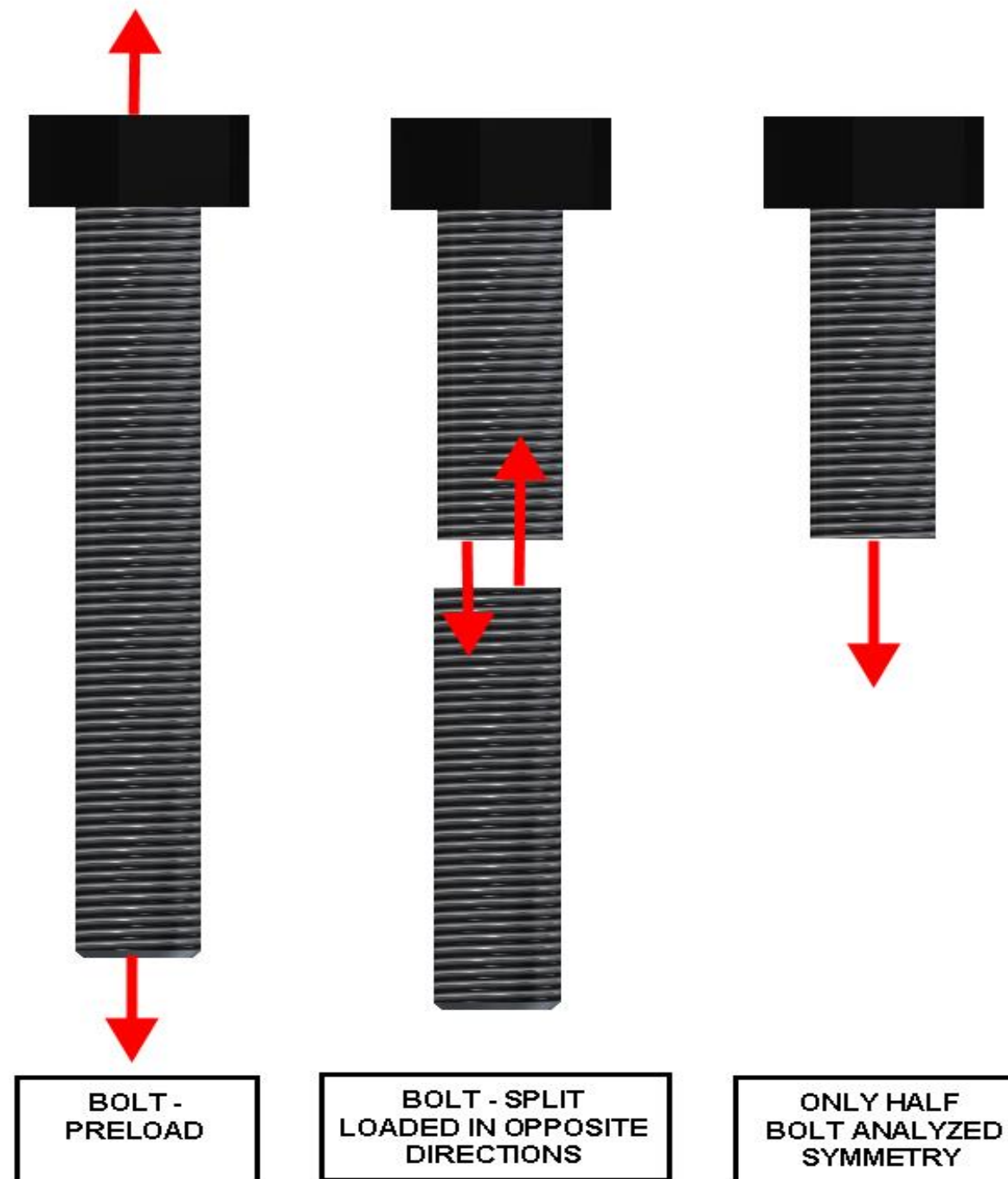


Goal: Is to make sure there is contact between seal and pipe



Design Criteria: Maximum Stress in Clamp for given bolt preload

Destec Engineering Ltd



Destec Engineering Ltd



The following equation and information will be used to determine the load to stress the bolt to a given specified value based on its diameter. This method agrees with the method given by the American Petroleum Institute Standard API 6A.

Bolt Size :- 1.1/8"-8UN

Nominal Bolt Size $NB = 1.125\text{in}$

Pitch of Thread $P = 0.125\text{in}$

Bolt Stress Area $A_b = \frac{\pi}{4} \cdot (NB - 1.3 \cdot P)^2$
 $A_b = 0.728 \cdot \text{in}^2$ ($A_b = 469.4 \cdot \text{mm}^2$)

Assembly Bolt Stress $\sigma_b = 25000\text{psi}$ ($\sigma_b = 172.4 \cdot \text{MPa}$)
 (Load on Bolt stress Area $\sigma_b \cdot A_b = 80912.9\text{N}$)

The following information is used to calculate the bolt torque required to stress the bolt to the allowable stress.

Nominal Thread Effective Diameter $D = 1.0438\text{in}$

Half Thread Angle $\alpha = 30\text{deg}$

Coefficient of Friction $\mu = 0.12$

Inside Radius of Nut Contact Face $R_1 = \frac{1.25}{2}\text{in}$

Outside Radius of Nut Contact Face $R_2 = \frac{1.813}{2}\text{in}$

Friction Torque at Thread $A = \frac{\mu \cdot A_b \cdot \sigma_b \cdot D}{2 \cdot \cos(\alpha)}$

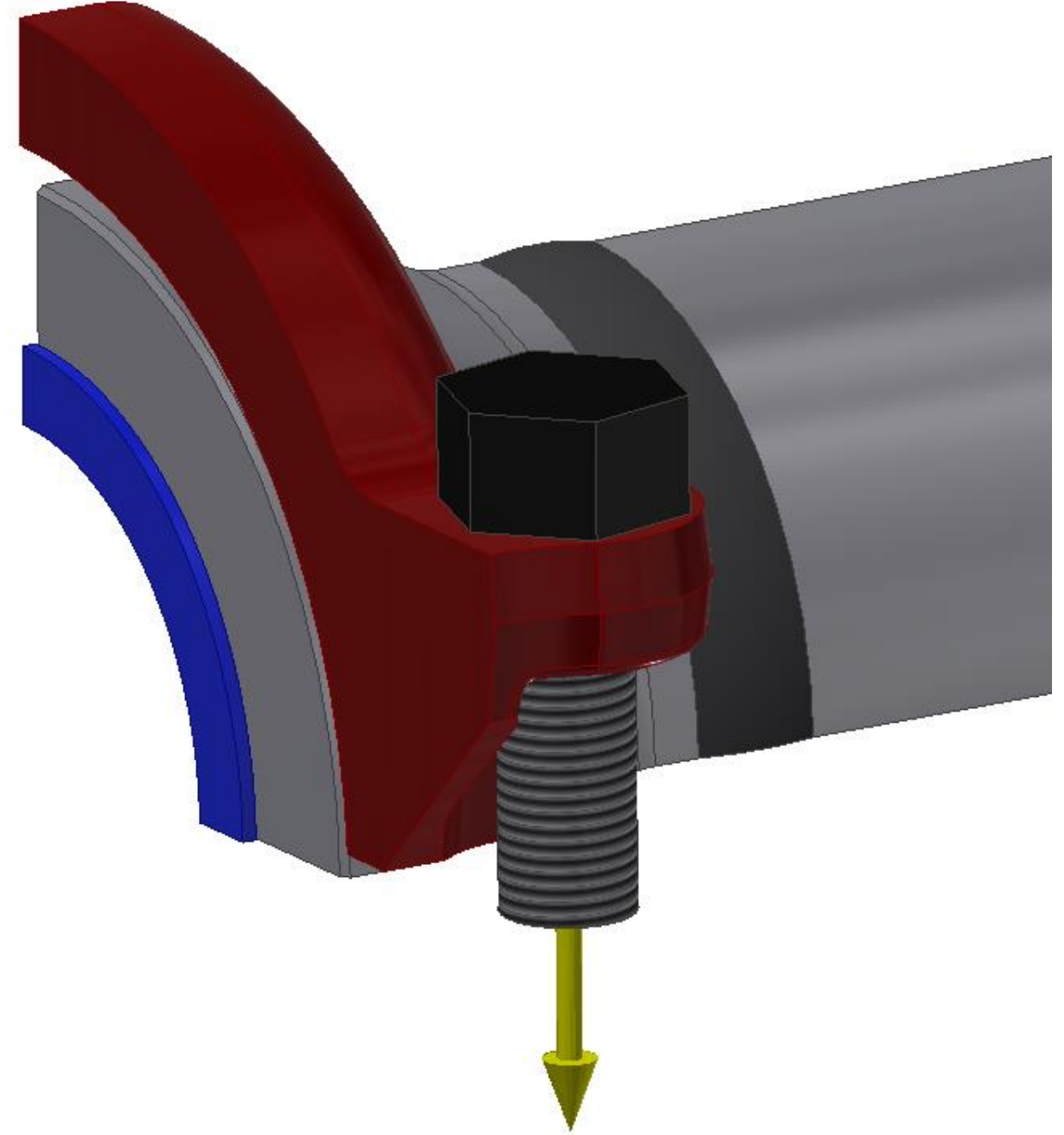
Friction Torque between Nut Face and Clamp/Cover $C = \left(2 \cdot \mu \cdot A_b \cdot \frac{\sigma_b}{3} \right) \cdot \frac{R_2^3 - R_1^3}{R_2^2 - R_1^2}$

Torque Required to Stretch Bolt Without Friction $B = \frac{A_b \cdot \sigma_b \cdot P}{2 \cdot \pi}$

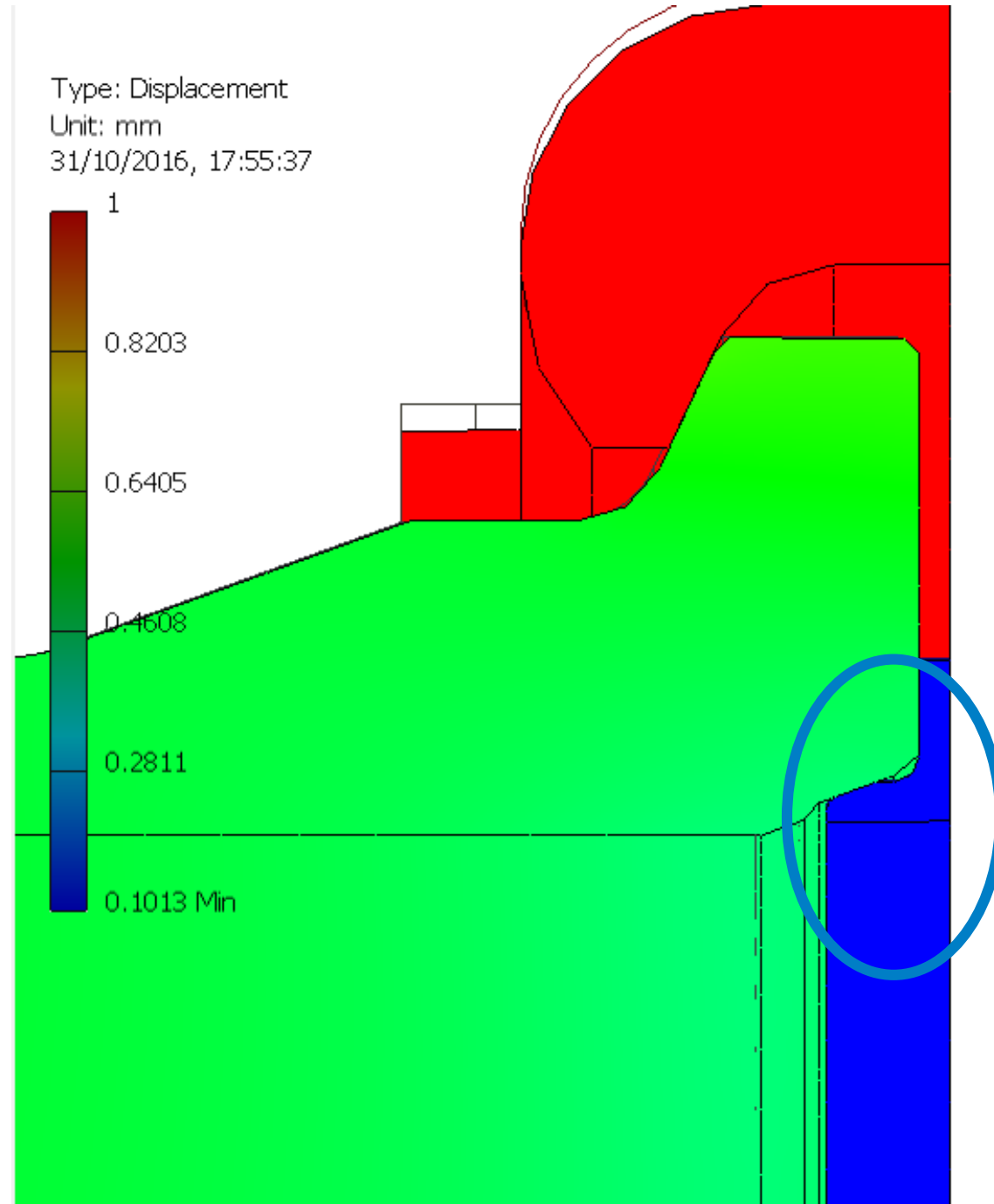
Total Torque Required $T = (A + B + C)$

$T = 280.6 \cdot \text{lbfft}$ ($T = 380.5 \cdot \text{N} \cdot \text{m}$)

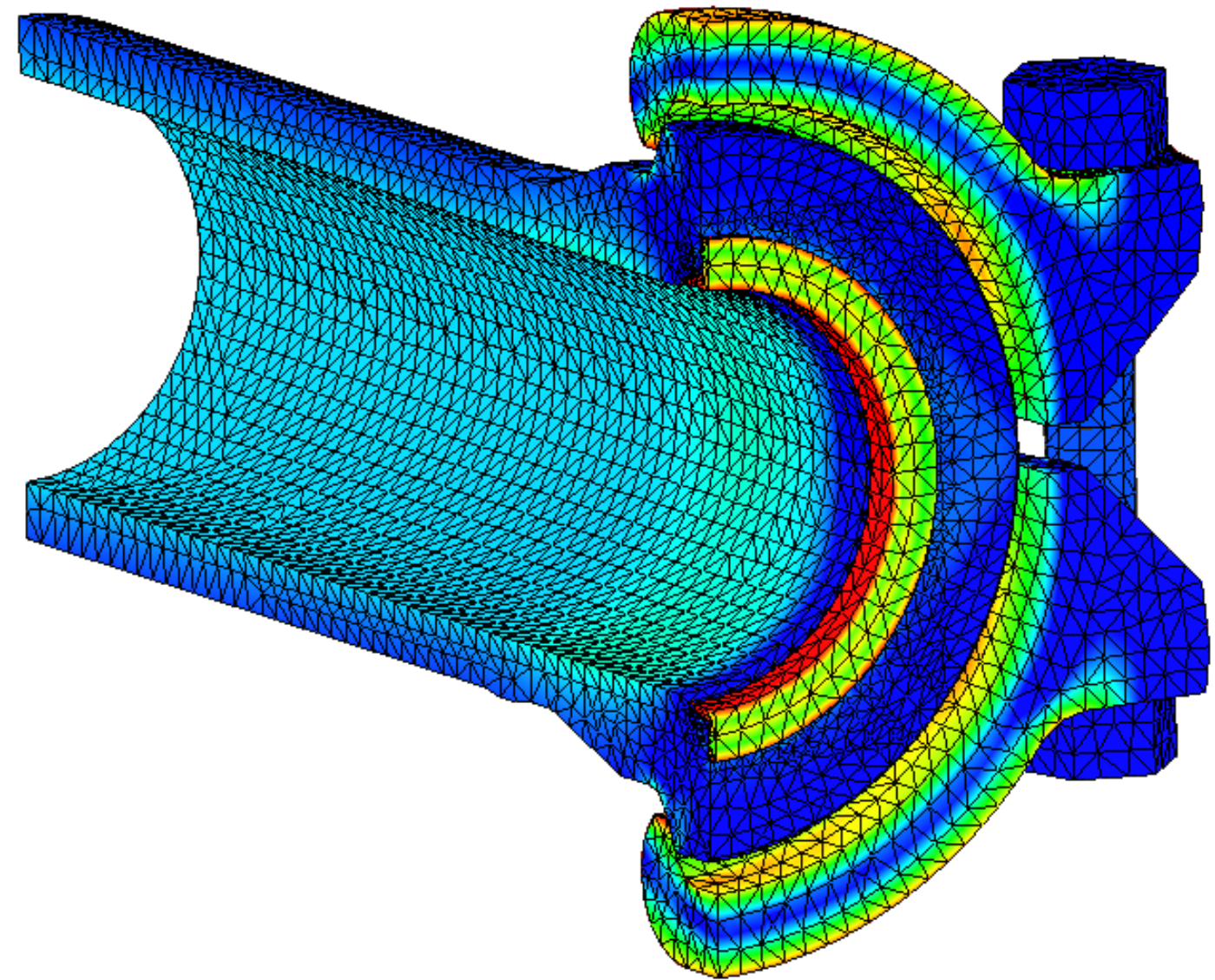
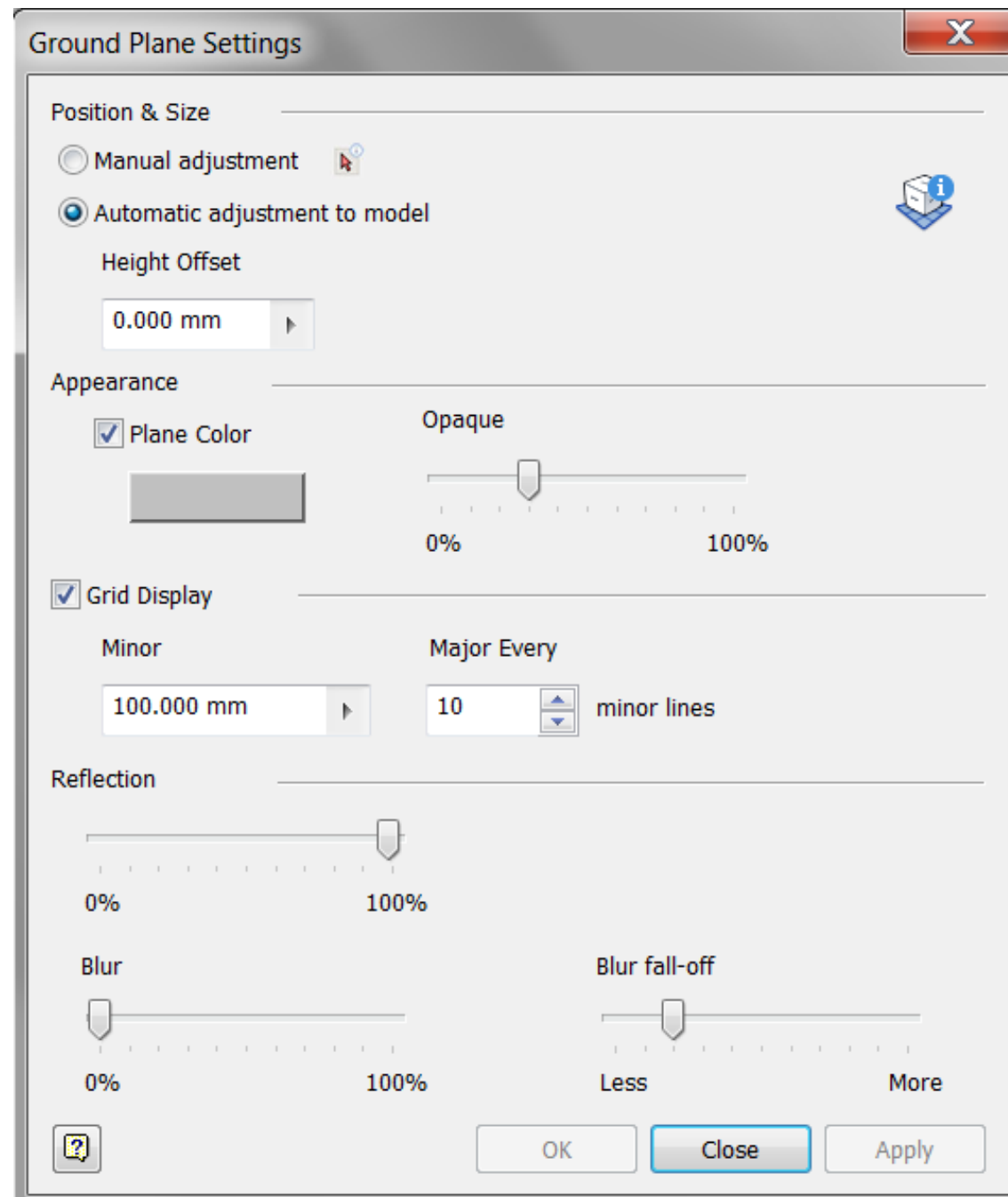
Destec Engineering Ltd



Destec Engineering Ltd



Destec Engineering Ltd



GKN Land Systems Ltd



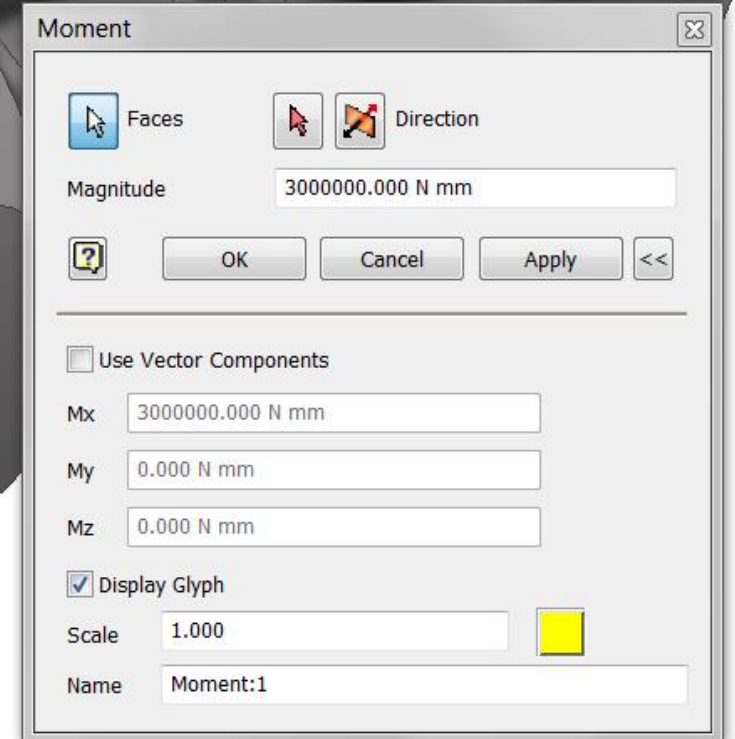
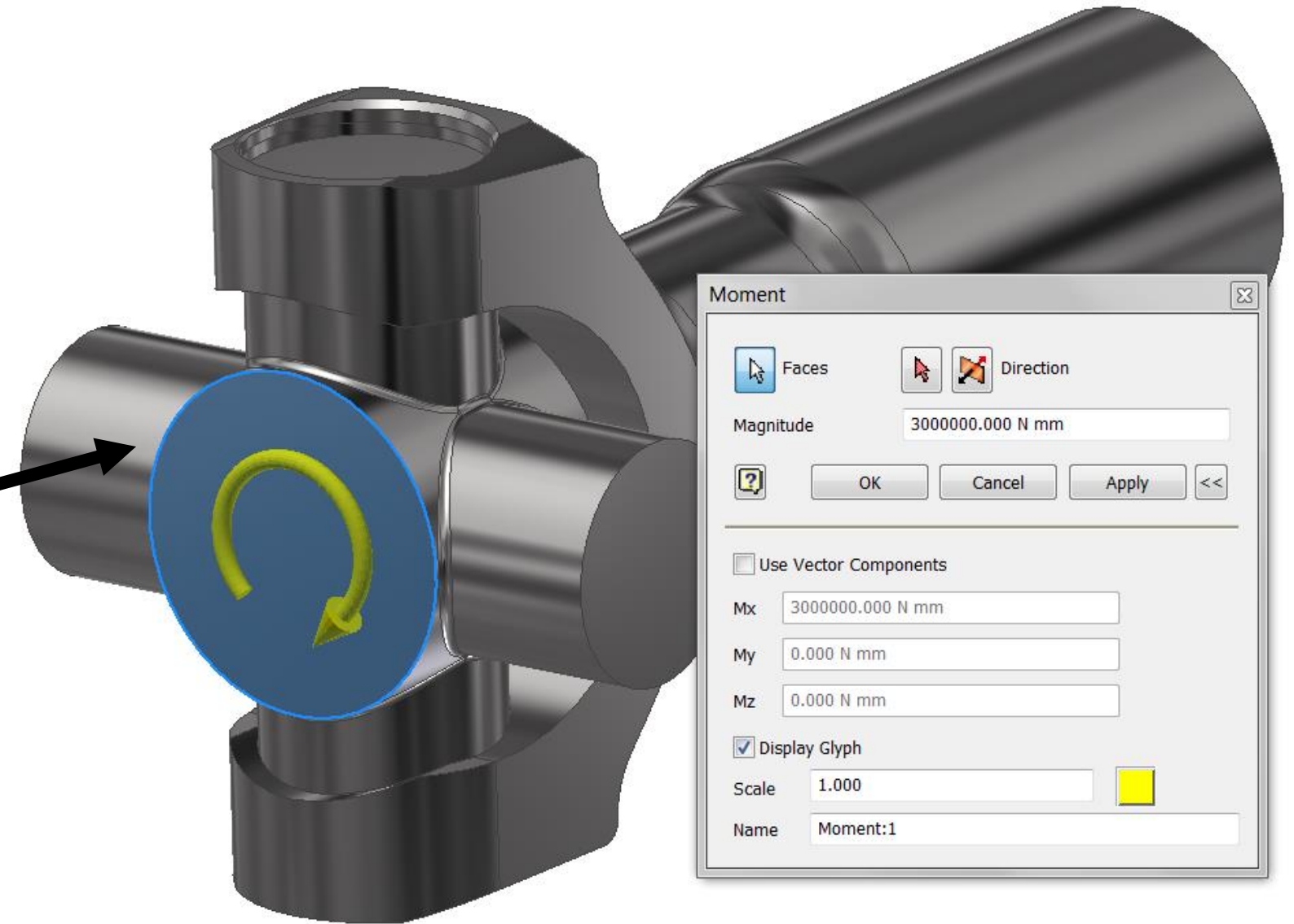
Goal: Is to determine operating stress of propshaft yoke



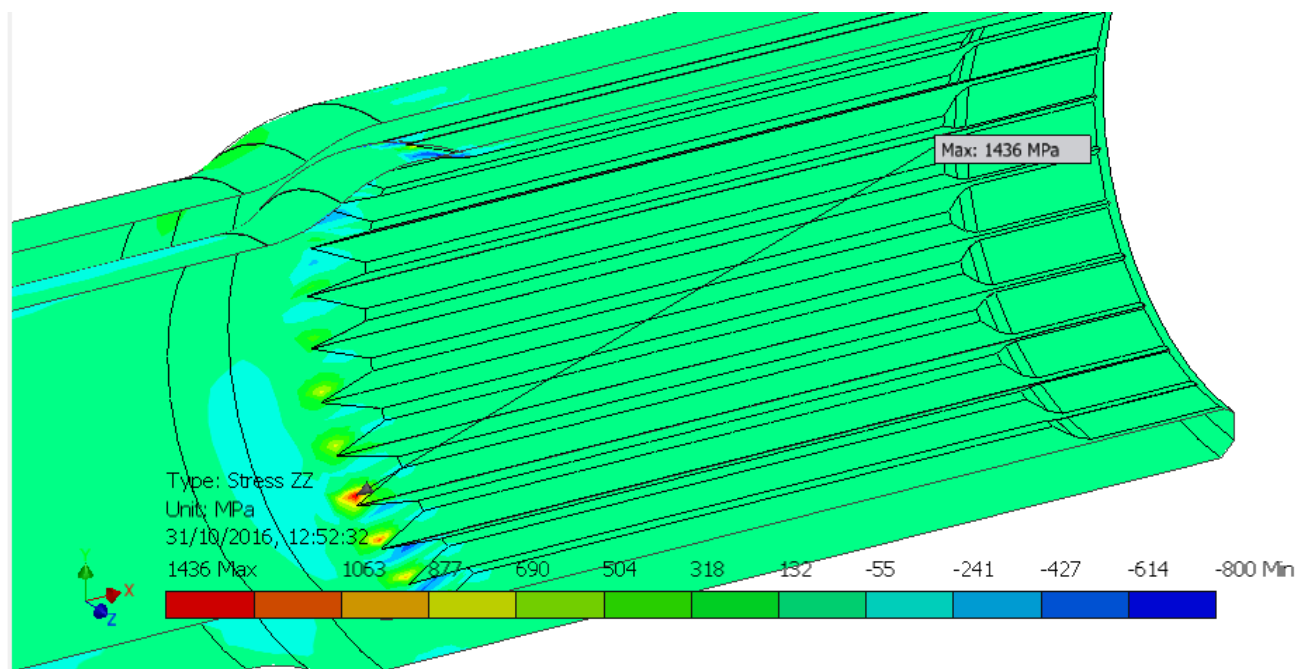
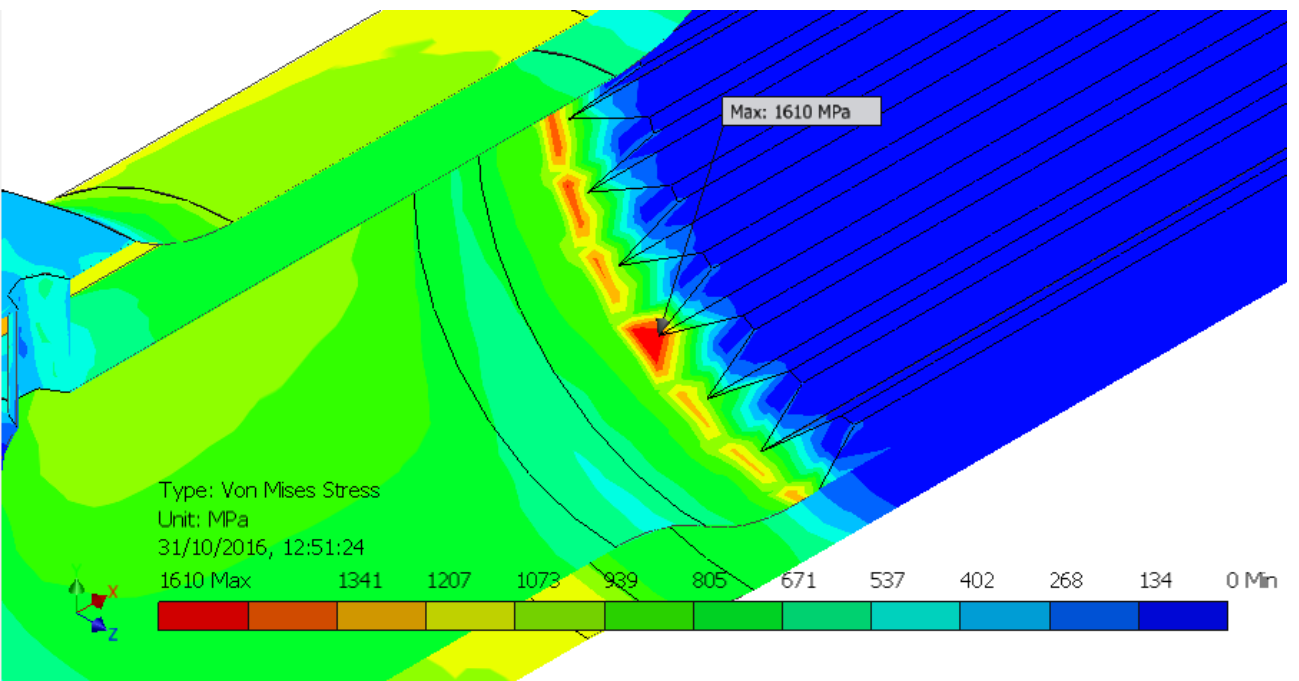
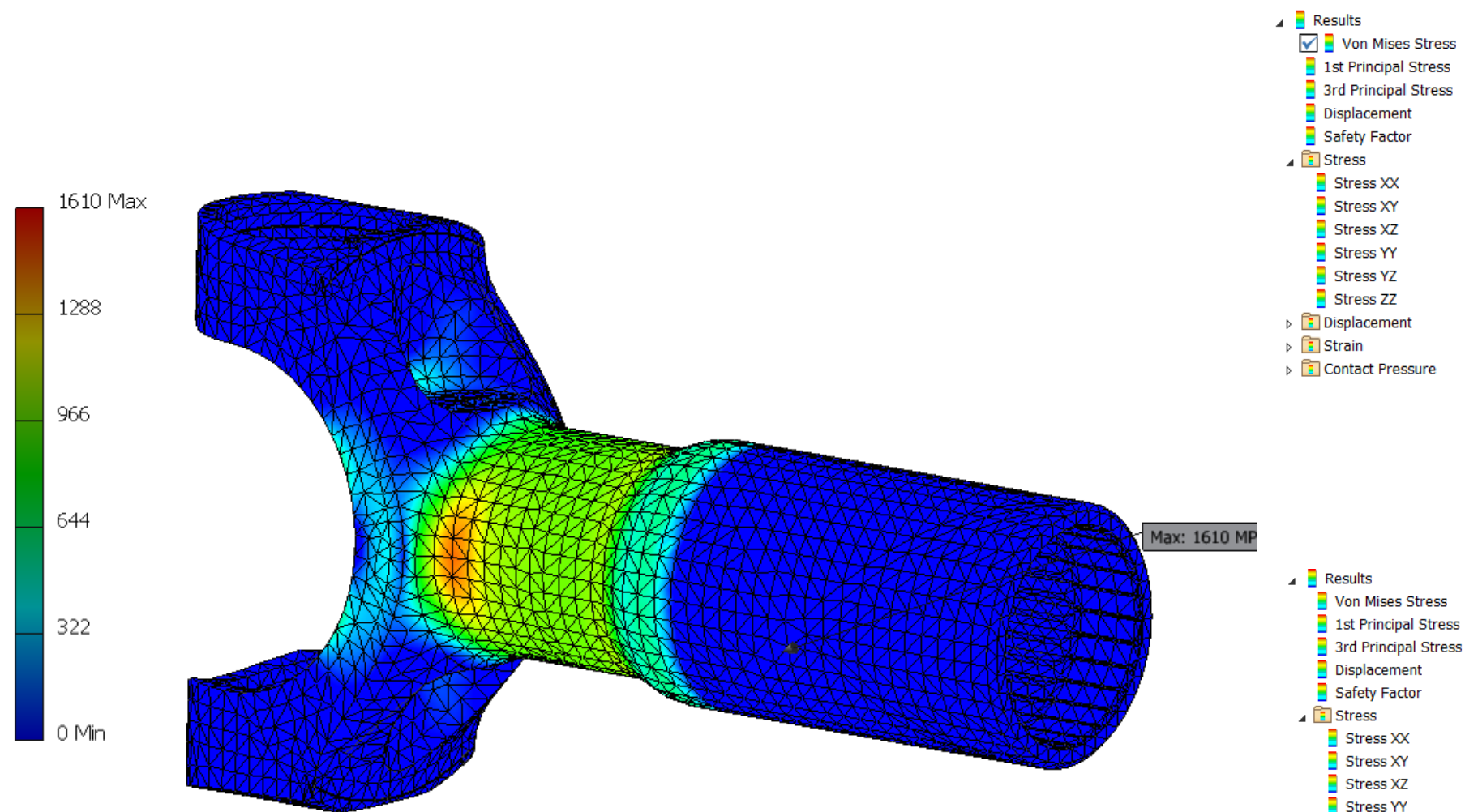
Design Criteria:

- Yield Limit is 1550 Mpa
- Moment 3000 Nm

GKN Land Systems Ltd



GKN Land Systems Ltd



Planet Platforms Ltd



Goal:

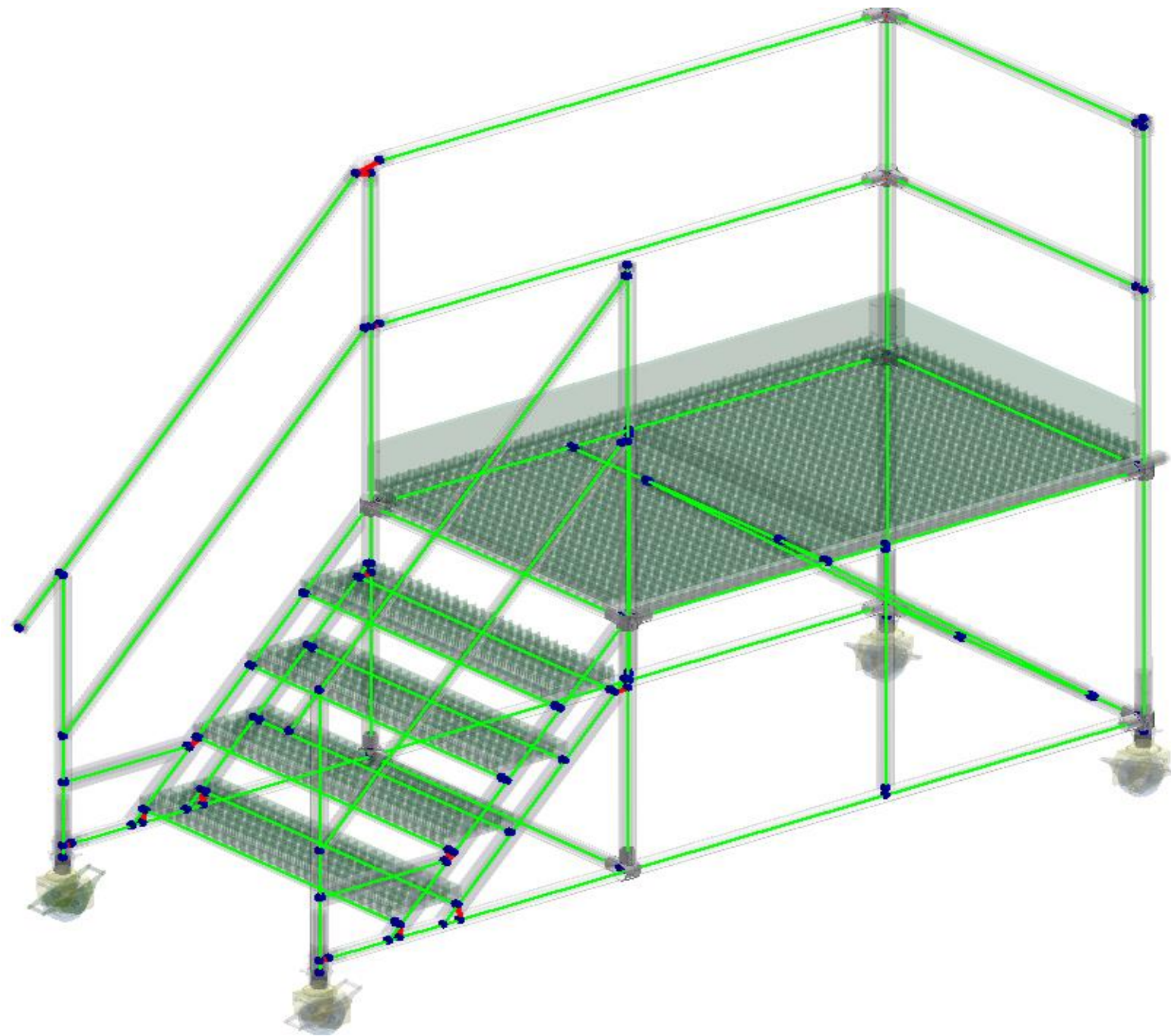
Is to make sure platform can withstand weight of two maintenance workers including their tools



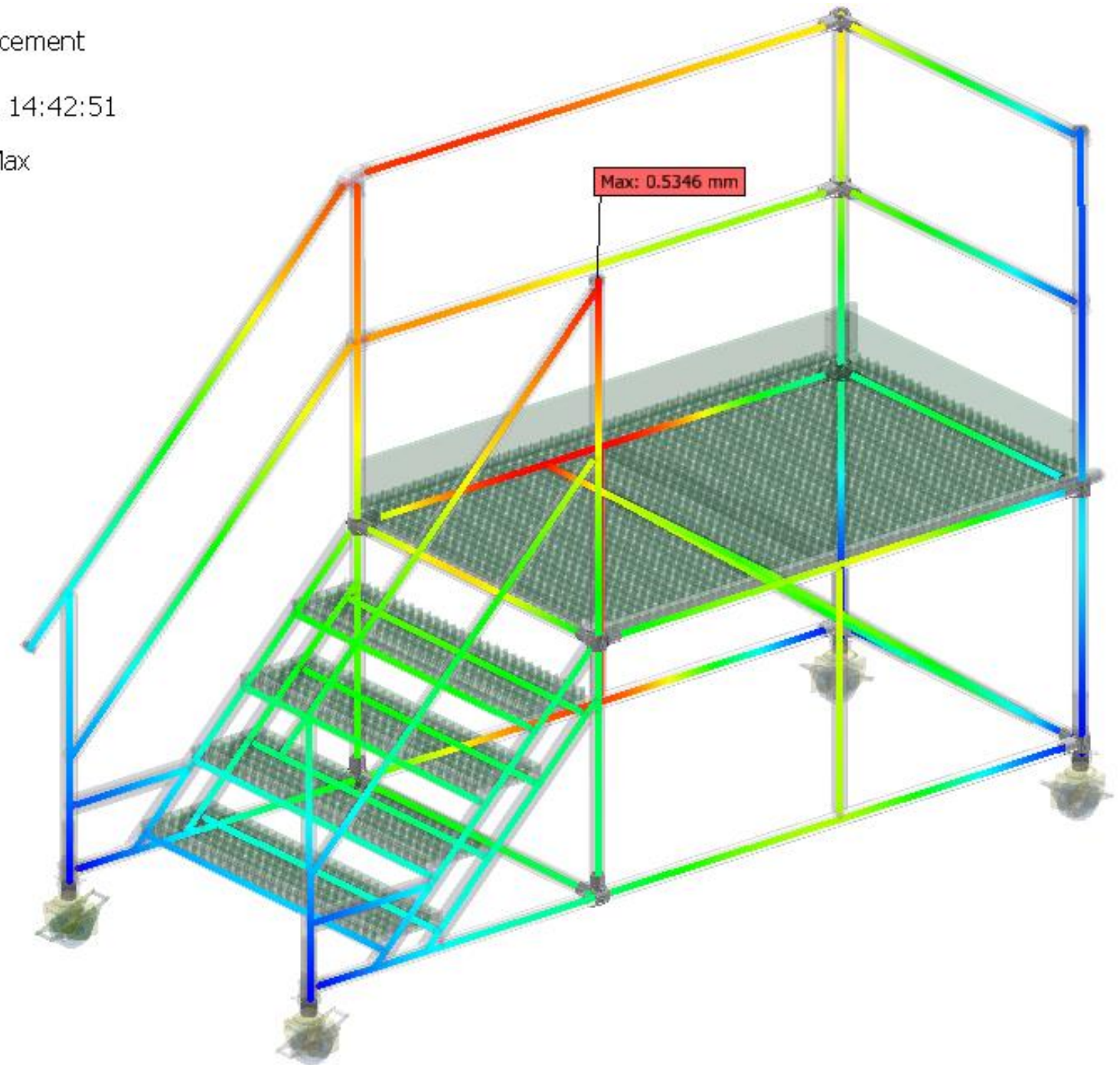
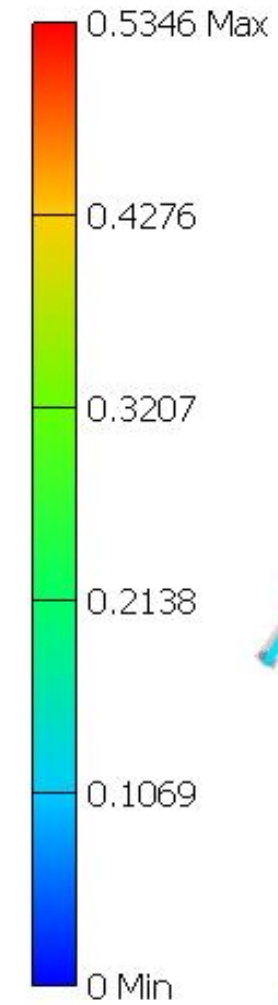
Design Criteria:

- Safety Factor of 4
- Max displacement of 10mm

Planet Platforms Ltd

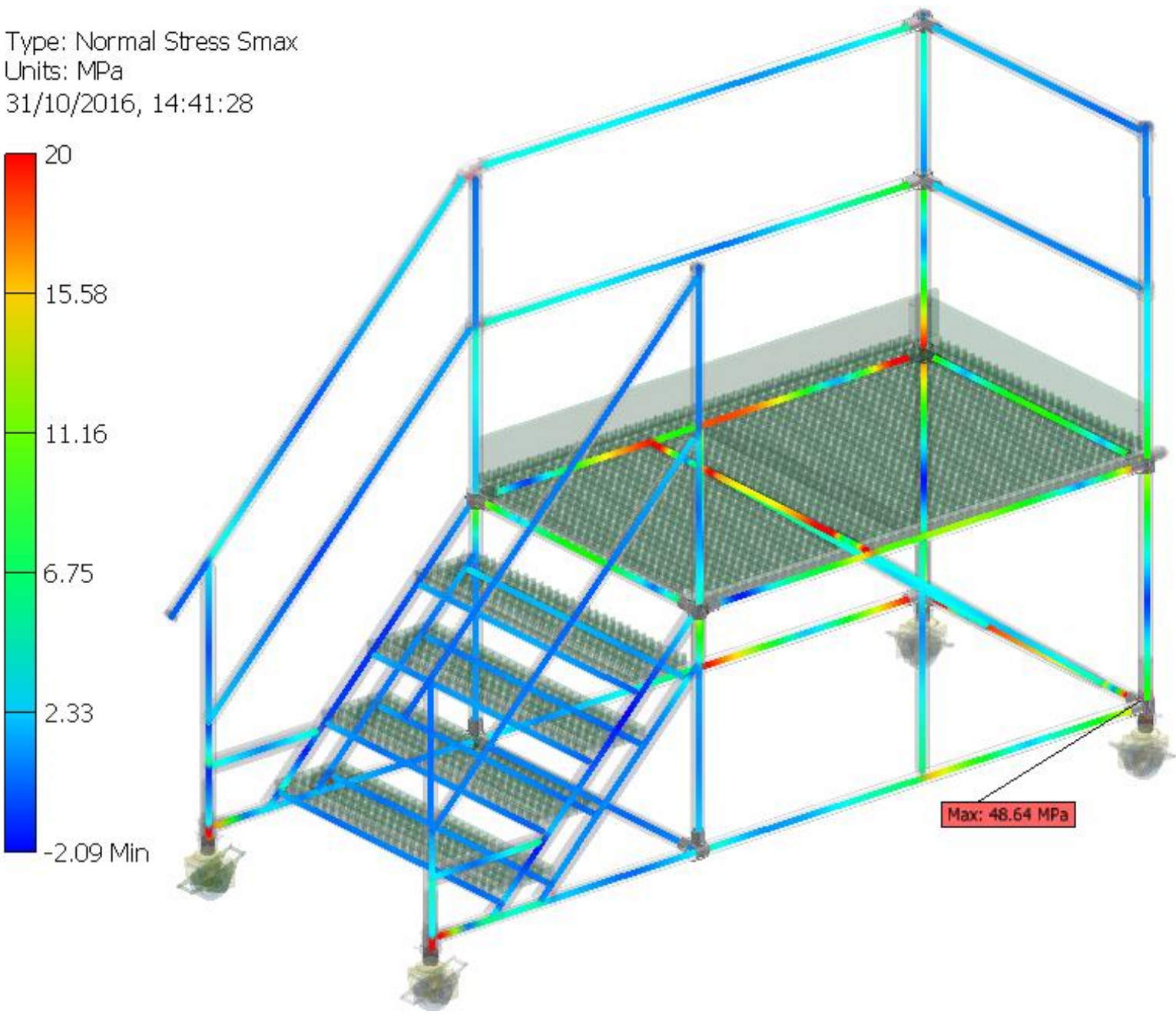


Type: Displacement
Units: mm
31/10/2016, 14:42:51



Planet Platforms Ltd

Type: Normal Stress Smax
Units: MPa
31/10/2016, 14:41:28



Beam Material

Beams

- ISO 4200 - 48.3x1.6 - 1010.ipt
- ISO 4200 - 48.3x1.6 - 760.ipt
- ISO 4200 - 48.3x1.6 - 1300.ipt
- ISO 4200 - 48.3x1.6 - 1040.ipt
- DIN EN 10305-5 - 60 x 30 x 2 - 1127.ipt
- DIN EN 10305-5 - 60 x 30 x 2 - 867.ipt
- DIN EN 10305-5 - 60 x 30 x 2 - 405.ipt
- ISO 4019 - 25x25x3 - 1041.5.ipt
- ISO 4200 - 48.3x1.6 - 1507.ipt
- ISO 4200 - 48.3x1.6 - 1680.ipt
- ISO 4200 - 48.3x1.6 - 2718.8.ipt
- ISO 4200 - 48.3x1.6 - 1952.1.ipt
- ISO 4200 - 48.3x1.6 - 1899.2.ipt
- ISO 4200 - 48.3x1.6 - 1825.8.ipt
- ISO 4200 - 48.3x1.6 - 900.ipt
- ISO 4200 - 48.3x1.6 - 1360.ipt

Material

Name: Aluminum 6061

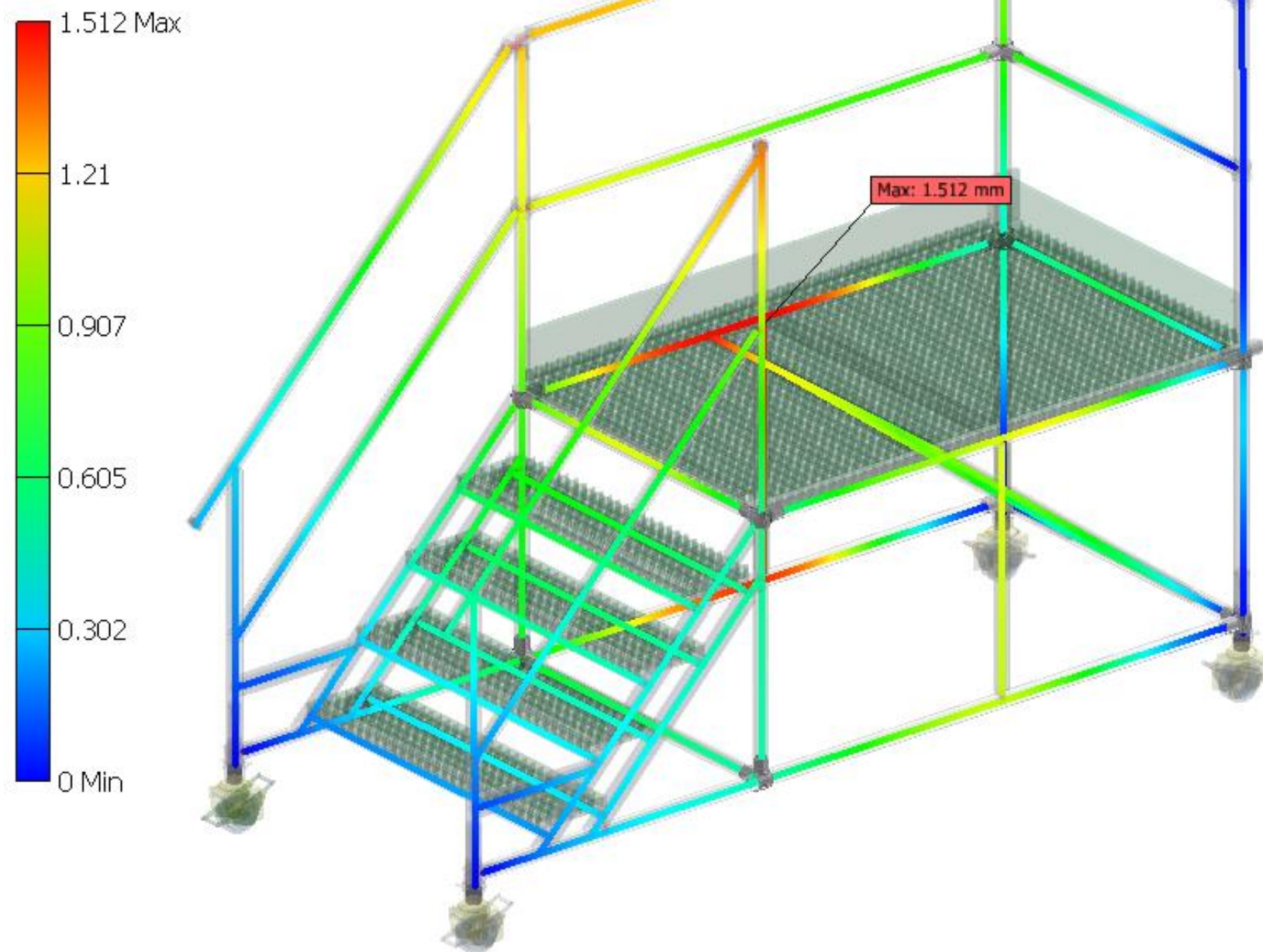
2.7 g/cm ³	Density
68.9 GPa	Young's Modulus
0.3 ul	Poisson's ratio
275.0 MPa	Yield Strength
310.0 MPa	Ultimate Tensile Strength
167.0 W/(m K)	Thermal Conductivity
0.0000236 ul/c	Linear Expansion
0.9 J/(kg K)	Specific Heat

☒ Customize

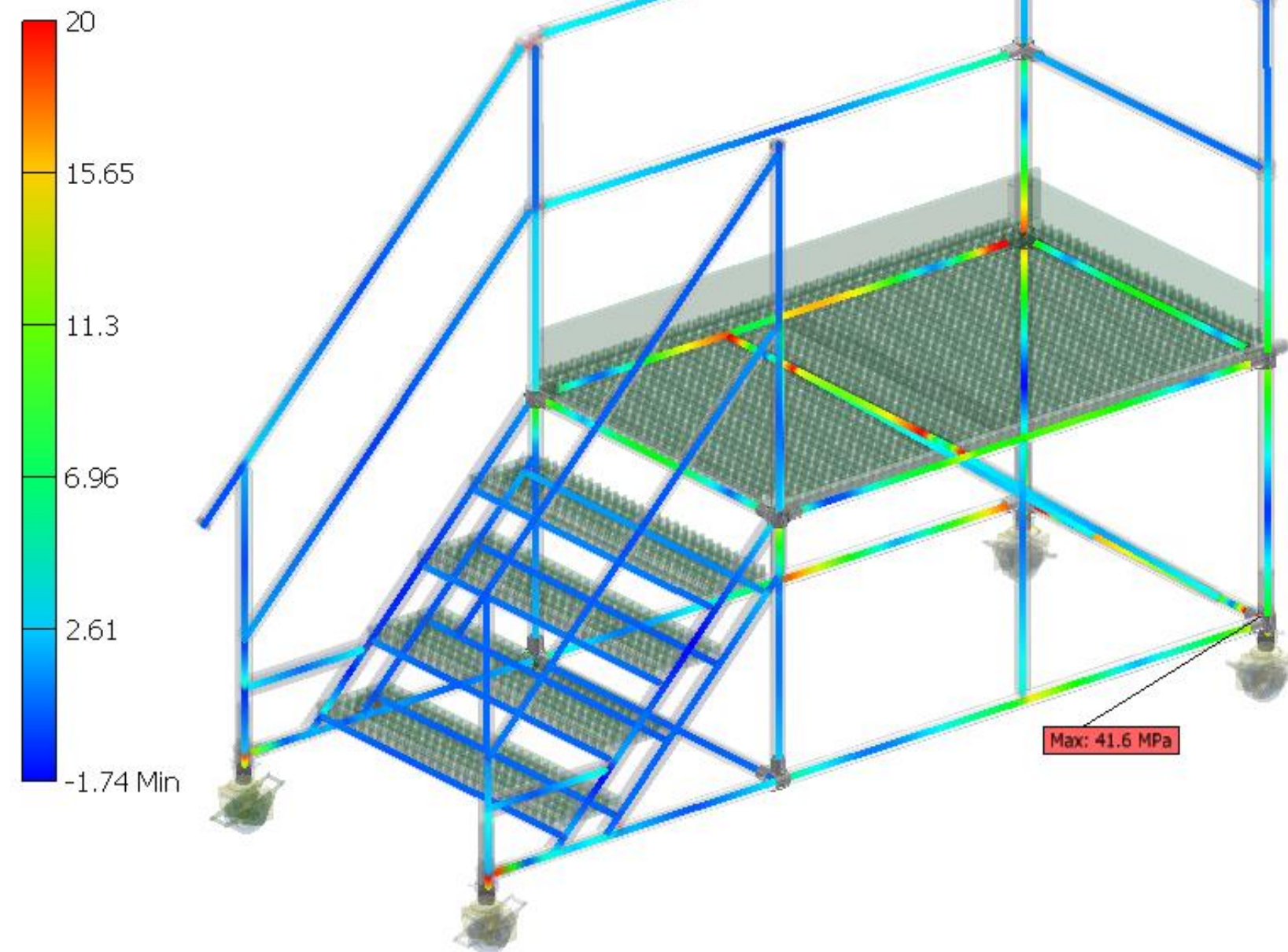
OK Cancel Apply

Planet Platforms Ltd

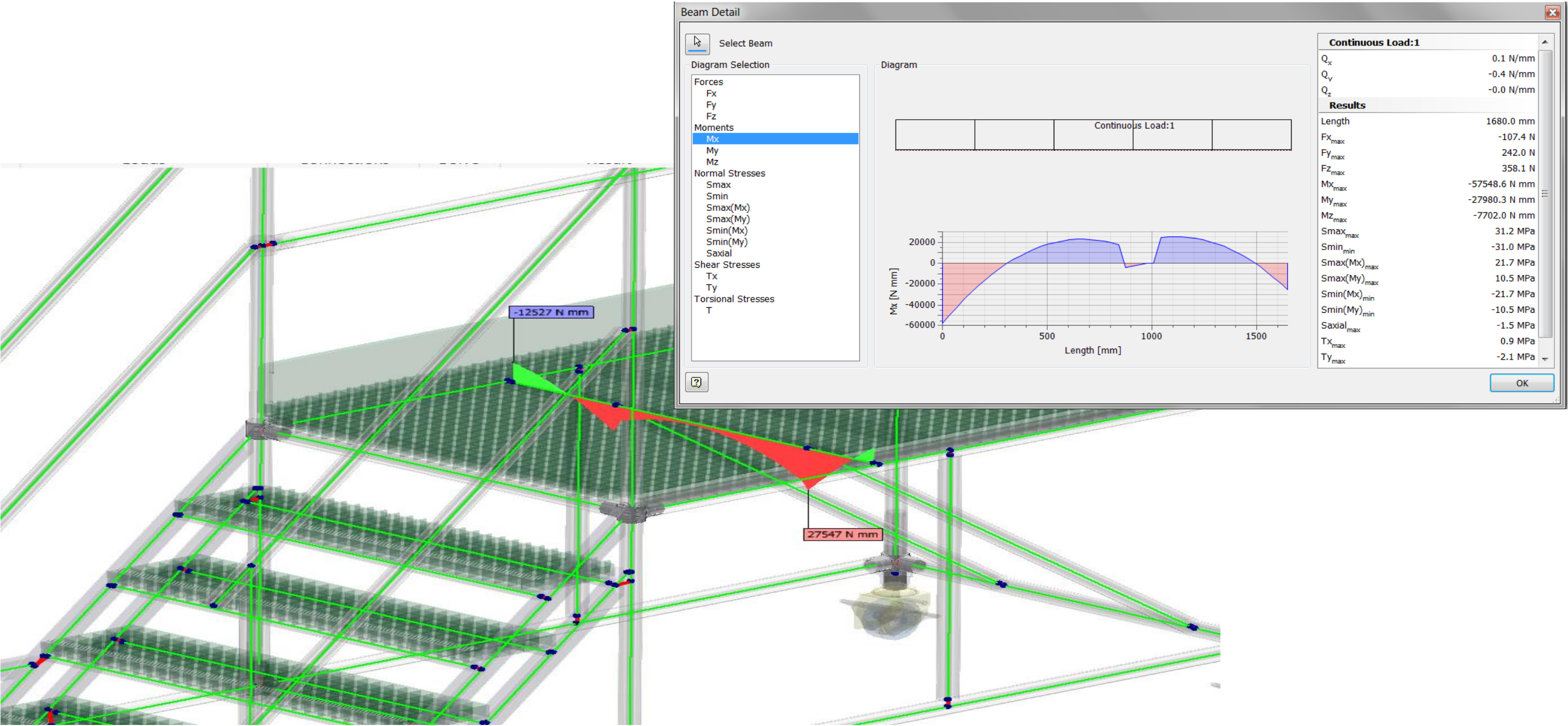
Type: Displacement
Units: mm
31/10/2016, 14:43:57



Type: Normal Stress Smax
Units: MPa
31/10/2016, 14:44:30



Planet Platforms Ltd



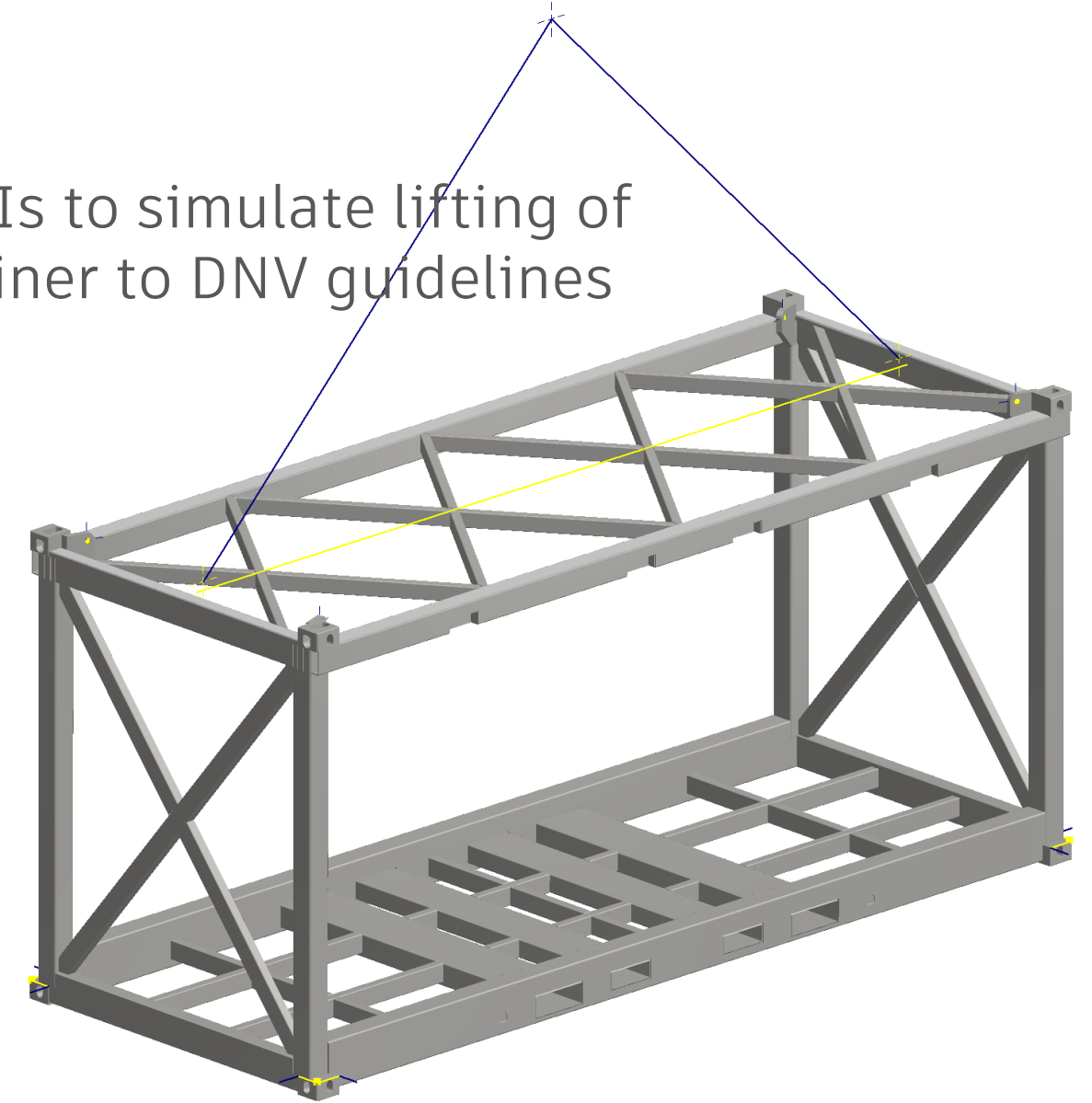
Nastran In-CAD

Take Inventor Simulation to next level

Swire Oilfield Services Ltd



Goal: Is to simulate lifting of container to DNV guidelines

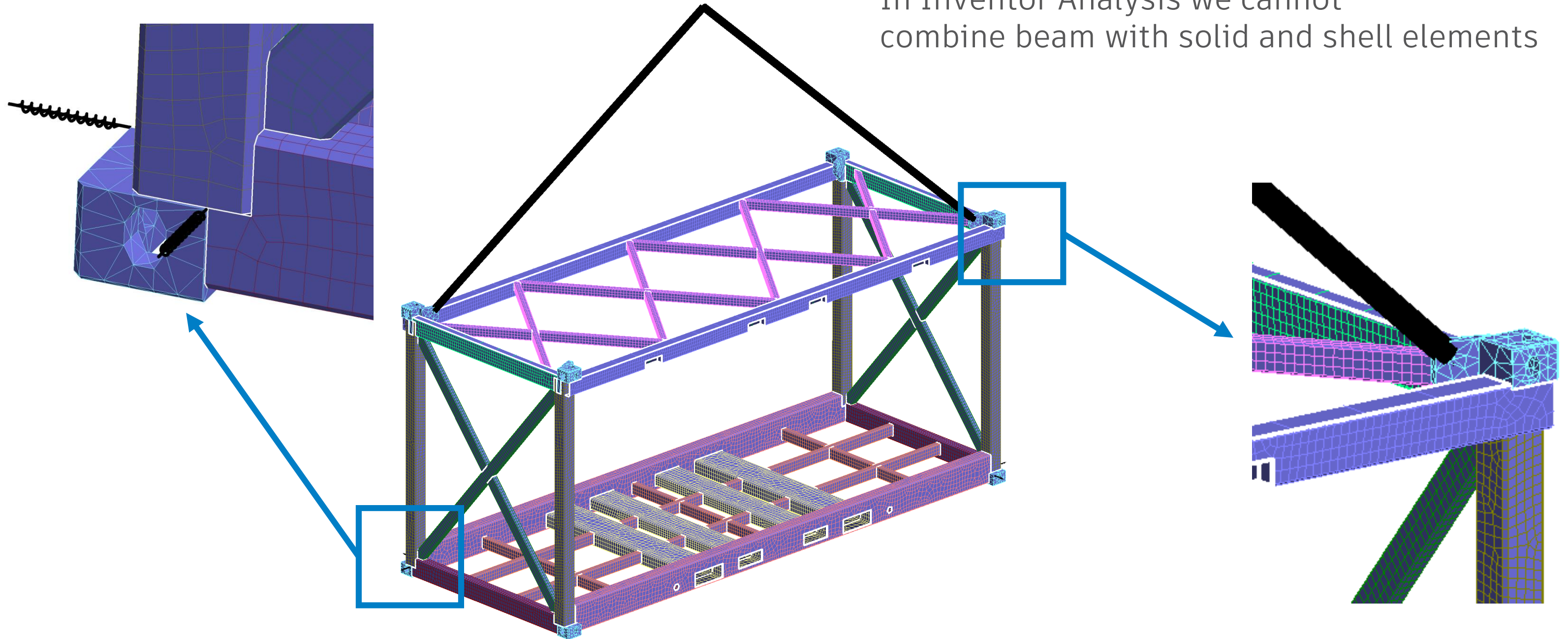


Design Criteria:

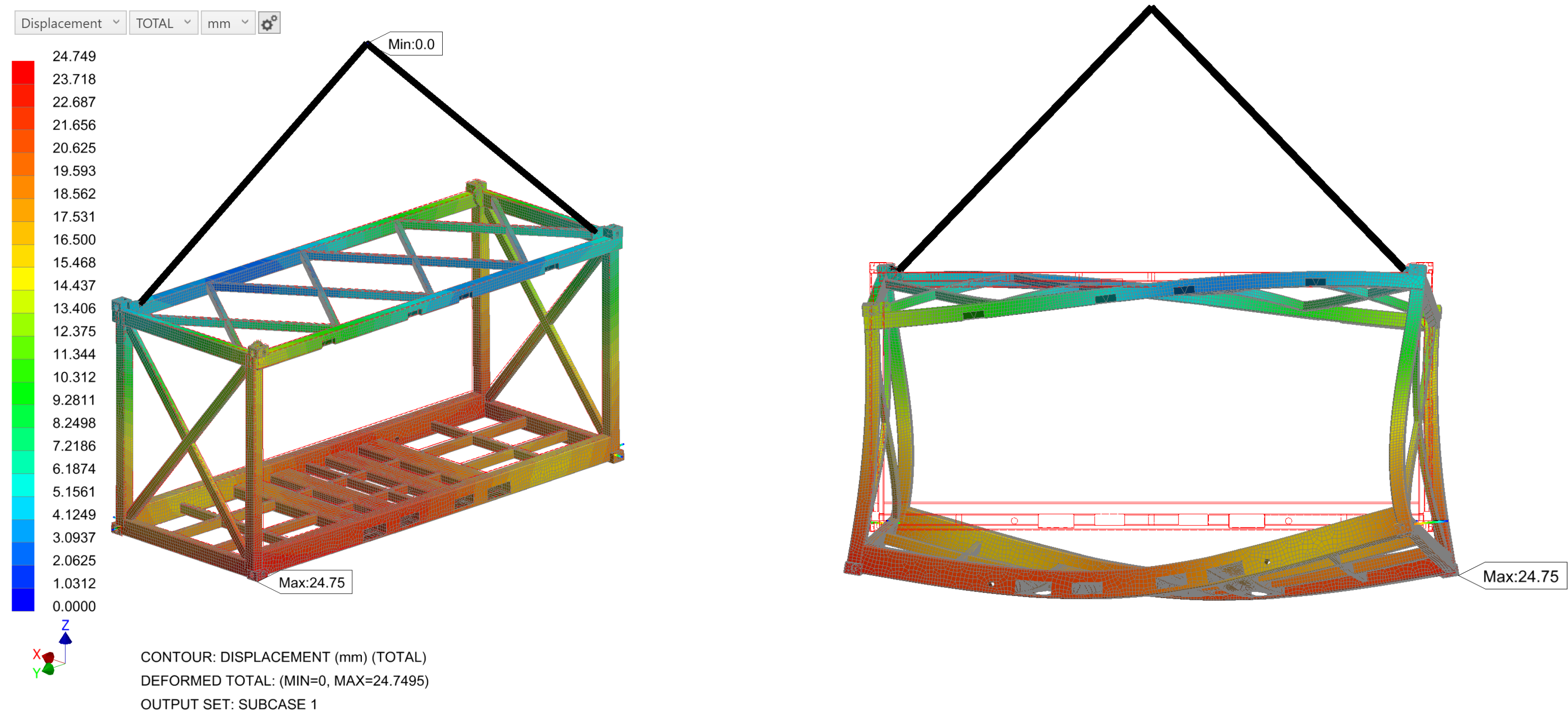
- Stress is below yield limit

Swire Oilfield Services Ltd

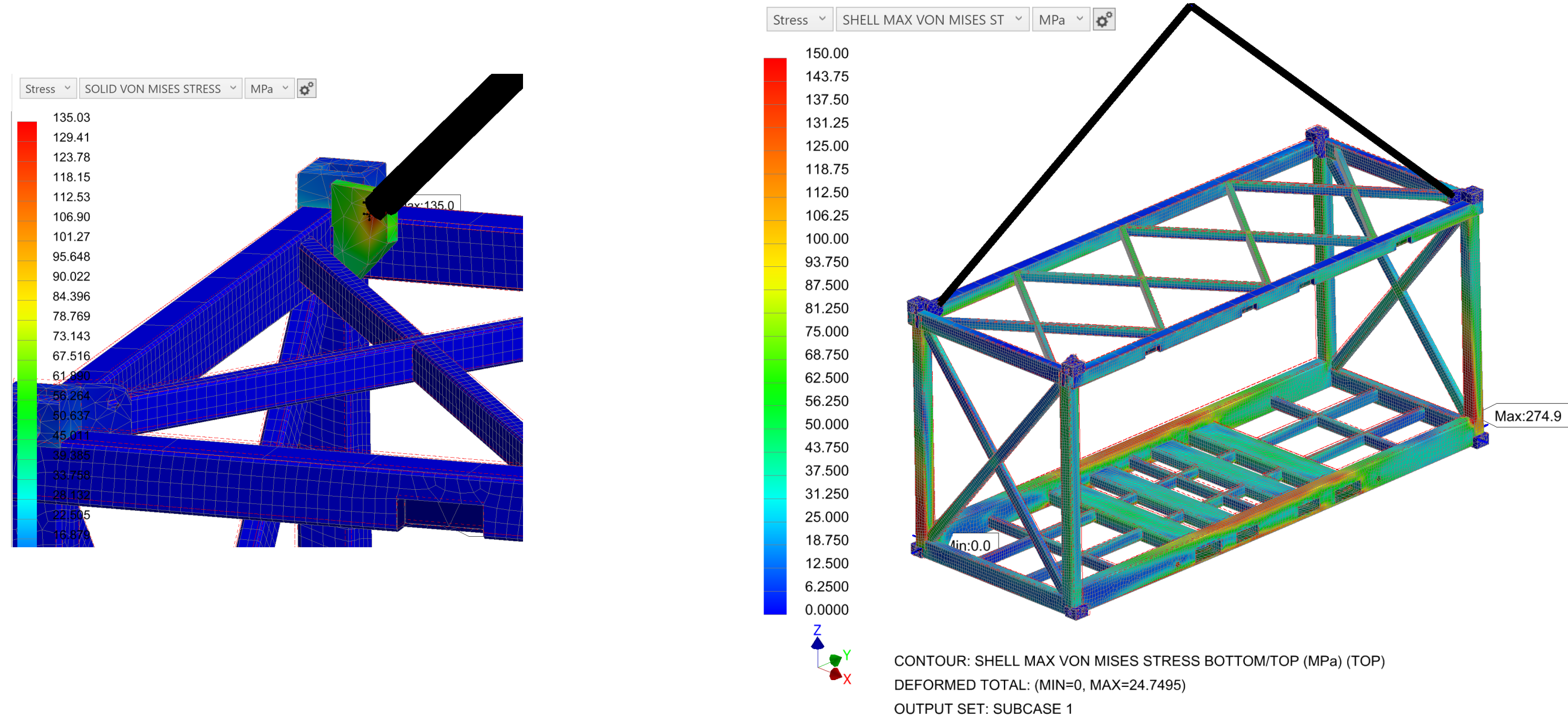
In Inventor Analysis we cannot
combine beam with solid and shell elements



Swire Oilfield Services Ltd



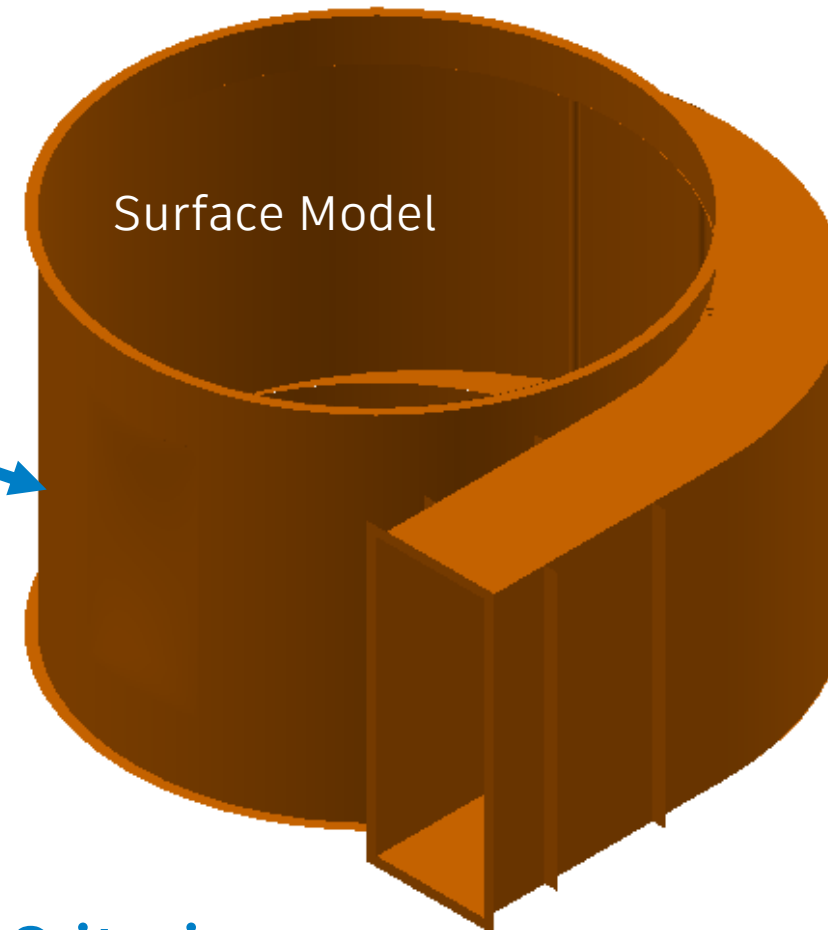
Swire Oilfield Services Ltd



Simatek A/S(Non-Linear Analysis)



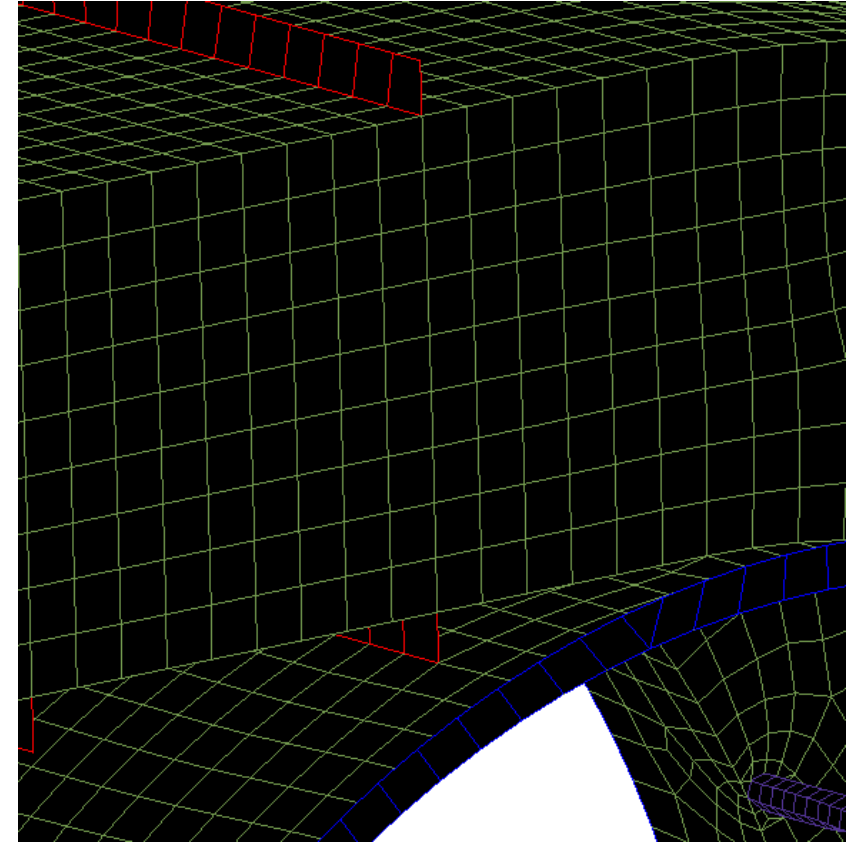
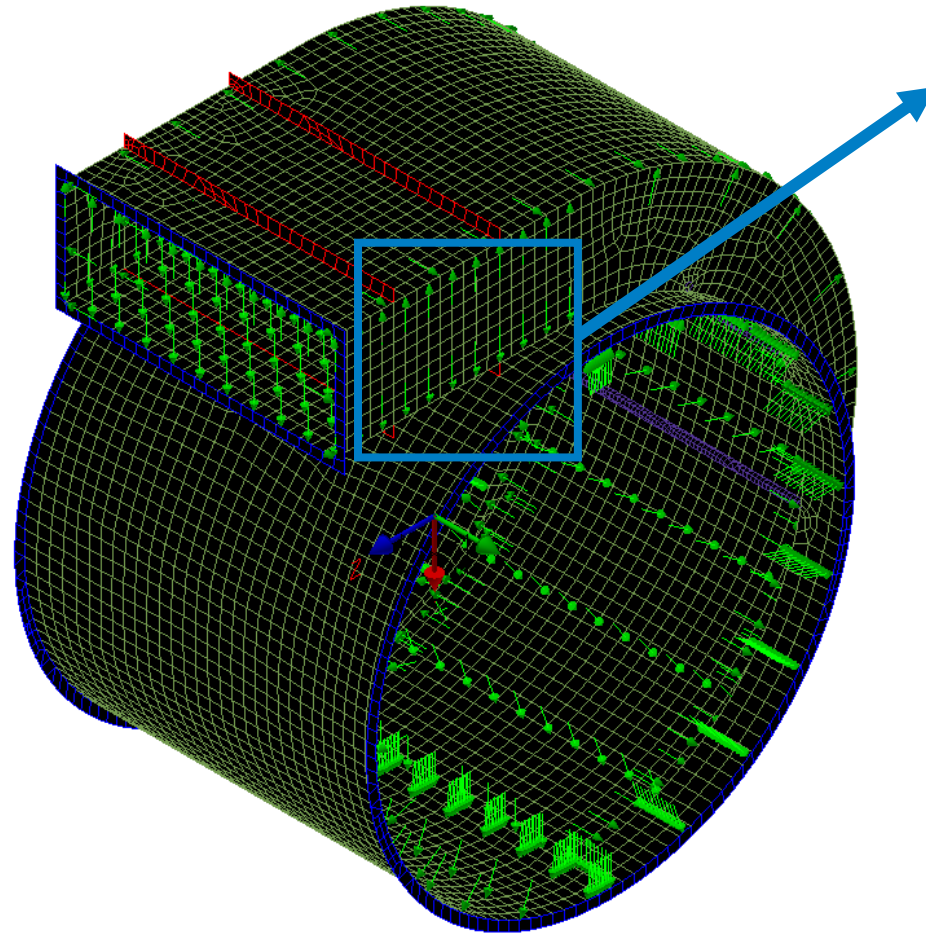
Goal: Is to determine amount of permanent deformation under loading



Design Criteria:

- Predefined Stress/Strain Material data
- Pressure 90 MPa

Simatek A/S



Simatek A/S

Nonlinear Material Data

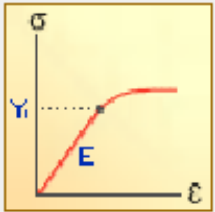
Type

☐ None

☐ Nonlinear Elastic

☐ Elasto-Plastic (Bi-Linear)

☒ Plastic



Properties

Tangent Modulus, Et (MPa):

19000

Hardening Rule:

Isotropic

Yield Function

Yield Criterion:

von Mises

Initial Yield Stress (MPa):

206

Friction Angle: (deg):

0

Strain

Stress (MPa)

0

0

0.001084210526

206

0.0015

216.2

0.002

230

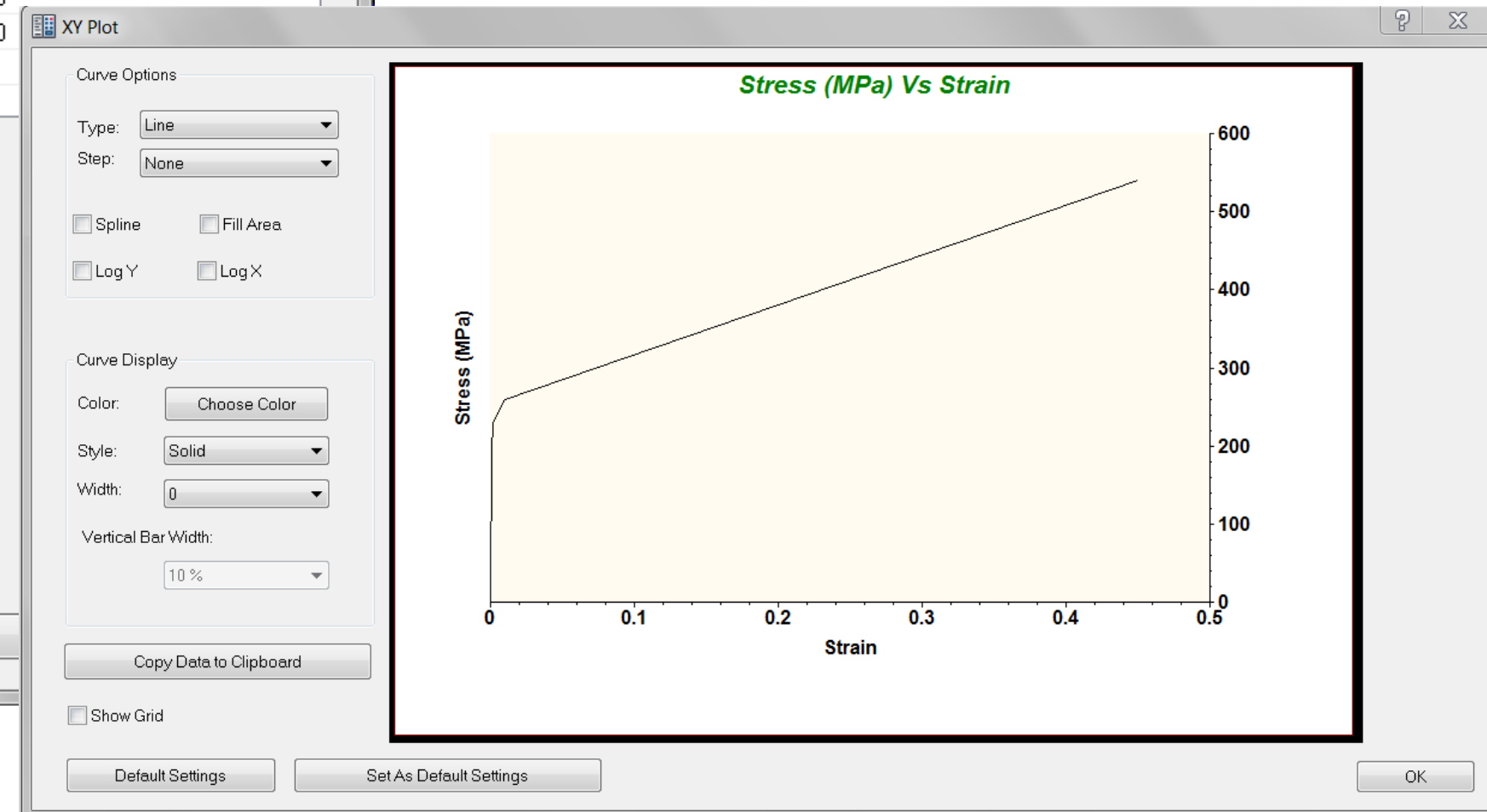
0.01

260

0.45

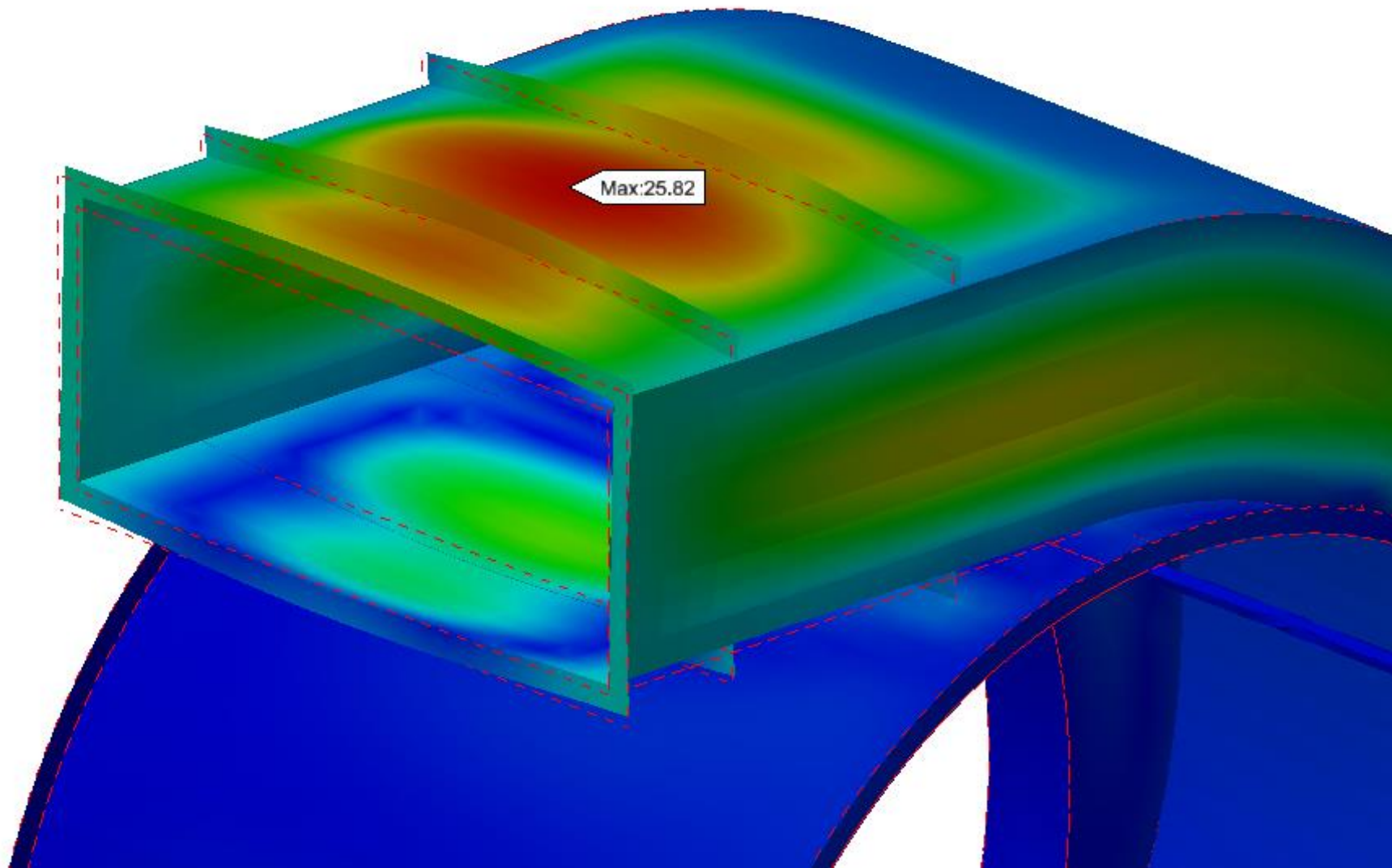
540

Show XY Plot

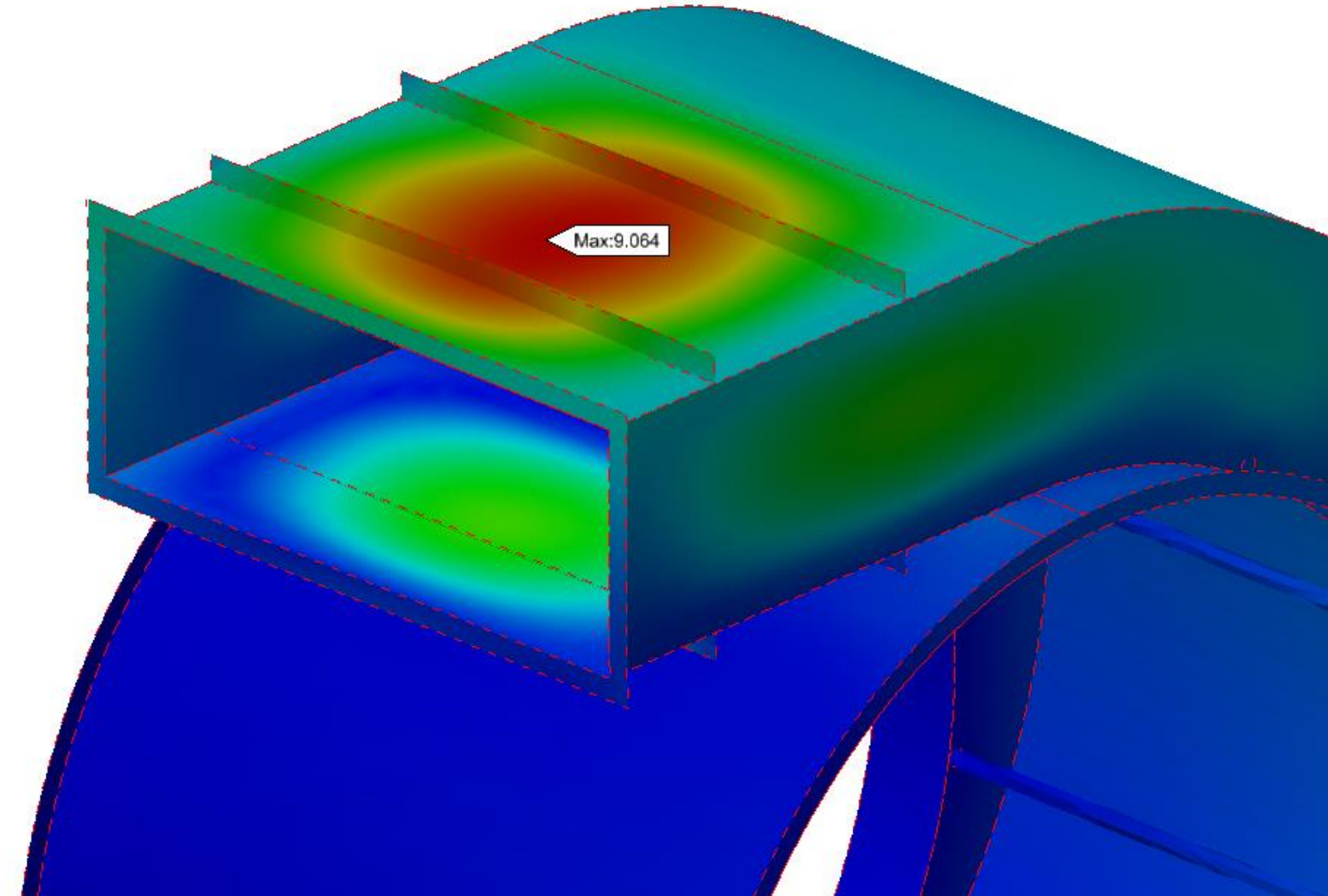


Simatek A/S

Deformation Under Loading



Permanent Deformation When Unloaded



CUE DEE (Frequency Response)



Goal: Is to verify structural integrity from vibration/shaking loading

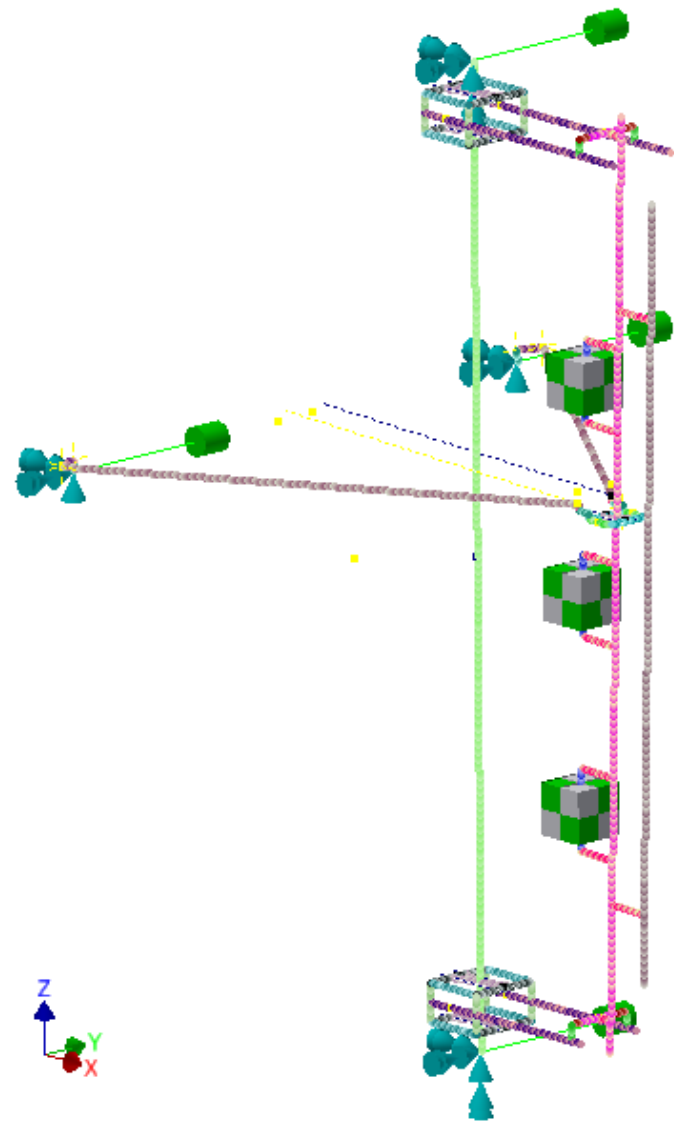


Design Criteria:

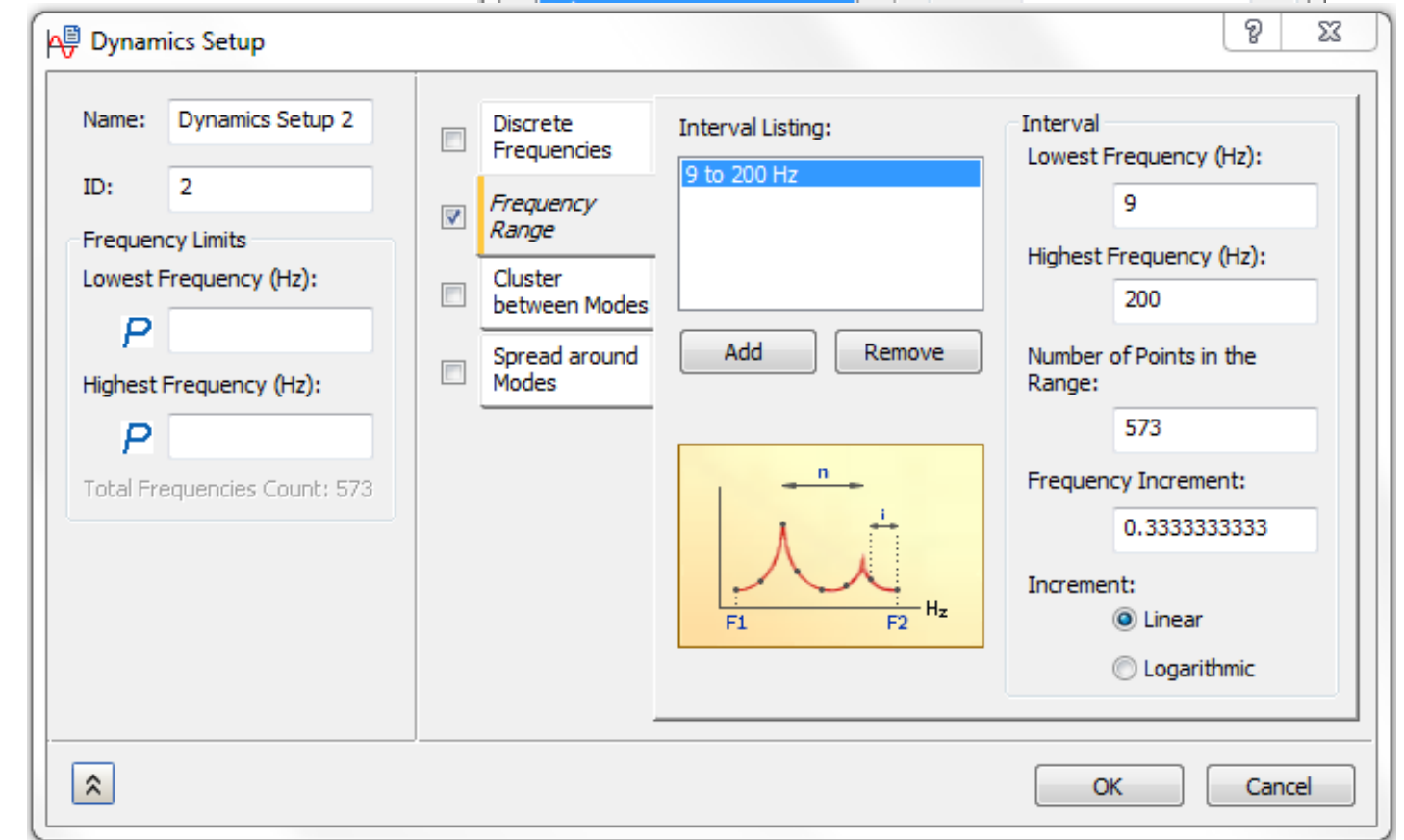
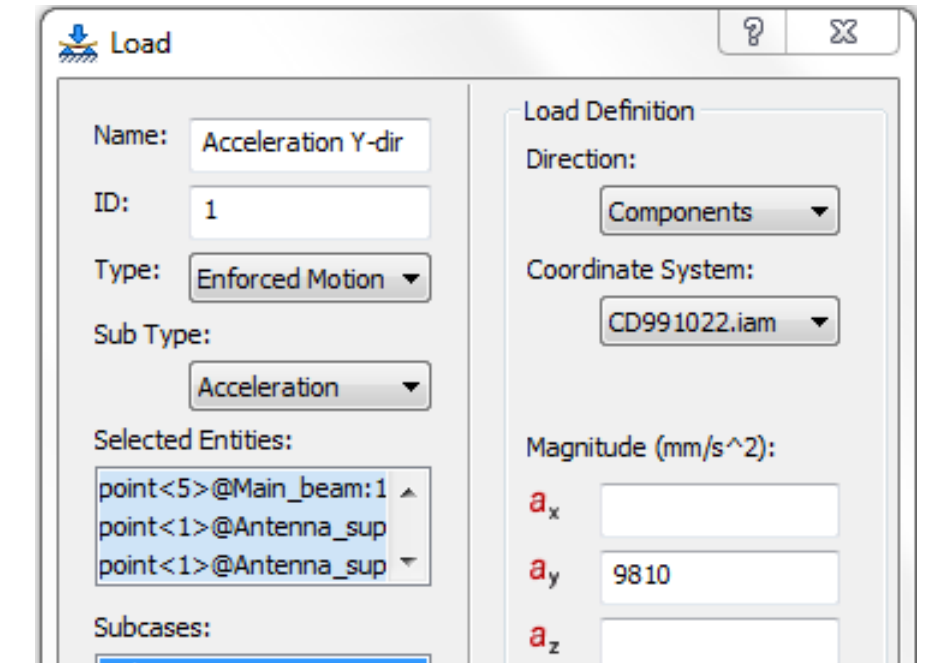
- Predefined displacements/acceleration within a specific frequency interval (according to standard testing procedures)
 - 2-9Hz: 3mm displacements
 - 9-200Hz: 1g acceleration
 - All directions

CUE DEE

Beam Elements



3D Visualisation



CUE DEE

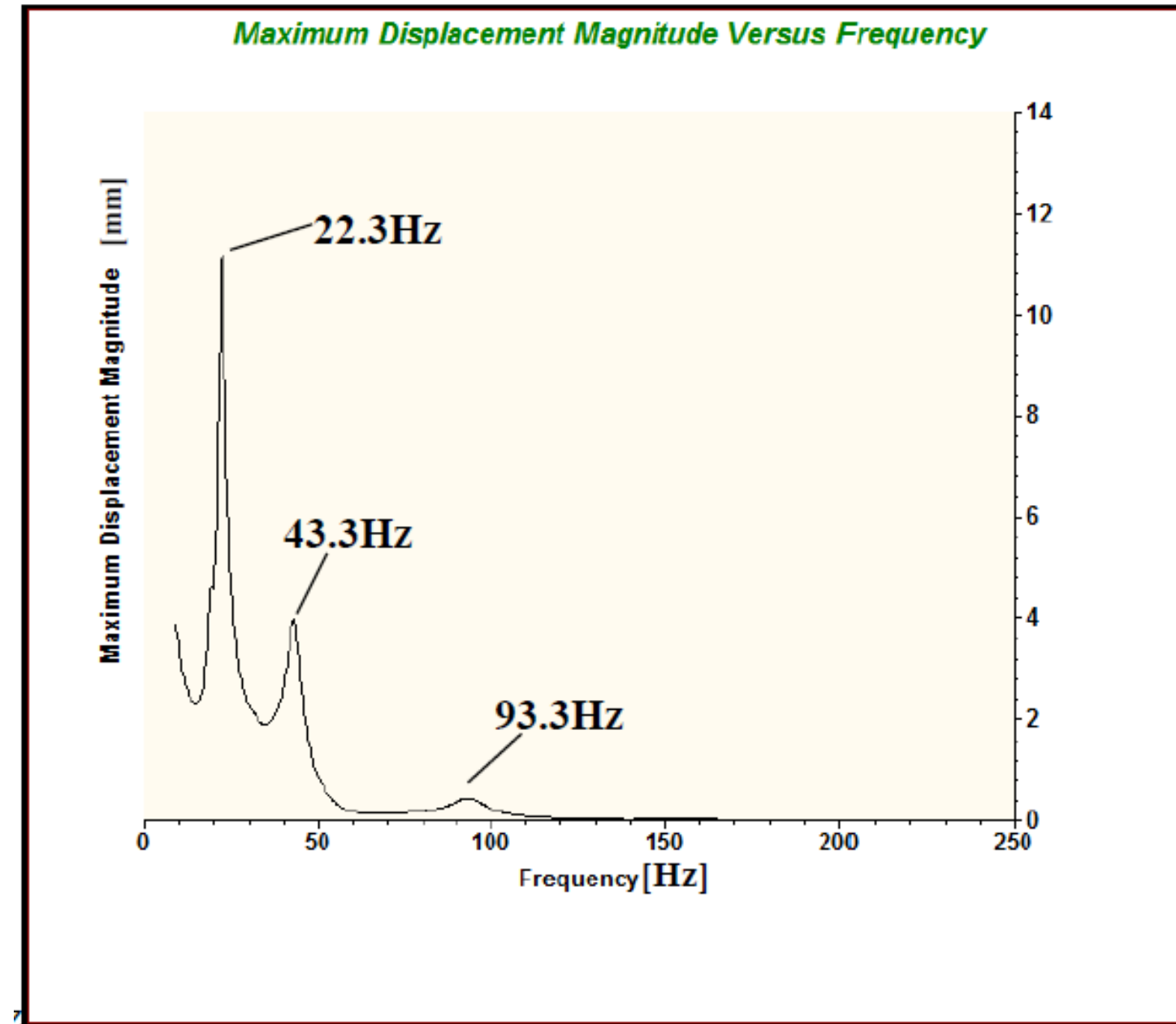
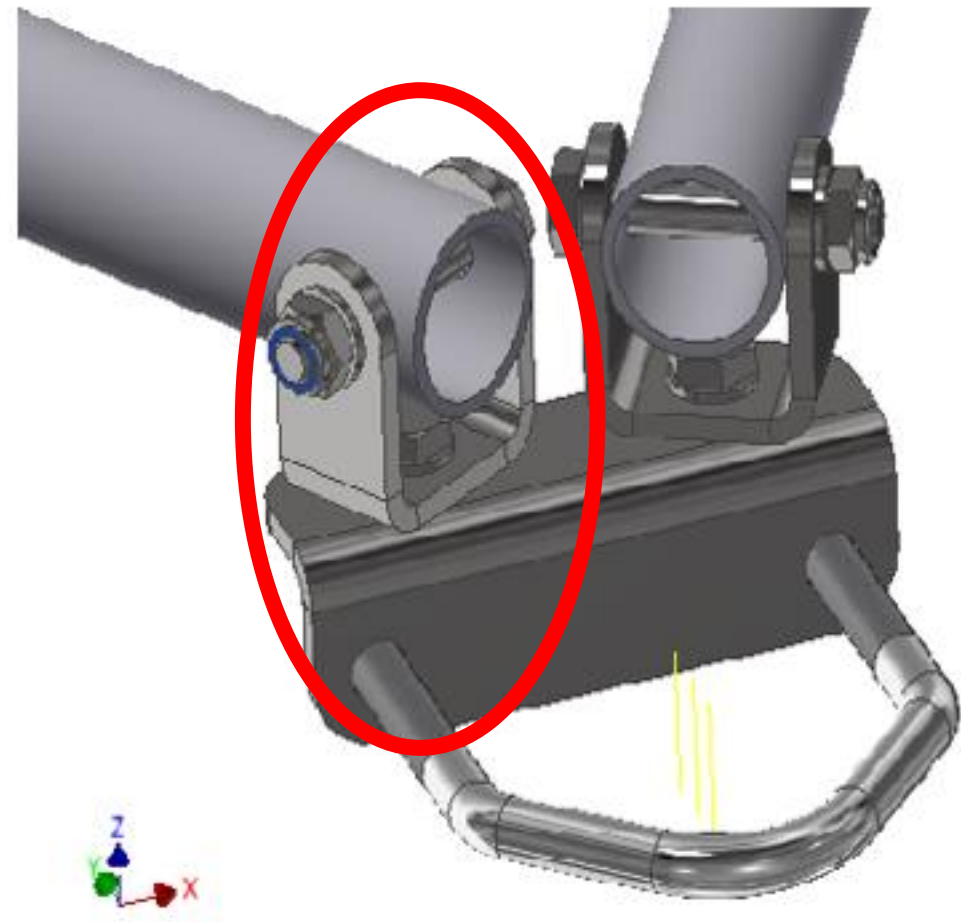
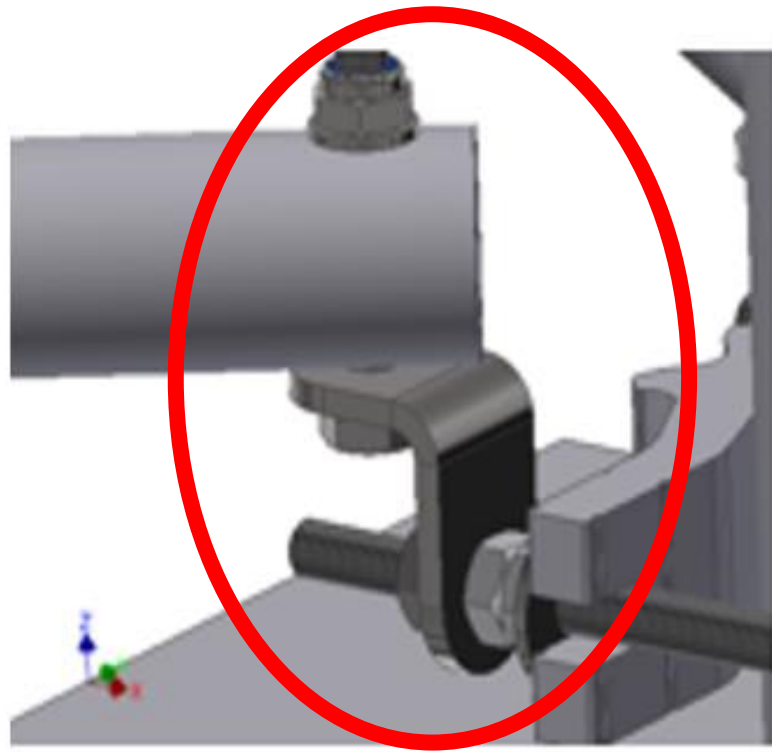


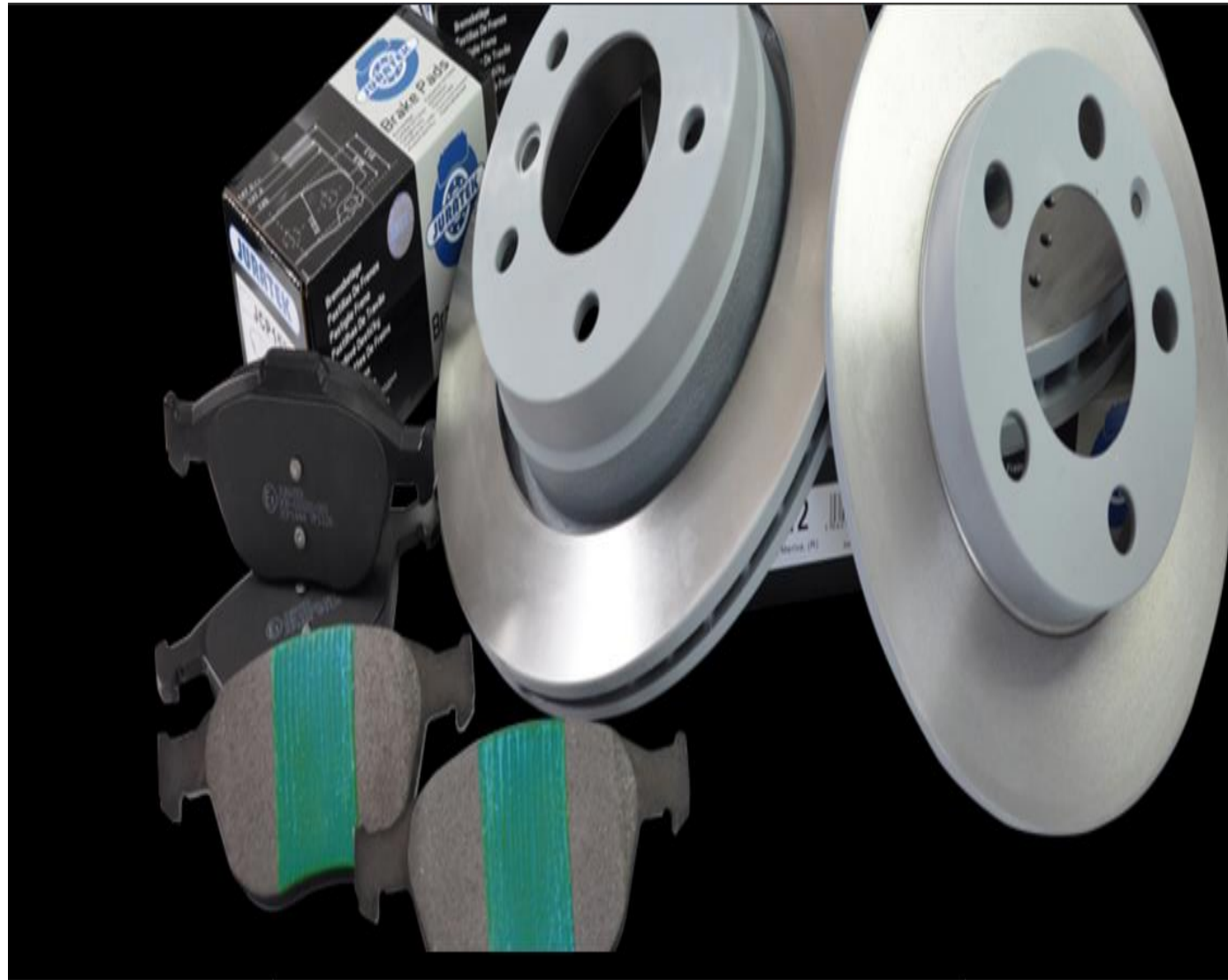
Figure 7 Max displacement vs frequency, x-direction.



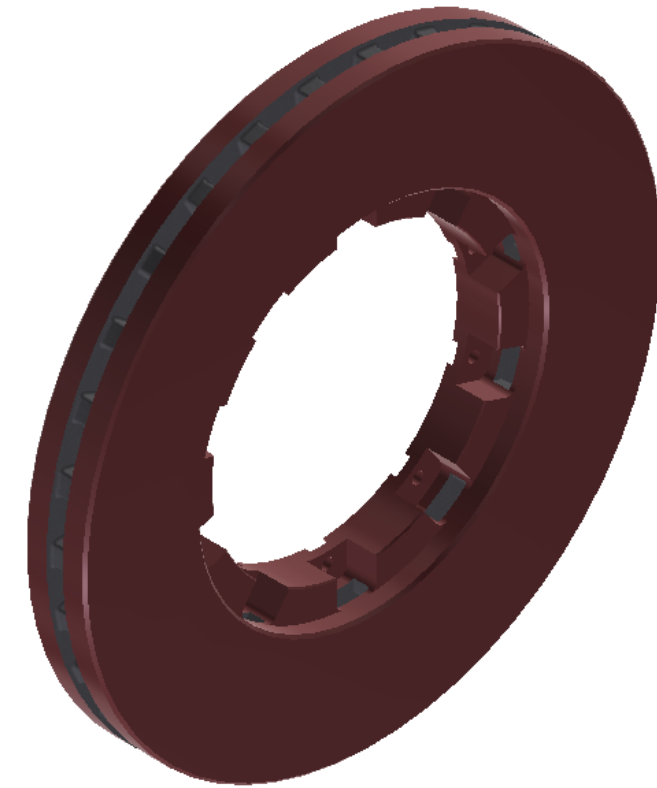
CUE DEE



Juratek (Thermal Stress)

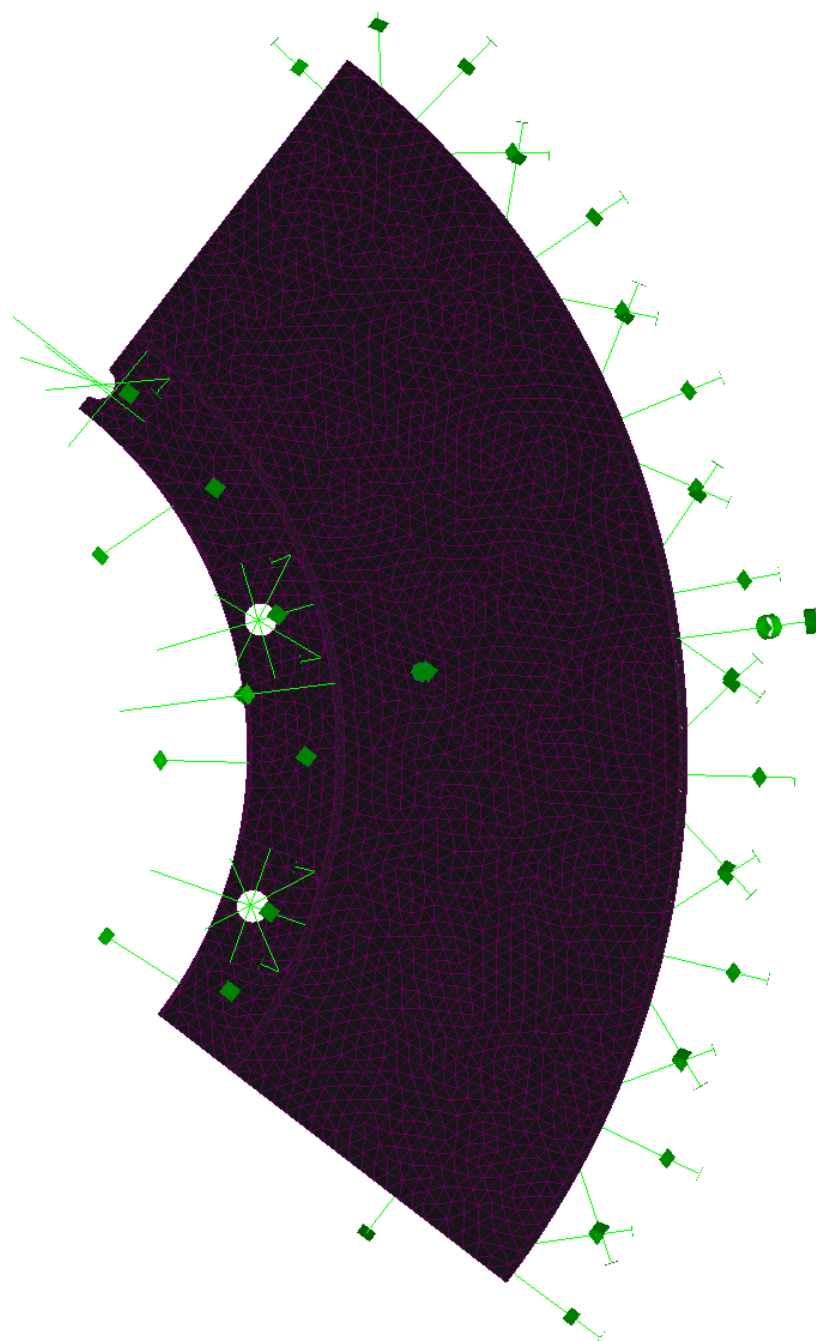
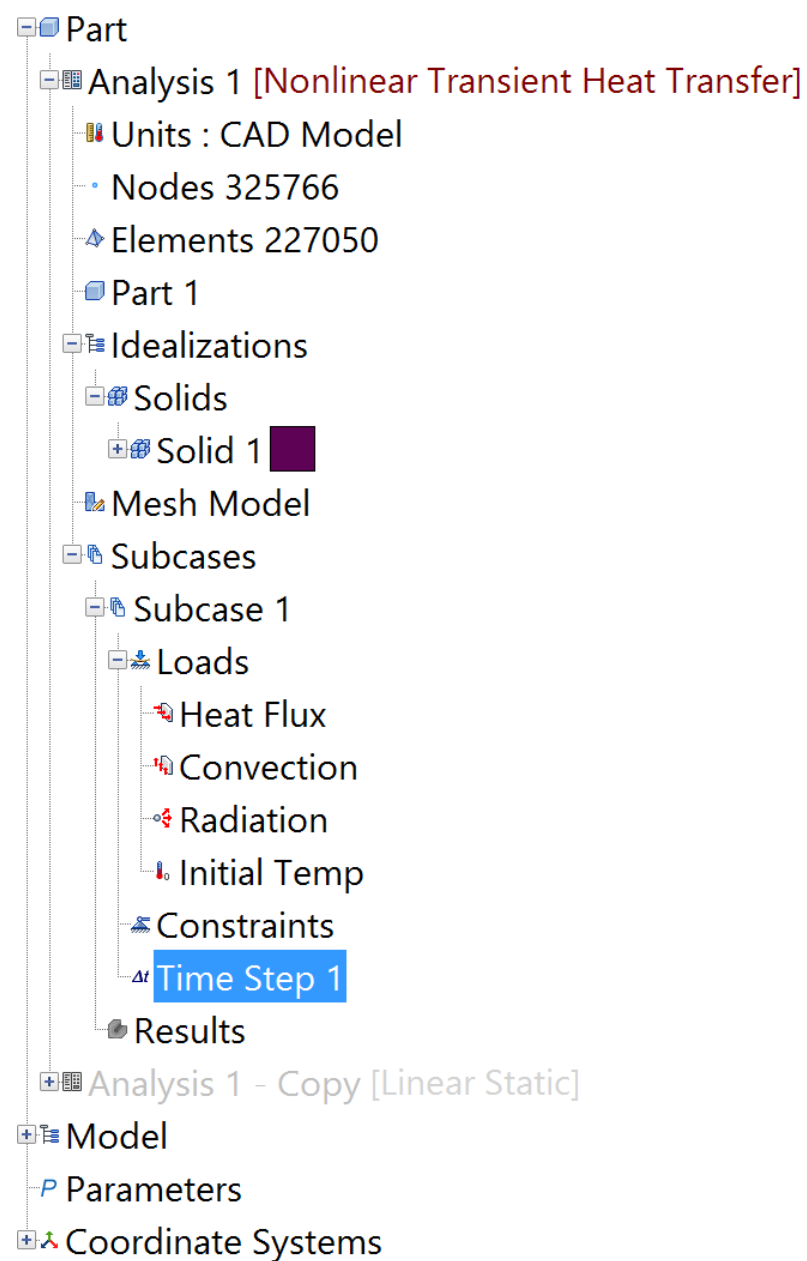


Goal: Is to determine stresses due to braking



Design Criteria:

- Stress is below yield limit



Time Step

Name: Time Step 1

ID: 1

Interval Listing:

0 to 4.5 s

Add Remove

Solution Settings

Step Method: ADAPTIVE

Interval Setup

Cycle Dependent

Duration (s):

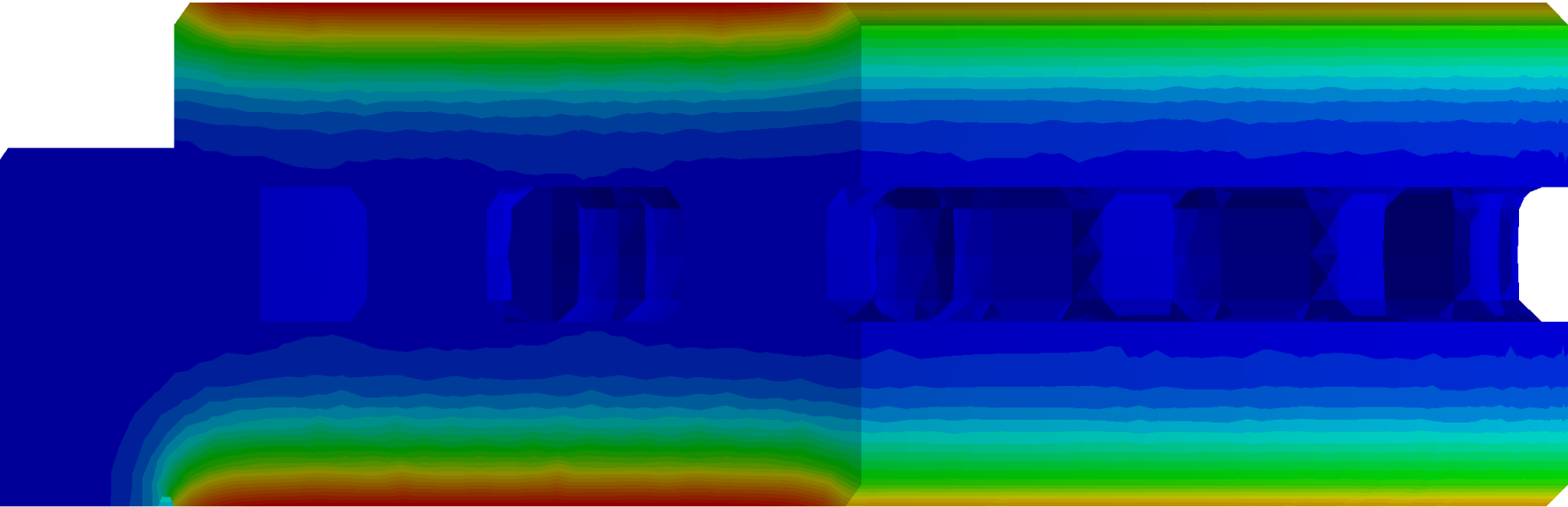
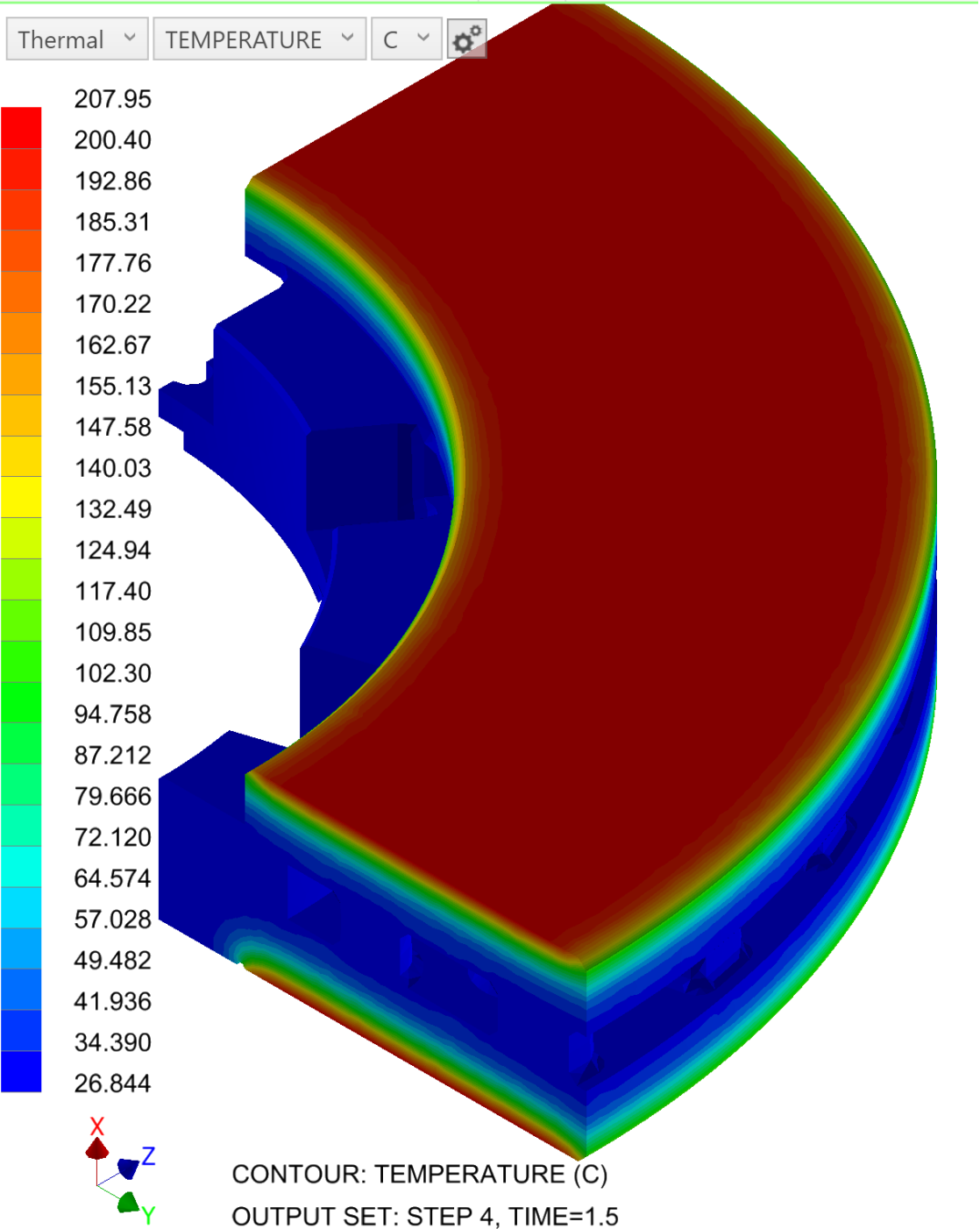
Time Step (s): 0.5

Number of Timesteps: 9

Duration (s): 4.5

Skip Factor (for output): 1

OK Cancel



Autodesk Nastran Model Tree

Part

Analysis 1 [Nonlinear Transient Heat Transfer]

Analysis 1 - Copy [Linear Static]

Units : CAD Model

Nodes 325766

Elements 227050

Part 1

Idealizations

Solids

Solid 1 - Copy

Mesh Model

Subcases

Subcase 1

Loads

Load 5

Constraints

Constraint 1

Constraint 2

Constraint 3

Results

Deformed

Displacement

Safety Factor

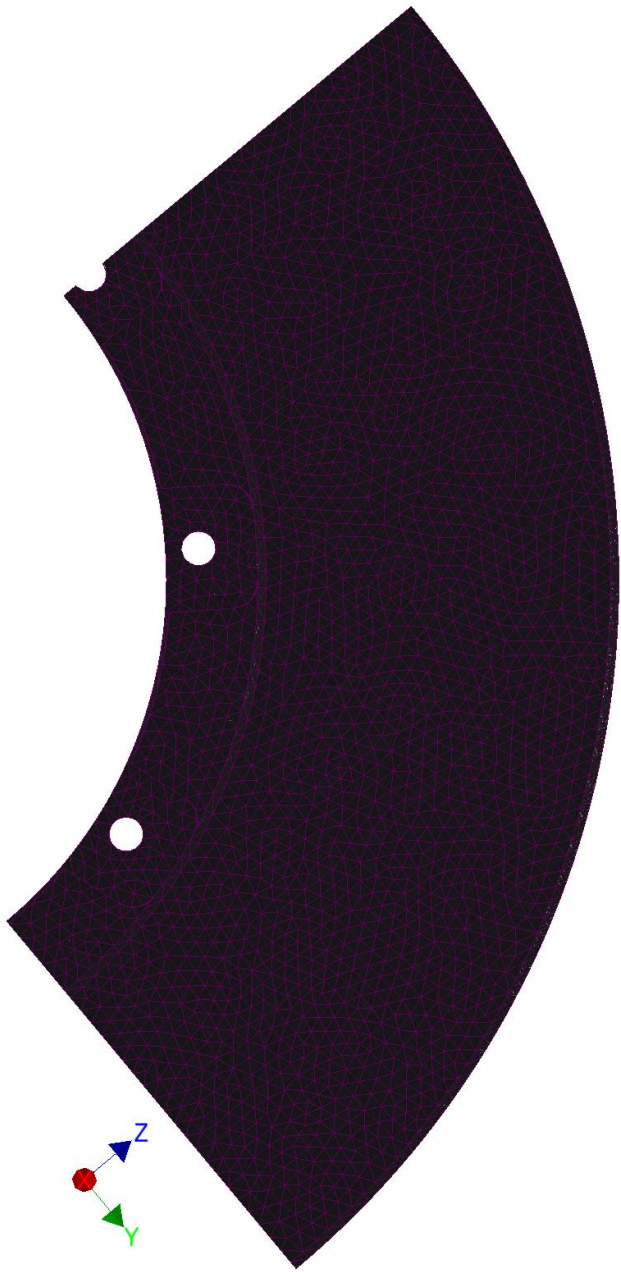
von Mises

XY Plot

Model

Parameters

Coordinate Systems



Load

Name: Load 5

ID: 5

Type: From Output

Sub Type:

Selected Entities:

Subcases:

Subcase 1

Display Options

Size:

Density:

Color:

Advanced Options >>

Load Definition

Results File:

C:\Users\wasyou\Desktop

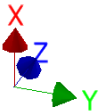
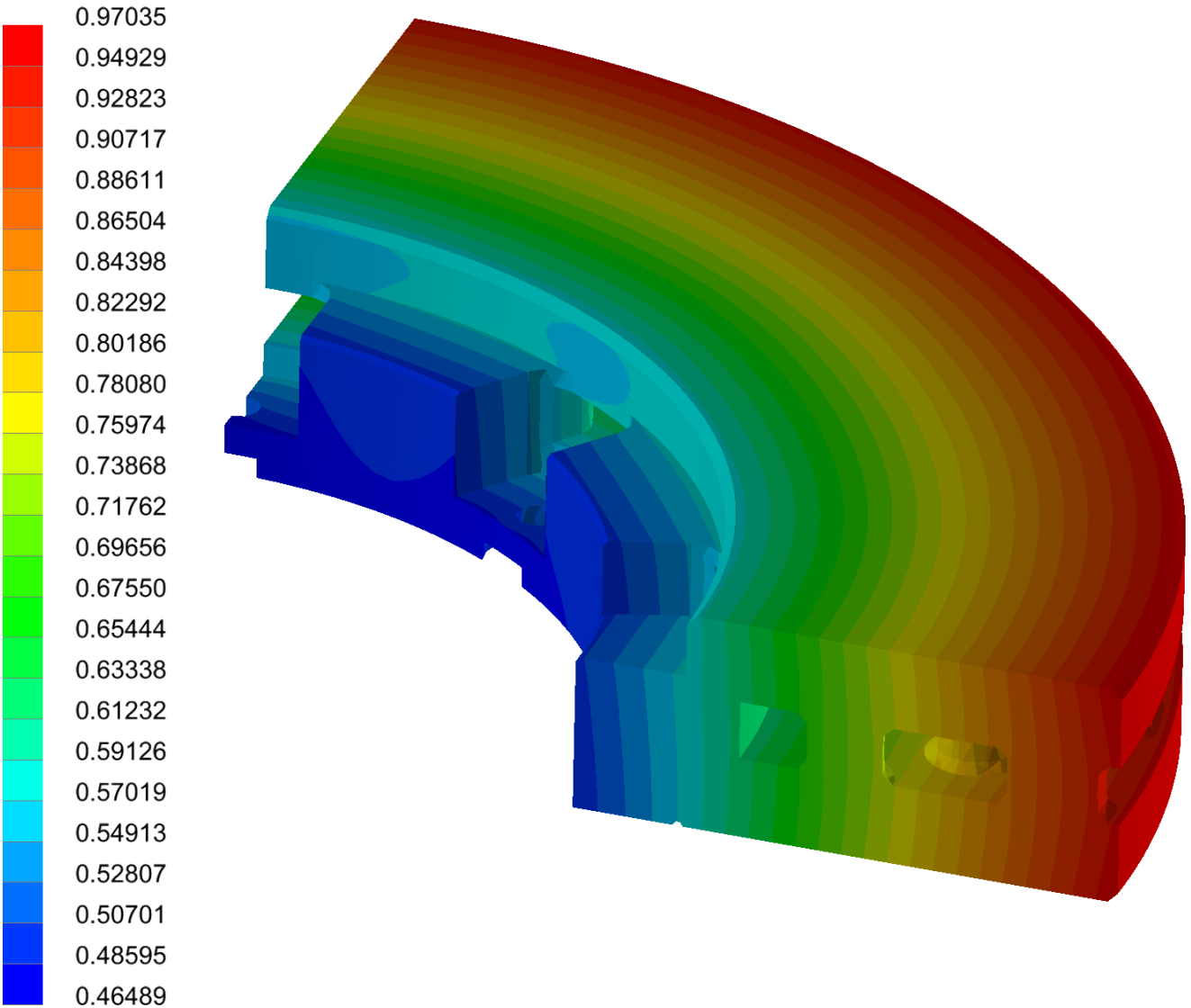
Output Set:

Nodal Load:

OK

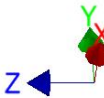
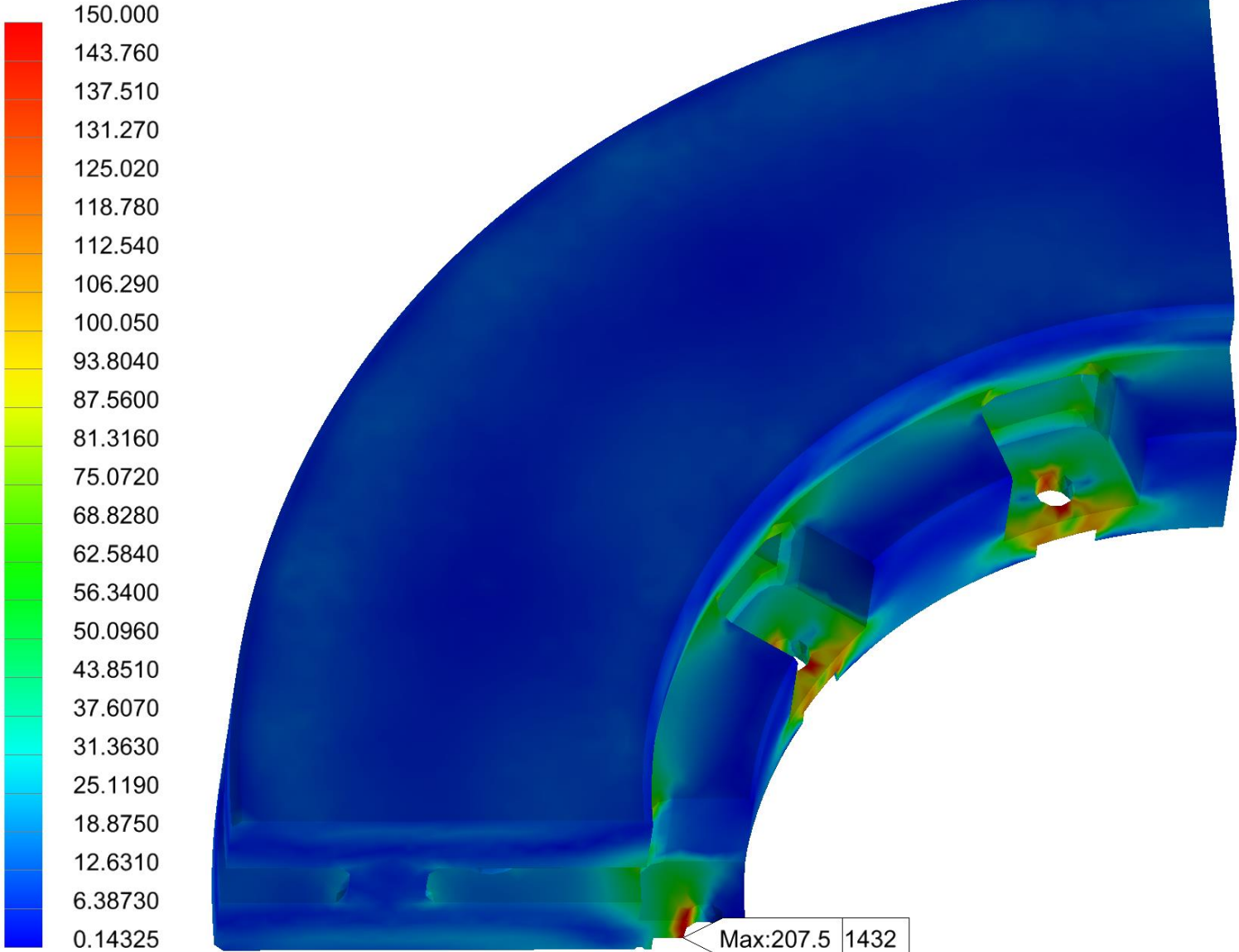
Cancel

Displacement ▾ TOTAL ▾ mm ▾ ⚙



CONTOUR: DISPLACEMENT (mm) (TOTAL)
OUTPUT SET: SUBCASE 1

Stress ▾ SOLID VON MISES STRESS ▾ MPa ▾ ⚙



CONTOUR: SOLID VON MISES STRESS (MPa)
OUTPUT SET: SUBCASE 1

Questions



Additional resources



- [Self paced learning books](#)
- [Training Courses](#)



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